

Periodic Update to the Run-on and Run-off Control System Plan Dolet Hills Fly Ash / Scrubber Sludge Landfill



CLECO Corporation

Dolet Hills Power Station Project No. 135359

> Revision 1 10/13/2021

Periodic Update to the Run-on and Run-off Control System Plan Dolet Hills Fly Ash / Scrubber Sludge Landfill

prepared for

CLECO Corporation Dolet Hills Power Station DeSoto Parish, Louisiana

Project No. 135359

Revision 1 10/13/2021

prepared by

Burns & McDonnell Engineering Company, Inc. Kansas City, Missouri

INDEX AND CERTIFICATION

CLECO Corporation Periodic Update to the Run-on and Run-off Control System Plan Dolet Hills Fly Ash / Scrubber Sludge Landfill

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Certification

I hereby certify, as a Professional Engineer in the state of Louisiana, that the information in this document was assembled under my direct supervisory control. This report is not intended or represented to be suitable for reuse by the CLECO Corporation or others without specific verification or adaptation by the Engineer.

Jason Entry

Jason C. Eichenberger, P.E. Louisiana License #42246

Date: October 13, 2021

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LIST OF ABBREVIATIONS

Abbreviation	Term/Phrase/Name
ac	Acre
BMcD	Burns & McDonnell
CCR	Coal Combustion Residual
CFR	Code of Federal Regulations
cfs	cubic feet per second
CLECO	CLECO Corporation
СҮ	cubic yard
Dolet Hills	Dolet Hills Power Station
ELG	Effluent Limitations Guidelines
EPA	Environmental Protection Agency
ft	Feet
GPM	Gallons per Minute
hr	Hour
in	Inch
Landfill	Fly Ash Scrubber Sludge Landfill
LPDES	Louisiana Pollutant Discharge Elimination System
LSU	Louisiana State University
MGD	Million Gallons per Day
min	Minute
NAD 83	North American Datum of 1983
NAVD 88	North American Vertical Datum of 1988

Abbreviation	Term/Phrase/Name
NRCS	Natural Resources Conservation Service
PFDS	Precipitation Frequency Data Server
RCRA	Resource Conservations and Recovery Act
SCS	Soil Conservation Service
U.S.C.	United States Code
USDA	US Department of Agriculture

1.0 INTRODUCTION

On April 17, 2015, the Environmental Protection Agency (EPA) issued the final version of the federal Coal Combustion Residual Rule (CCR Rule) to regulate the disposal of CCR materials generated at coalfired units. The rule will be administered as part of the Resource Conservation and Recovery Act [RCRA, 42 United States Code (U.S.C.) §6901 et seq.], using the Subtitle D approach.

CLECO Corporation (CLECO) is subject to the CCR Rule and as such must develop a run-on and run-off control system plan for each CCR landfill per 40 Code of Federal Regulations (CFR) §257.81 and prepare periodic plans every five years. This report serves as the periodic update to the initial run-on and run-off control system plan for the Fly Ash / Scrubber Sludge Landfill (the Landfill) at Dolet Hills Power Station (Dolet Hills).

This run-on and run-off control system plan is in addition to, not in place of, any other applicable site permits, environmental standards, or work safety practices.

2.0 PLAN OBJECTIVES

Per 40 CFR §257.81, the run-on and run-off control system plan must contain documentation (including supporting engineering calculations) that the control system has been designed and constructed to:

- Prevent flow onto the active portion of the CCR unit during peak discharge from a 25-year, 24-hour storm,
- Collect and control at least the water volume resulting from a 25-year, 24-hour storm, and
- Handle run-off from the active portion of the CCR landfill in accordance with the surface water requirements under 40 CFR §257.3-3.

Per 40 CFR §257.81(c)(5), CLECO must obtain certification from a qualified professional engineer that the run-on and run-off control system plan, and subsequent updates to the plan, meet the requirements of 40 CFR §257.81. This sealed document serves as that certification.

3.0 EXISTING CONDITIONS

Dolet Hills is located east of Mansfield in DeSoto Parish, Louisiana. Dolet Hills contains one CCR landfill which receives fly ash and scrubber sludge. The site plan is shown in Figure SK-CIVIL-001 in Appendix A.

Run-on and run-off controls were designed by others as part of the Landfill permit application to the Louisiana Department of Environmental Quality (LDEQ). The applicable sections of the permit renewal application prepared by Providence Engineering and Environmental Group LLC. in 2019 are included as Appendix B, along with as-built drawings of the current active landfill cell (Cell 11). The run-on and run-off control system plan provided herein is based on review and assessment of the certified permit information, as well as supplementary design documents and operational characteristics provided by CLECO.

3.1 Existing Design Document Review

The CCR Rule requires that peak stormwater flows from the 25-year, 24-hour storm event be handled by run-on and run-off control measures. The EPA defines run-on as any rainwater, leachate, or other liquid that drains over land onto any part of a CCR landfill or lateral expansion of a CCR landfill. The EPA defines run-off as any rainwater, leachate, or other liquid that drains over land from any part of a CCR landfill or lateral expansion of a CCR landfill. The EPA defines run-off as any rainwater, leachate, or other liquid that drains over land from any part of a CCR landfill or lateral expansion of a CCR landfill. The information included in Appendix B indicates compliance with the CCR Rule run-on and run-off control system plan requirements.

3.1.1 Run-on

The Landfill was sited so that it sits in a stream valley surrounded by ridgelines on three sides which prevent run-off from surrounding watersheds from entering the Landfill area. The Landfill filling sequence is such that filling begins in the southern, closed end of the stream valley and proceeds northward to the open end. As the Landfill is developed, perimeter drainage diversion dikes are configured to prevent outside run-off (non-contact stormwater run-off) from the portion of the Landfill not surrounded by a ridgeline from entering the Landfill cell. Perimeter drainage ditches collect this non-contact stormwater run-off and drain it offsite. The collection ditches have a triangular section with an average bottom slope of 2%, minimum 2-foot depth, and 3H:1V side slopes (see Figure 3-1).

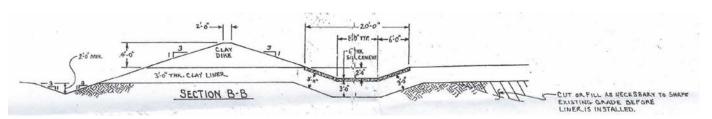


Figure 3-1: Typical run-off collection ditches and diversion dike

Additional diversion dikes are installed to prevent run-off from the closed portion of the Landfill from entering the active area. Run-off from the closed portion of the Landfill is typically drained offsite via natural drainage although some currently drains to the temporary sump as noted in Section 3.1.2.

3.1.2 Run-off

As the Landfill expands to the north, levees are reconstructed along the interface of the closed and open portions of the Landfill as well as around the perimeter of the open portion of the Landfill in order to isolate contact stormwater run-off from non-contact stormwater run-off.

As noted above, run-off from the closed portion of the landfill is collected in perimeter drainage ditches and typically discharged off-site via natural drainage. A series of perimeter drainage ditches within the levee divert contact stormwater run-off to a temporary sump. The perimeter ditches have an approximately trapezoidal section with an 8-foot bottom width, 1% bottom slope, 2-foot minimum depth, and 3H:1V side slopes (see Figure 3-1). At the time of this periodic update, there are currently approximately 10.5 acres of closed landfill that are still contributing to the sump area.

The landfill sump area is reconstructed each time the landfill expands. The sump area consists of a primary sump (i.e., the Cell 11 Sedimentation Pond) which overflows to an auxiliary sump (i.e., the Cell 11 Overflow Sump) via a concrete spillway. From the auxiliary sump, flow is discharged via a 36-inch vertical outlet pipe which ties into a 48-inch collector pipe which gravity drains to the Runoff Pond. The current Cell 11 sump spillway is trapezoidal in shape with a bottom width of 20 feet and 6H:1V side slopes. Refer to Appendix B for existing design drawings.

The Runoff Pond is approximately 4-acres and sits north of the Landfill cell. The pond is partially surrounded by a run-on diversion dike to limit run-off inflow from the surrounding watershed area (see DWG No. DH-123 in Appendix B). The pond is designed to store contact run-off from the 25-year, 24-hour storm and contains an emergency spillway for larger storm events. The concrete spillway was added to the pond in 1998 when the dike was raised and the reinforced concrete wall was installed. The top of dam is now approximately 270 feet.

From the Runoff Pond, run-off may be discharged via a valve-controlled outlet pipe. The valve is normally closed and has an invert elevation of 253 feet. For the purposes of this modeling effort, Burns & McDonnell has assumed that the plant operations team maintains the normal water level (prior to rain events) at or below elevation 259.0. Water stored in the pond may be discharged under the conditions of the discharge permit (LA0062600); consequently, all discharges are permitted and conform to CFR 257.3-3.

4.0 DESIGN BASIS / FLOOD CONTROL SYSTEM

4.1 Capacity Criteria

The CCR Rule discusses that stormwater control systems at CCR landfills must have adequate hydrologic and hydraulic capacity to manage flows for the 25-year, 24-hour storm event. For this analysis, the criteria was interpreted as being that the top of the stormwater conveyance and storage features should not be overtopped during the design storm event.

4.2 Project Mapping

Project mapping for this analysis consisted of an inventory of stormwater assets that contribute to the surface impoundment. Two primary sources of information were utilized: construction record drawings and publicly available LiDAR survey data.

4.2.1 Mapping Sources

Survey data utilized included LiDAR topography from the Louisiana State University (LSU) Atlas LiDAR Downloader, which was posted in February of 2008 and retrieved in January of 2016. Construction record drawings of the Landfill, sump area, and surface impoundment were also utilized in the analysis.

4.2.2 Vertical Datum

Mapping sources referenced were in the North American Vertical Datum of 1988 (NAVD 88).

4.2.3 Horizontal Coordinate System

Data from the LSU Atlas LiDAR which was utilized as the basis for mapping and modeling efforts is in the Louisiana State Plane North, North American Datum of 1983 (NAD 83) coordinate system.

5.0 HYDROLOGIC AND HYDRAULIC CAPACITY

HydroCAD 10.00-24 was used to model drainage area and basin characteristics under the design storm event and FlowMaster V8i was used to model channel characteristics. Inputs to the HydroCAD and FlowMaster models are described in the following sections. For detailed calculations, refer to Appendix C.

5.1 Rainfall Distribution and Depth

The Soil Conservation Service (SCS) Type III rainfall distribution was used for computations associated with this evaluation. Precipitation data was acquired from the NOAA Precipitation Frequency Data Server (PFDS). Precipitation depth for design storm event is 8.16 inches.

5.2 Subbasin Characteristics

5.2.1 Landfill

Stormwater falling over the open portion of the Landfill (see SK-CIVIL-002 in Appendix A for approximate limits) is collected in the contact stormwater run-off ditches which drain to the sump(s) and then to the Runoff Pond via the 48-inch collector pipe. This watershed consists mainly of steeply sloped (3H:1V), compacted CCR material. Calculations for this watershed area were determined based on the parameters shown in Table 5-1.

Component	Value	Unit
Watershed Area (currently includes 10.5 acres of capped landfill still contributing to		
sump and runoff pond)	44.1	ac
Weighted Curve Number	85	-
Time of Concentration	16.2	min

Table 5-1: Watershed Run-off Calculated Data for Landfill Run-off

5.2.2 Runoff Pond

Drainage into the Runoff Pond (see SK-CIVIL-002 in Appendix A for approximate watershed limits) is minimized, in part, by dikes surrounding the pond. This watershed consists mainly of moderately sloped (8H:1V), undeveloped, forested area with grassy, open areas near the pond limits. Calculations for the Runoff Pond watershed area were determined based on the parameters shown in Table 5-2.

Component	Value	Unit
Watershed Area	7.7	ac
Weighted Curve Number	88	-
Time of Concentration	13.7	min

Table 5-2: Watershed Run-off Calculated Data for Runoff Pond

5.2.3 Outside Run-off

Stormwater falling over the outside run-off area (see SK-CIVIL-002 in Appendix A for approximate watershed limits) is collected in run-off collection ditches which drain offsite. This watershed consists mainly of moderately sloped (8H:1V), undeveloped, forested area with grassy, open areas near the Landfill limits. Calculations for this watershed were determined based on the parameters shown in Table 5-3.

Table 5-3: Watershed Run-off Calculated Data for Outside Run-off

Component	Value	Unit
Watershed Area	4.0	ac
Weighted Curve Number	80	-
Time of Concentration	7.2	min

5.3 Channel Characteristics

Flow calculations were determined based on the channel parameters shown in Table 5-4 (contact stormwater run-off) and Table 5-5 (non-contact stormwater run-off).

Table 5-4: Channel Data for Contact Stormwater Run-off, Flat Bottom Ditch

Component	Value	Unit
Roughness Coefficient, Manning's n	0.012	(geomembrane liner)
Channel Slope	0.01	ft/ft
Left Side Slope	3H:1V	-
Right Side Slope	3H:1V	-
Bottom Width	8.00	ft

Table 5-5: Channel Data for Non-Contact Stormwater Run-off, Triangular Ditch

Component	Value	Unit
Roughness Coefficient, Manning's n	0.025	(earth, clean & winding)
Channel Slope	0.02	ft/ft
Left Side Slope	3H:1V	-
Right Side Slope	3H:1V	-

6.0 RESULTS

6.1 Basins

Ponds were modeled under the 25-year, 24-hour storm event with results as follows:

Component	Property	Value	Unit
Subcatchment	Runoff Depth	6.37	in
Landfill	Peak Runoff	233.81	cfs
Pond Cell 11	Initial Elevation	286.00	ft
Sedimentation	Peak Inflow	233.81	cfs
Pond	Peak Discharge	229.92	cfs
	Peak Elevation	287.81	ft
	Peak Storage	2.721	ac-ft
Pond	Initial Elevation	N/A	ft
Cell 11 Overflow Sump	Peak Inflow	229.92	cfs
	Peak Discharge	217.41	cfs
	Peak Elevation	285.19	ft
	Peak Storage	0.183	ac-ft

Table 6-1: Modeled Conditions – Landfill

Component	Property	Value	Unit
Subcatchment Watershed	Runoff Depth	6.72	in
Watersheu	Peak Runoff	44.99	cfs
Pond Runoff Pond	Initial EL	259.0	ft
	Peak Inflow	253.91	cfs
	Peak Discharge	0.00	cfs
	Peak EL	268.52	ft
	Peak Storage	38.913	ac-ft

Component	Property	Value	Unit
Subcatchment	Runoff Depth	5.78	in
Watershed	Peak Runoff	25.38	cfs

The Landfill sumps and the Runoff Pond do not overtop under the modeled conditions; therefore, it can be assumed that they are adequately sized to control run-off the 25-year, 24-hour storm event (as long as the plant operations team maintains a normal water level in the Runoff Pond less than 259.0 ft). After a

significant storm event, excess water collected in the Runoff Pond can be discharged under the conditions of the LPDES permit.

6.2 Stormwater Channels

Under the modeled conditions, the channels were able to control and convey the design storm. The results of the modeled peak conditions are as follows:

Property	Peak Discharge (cfs)	Normal Depth (in)
Contact Stormwater Run-off 1/2 Landfill (Open)	116.91	12.2
Non-Contact Stormwater Run-off Outside Run-off	25.38	14.5

Table 6-4: Modeled Channel Conditions

6.2.1 Contact Stormwater Run-off (Open Portion of Landfill)

Contact stormwater run-off (run-off from the open portion of the Landfill) from the design storm is conveyed to the sump area via perimeter drainage ditches which are at minimum 2 feet deep, not including the height of the clay diversion dike. At the maximum flow rate, the contact stormwater run-off will have a normal depth of 1.02 feet within the drainage ditch. Because the stormwater channels do not overtop during the design storm event, it can be assumed that they are adequately sized to convey contact stormwater run-off from the 25-year, 24-hour storm event.

6.2.2 Non-Contact Stormwater Run-off (Outside Run-off)

Non-contact stormwater run-off (outside run-off) from the design storm is discharged off-site via perimeter drainage ditches which are at minimum 2 feet deep, not including the height of the clay diversion dike. At the maximum flow rate, the non-contact stormwater run-off will have a normal depth of 1.21 feet within the drainage ditch. Because the stormwater channels do not overtop during the design storm event, it can be determined that they are adequately sized to convey run-off from the 25-year, 24-hour storm event.

7.0 STORMWATER BEST MANAGEMENT PRACTICES

Stormwater best management practices (BMPs) shall be employed at the site to comply with CFR 257.3-3 which, in summary, stipulates that a facility shall not cause a discharge of pollutants, dredged material, or fill material to waters of the United States or cause non-point source pollution of waters of the United States.

Vegetation enhances evapotranspiration and reduces erosion, thus playing an important part in surface water control. Channels not requiring riprap shall be prepared for seeding as they are constructed. Final cover shall be prepared for seeding after it is applied. The use of terrace and downdrain channels for stormwater conveyance provides a means to control run-off velocities and reduce sediment transport.

8.0 PERIODIC ASSESSMENT AND AMMENDMENT

CLECO placed the initial run-on and run-off control system plan in the CCR Operating Record by October 17, 2016. CLECO must prepare periodic run-on and run-off control system plans every five years. This report serves as the first periodic update to the initial run-on and run-off control system plan. CLECO may amend the plan at any time and is required to do so whenever there is a change in conditions which would substantially affect the written plan in effect. Preparing the periodic plans may be achieved by reviewing the current plan in effect and amending the plan as required. In all cases, the date for completing the previous plan is the basis for establishing the deadline to complete the subsequent periodic plan. Each periodic plan shall be certified by a qualified professional engineer in the state of Louisiana. All amendments and revisions must be placed on the CCR public website within a reasonable amount of time following placement in the facility's CCR Operating Record. A record of revisions made to this document is included in Section 9.0.

9.0 REVISIONS AND UPDATES

Revision Number	Date	Revisions Made	By Whom
Humbol	Duito		by mon
0	10/14/2016	Initial Issue	Burns & McDonnell
1	10/13/2021	Periodic Update to the Initial Plan	Burns & McDonnell

APPENDIX A – SITE PLAN

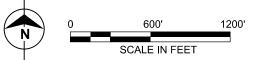
NOTES:

- 1. RUN-OFF FROM THE OPEN PORTION OF THE LANDFILL IS ISOLATED FROM RUN-OFF FROM THE CLOSED PORTION OF THE LANDFILL VIA DIVERSION DIKES AND CONVEYED TO SUMP AND RUNOFF POND. RUN-OFF FROM CLOSED PORTION OF LANDFILL WHICH DOES NOT DRAIN TO SUMP IS CONVEYED OFF-SITE VIA NATURAL DRAINAGE.
- 2. AS THE LANDFILL EXPANDS, ONLY 40 ACRES ARE "OPEN" (OPERATING WITHOUT COVER) AT A GIVEN POINT IN TIME. THE SUMP AREÁ, **DIVERSION DIKES, AND PERIMETER COLLECTION** DITCHES ARE RE-CONFIGURED FOR EACH PHASE OF CONSTRUCTION.



date 8/20/2021

designed A. MYERS



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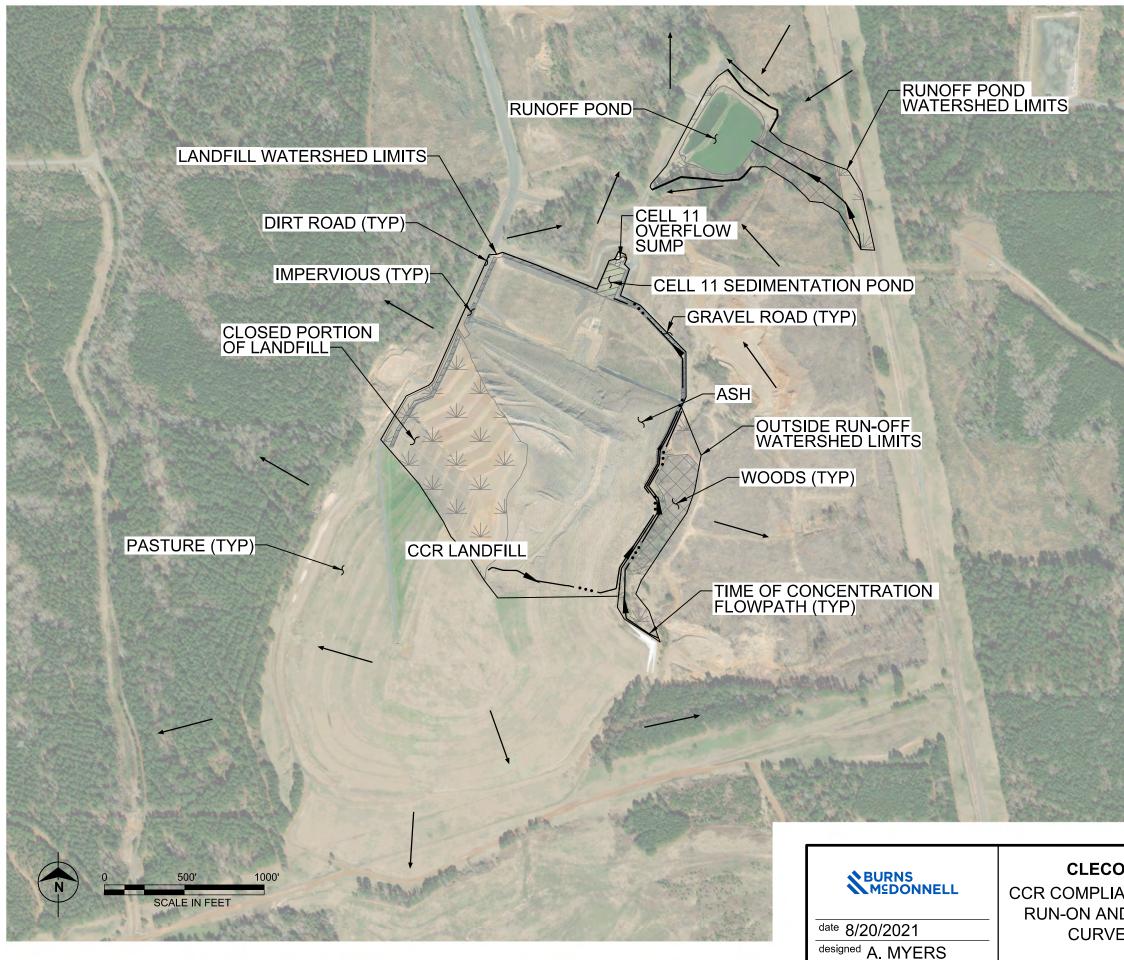
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OUTSIDE RUN-OFF WATERSHED LIMITS

CLECO CORPORATION CCR COMPLIANCE DOCUMENTATION RUN-ON AND RUN-OFF CONTROL SITE PLAN

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CLECO CORPORATION CCR COMPLIANCE DOCUMENTATION RUN-ON AND RUN-OFF CONTROL CURVE NUMBER DATA

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contract

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APPENDIX B – EXISTING PERMIT INFORMATION / DRAWINGS

ATTACHMENT 22

DESCRIPTION OF FACILITY RUNOFF COLLECTION SYSTEM

ATTACHMENT 22

DESCRIPTION OF FACILITY RUNOFF COLLECTION SYSTEM

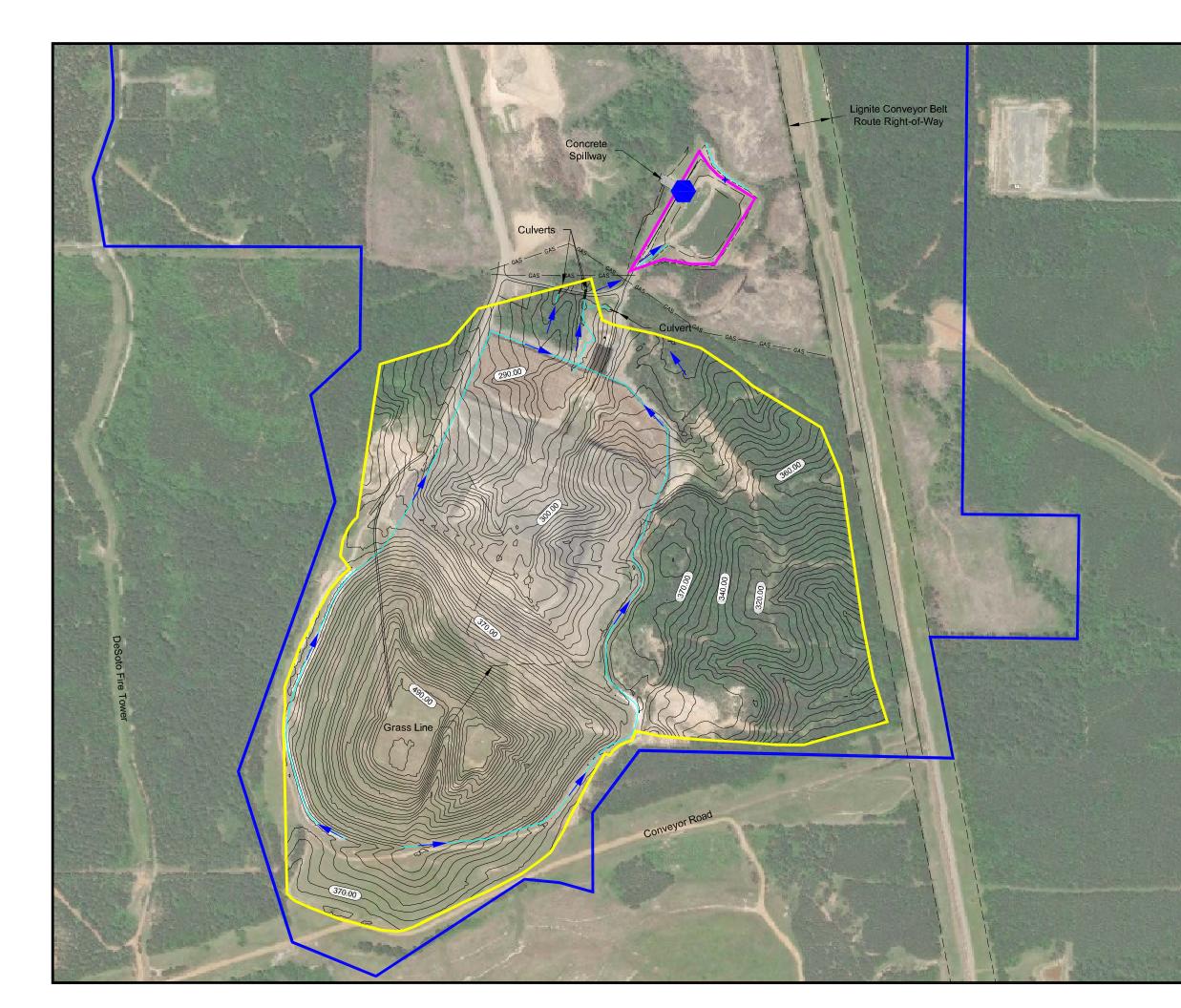
The purpose of the impoundment is to store contact storm water runoff from the active cell(s) of the landfill resulting from the 25-year, 24-hour design storm. The stored runoff will be discharged under conditions of the power station's water discharge permits. **Attachment 22** shows the site runoff collection system. This system consists of levees that will be constructed along the northern edge of the covered cells and down the valley slopes on either side of the active cell. The levee alignment along the valley slope will be such that it will encompass all of the waste placed in the active cells. This levee will segregate non-contact storm water runoff from contact storm water runoff. All rain falling within the levee will flow by gravity to a temporary collection sump located at the lowest end of the active cell area. A dike will be constructed across the valley to prevent any runoff from leaving the site. The collected runoff will then be transferred to the surface impoundment where it will be discharged under the conditions of the power station's water discharge permits. All rainfall that contacts the waste will be collected and transported to the surface impoundment.

Since the waste will have no free liquids nor generate any leachate, the only water that must be removed is rainfall. The system of culverts, levees, swales, sumps, and pumps described previously will be used to dewater the site when necessary.

All rain falling within areas of the landfill that have received certified final cover will be routed to other storm water outfalls.

Waste materials disposed in the expansion area will have no free liquids or generate any leachate. The only water required to be removed from the expansion area is rainfall. A perimeter levee system will be constructed around the expansion area to prevent runon from entering the operational areas of the facility expansion. This perimeter levee will also prevent runoff from leaving the operational areas of the facility expansion. As each disposal cell is constructed in the expansion area, a cell separation berm will be constructed to contain and capture all contact storm water runoff from each active cell. This collected storm water will be pumped from within each active cell and transported via gravity main or force main to the existing surface impoundment.

As final cover is installed in the expansion area, all non-contact storm water runoff from the certified closed areas will be routed to other storm water outfalls.



Legend

- Property Boundary
- Permitted Landfill Limit
- Drainage Ditch
- ———— Right-of-Way
- GAS Gas Pipeline
 - —— 5' Lidar Contours (10/17/19)
- Surface Flow Direction
 - Outfall Location

Reference

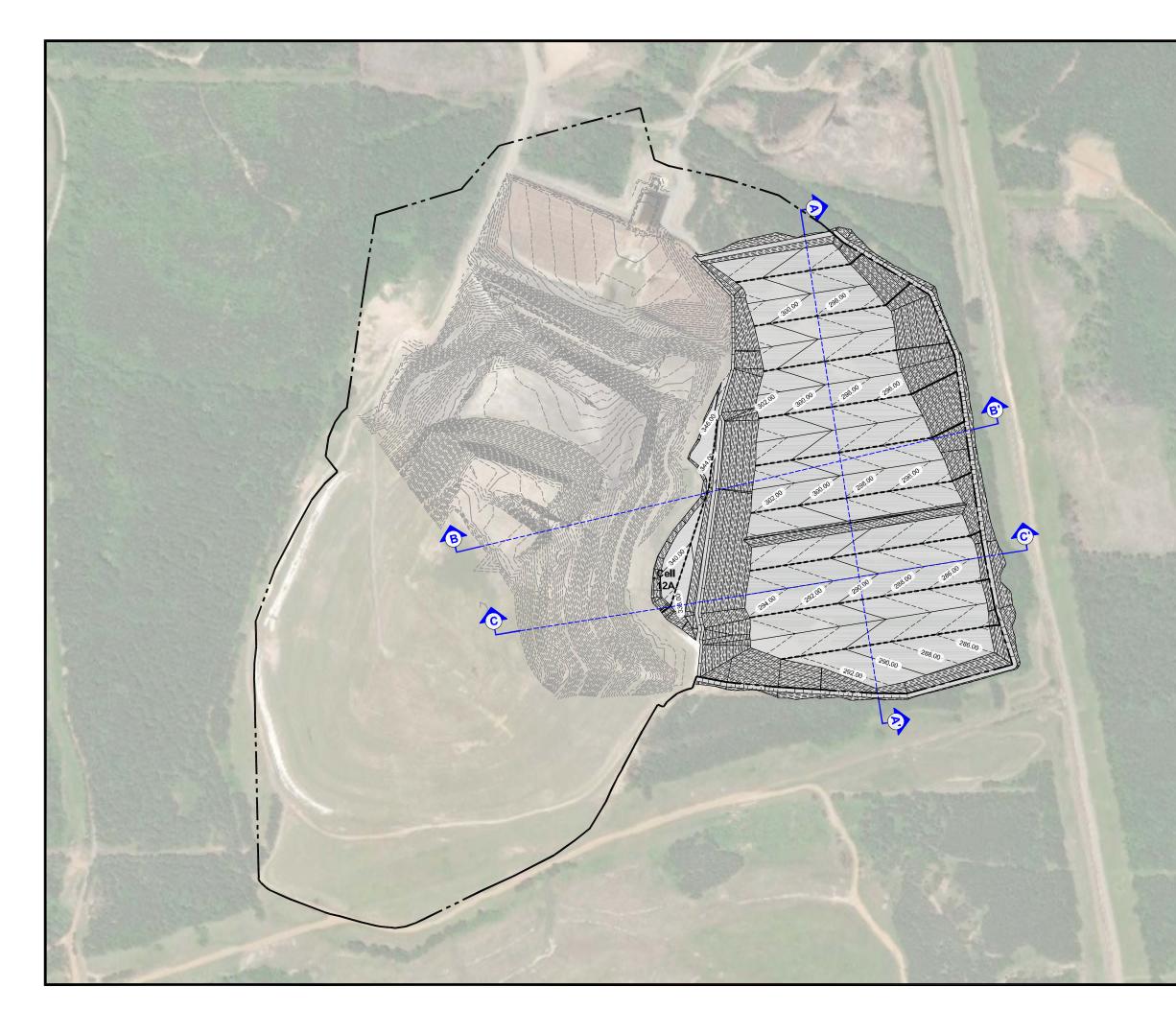
Base map comprised of Bing aerial imagery 06/18/19 and client provided file name: 13-51 topo.dwg.

) 1'' = 500'	500	
Facility Collectio			
Solid Waste Permit Renewal Mansfield, DeSoto Parish, Louisiana			
Cleco Power LLC Dolet Hills Power Station			
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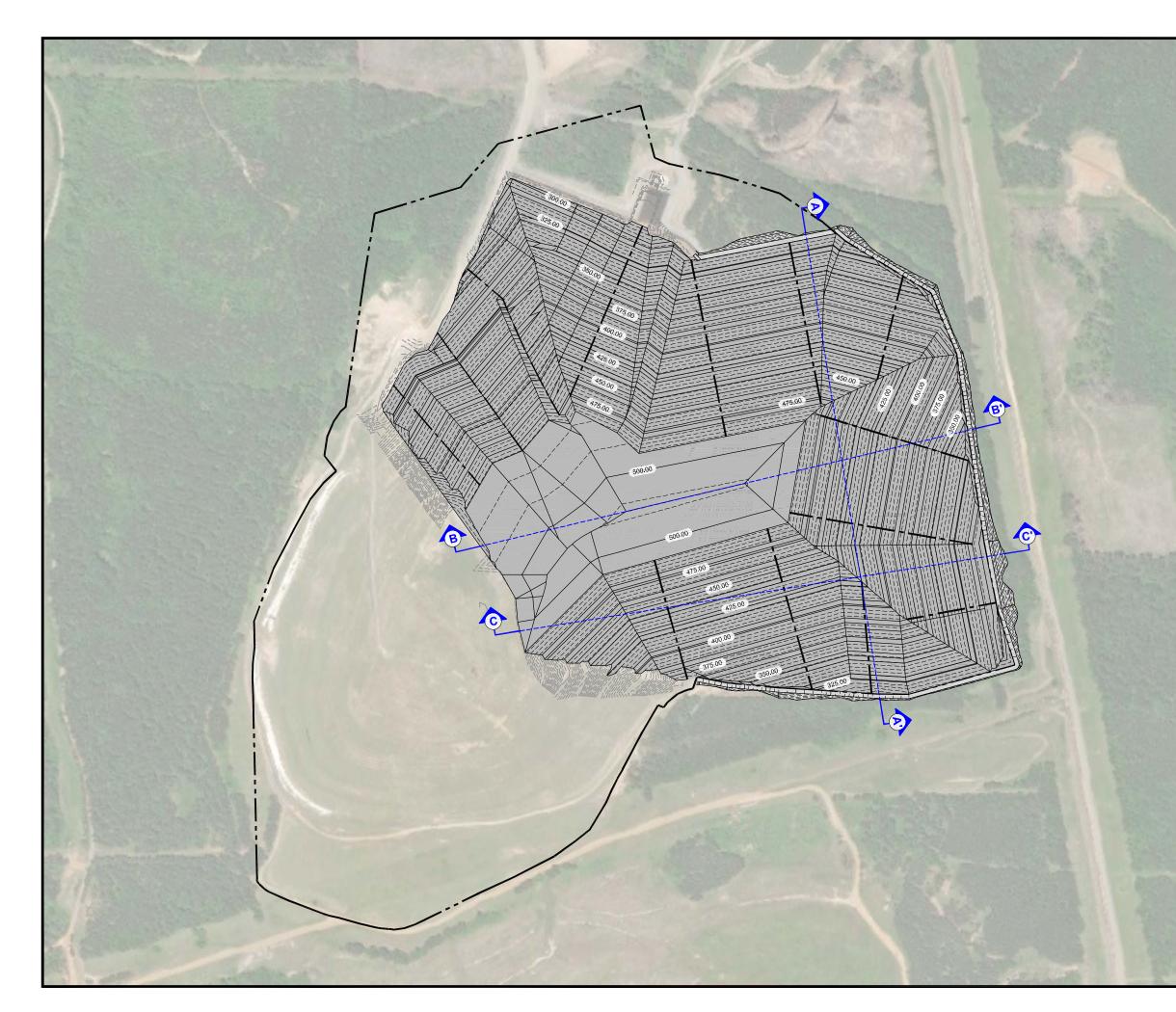
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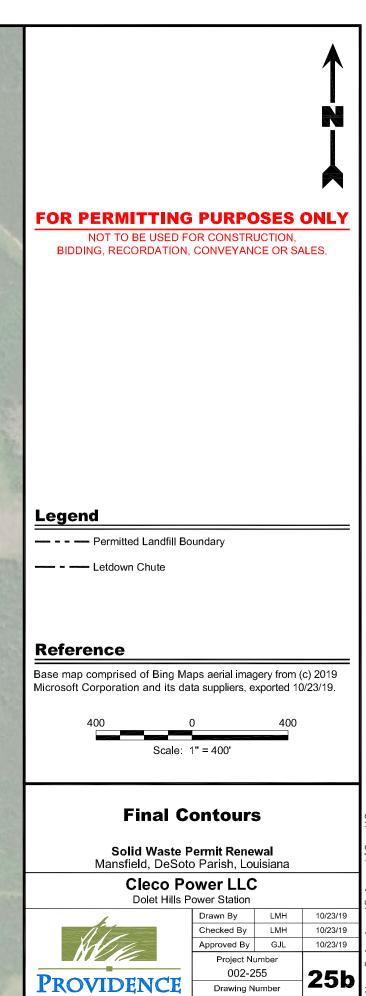
ATTACHMENT 25

PLAN-VIEW DRAWINGS SHOWING ORIGINAL CONTOURS, PROPOSED ELEVATIONS, PROPOSED FINAL CONTOURS, SLOPES, LEVEES, AND OTHER PERTINENT FEATURES



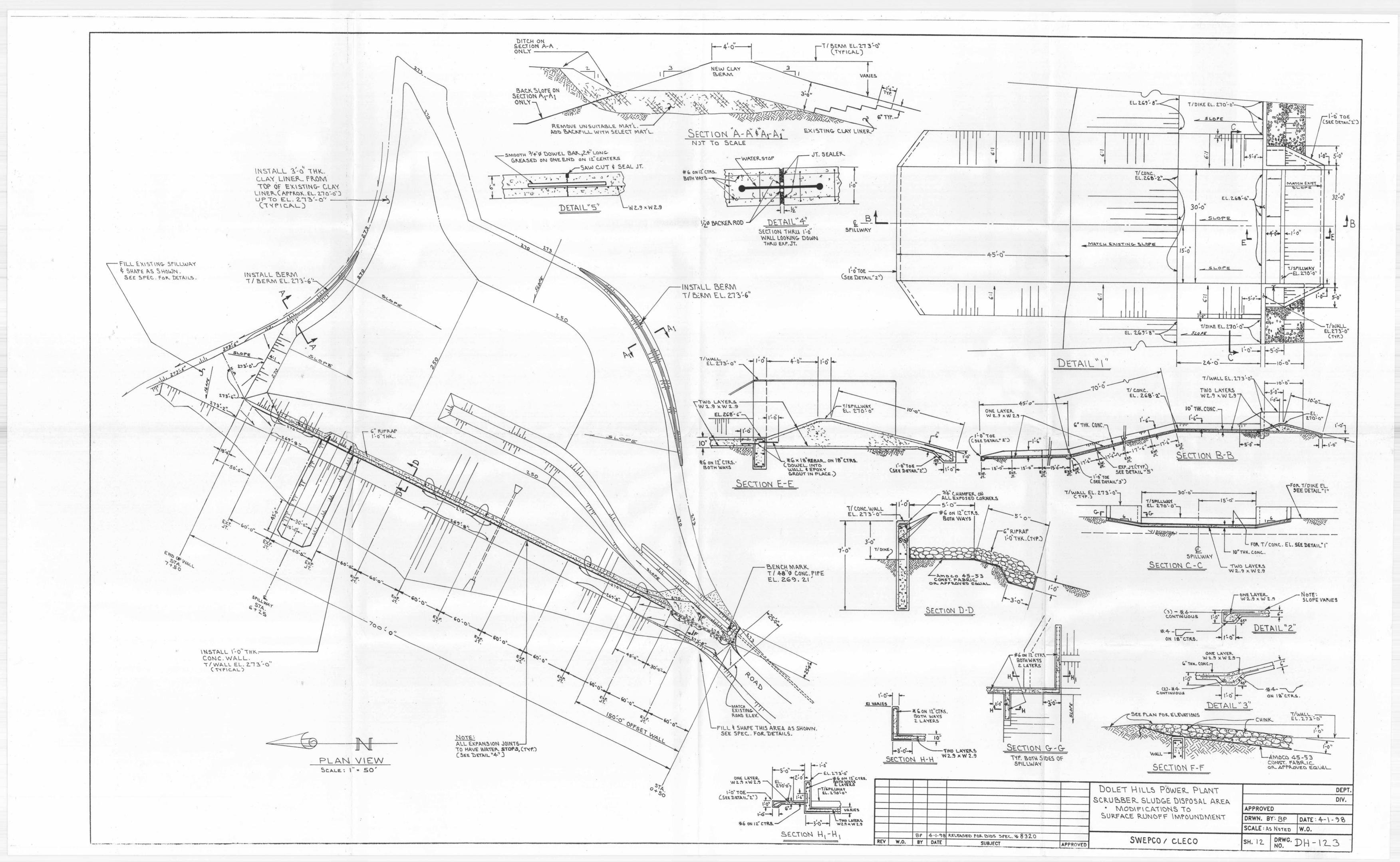
FOR PERMITTING NOT TO BE USED F BIDDING, RECORDATION	OR CONSTR	UCTION,	
Lorond			
Legend			
Permitted Landfill B	·		
Leachate Riser Pipe	9		
Leachate Collection	Pipe		
Reference			
Base map comprised of Bing M Microsoft Corporation and its da			
400	0	400	
Scale:	1" = 400'		
Excava	tion Pla	n	
Solid Waste	Salid Waste Damet Damer		
	Solid Waste Permit Renewal Mansfield, DeSoto Parish, Louisiana		
	ower LLC Power Station	;	
	Drawn By	LMH	10/23/19
Alle	Checked By Approved By	LMH GJL	10/23/19 10/23/19
	Project N	umber	
PROVIDENCE	002-2 Drawing N		25a
	-		Attachment





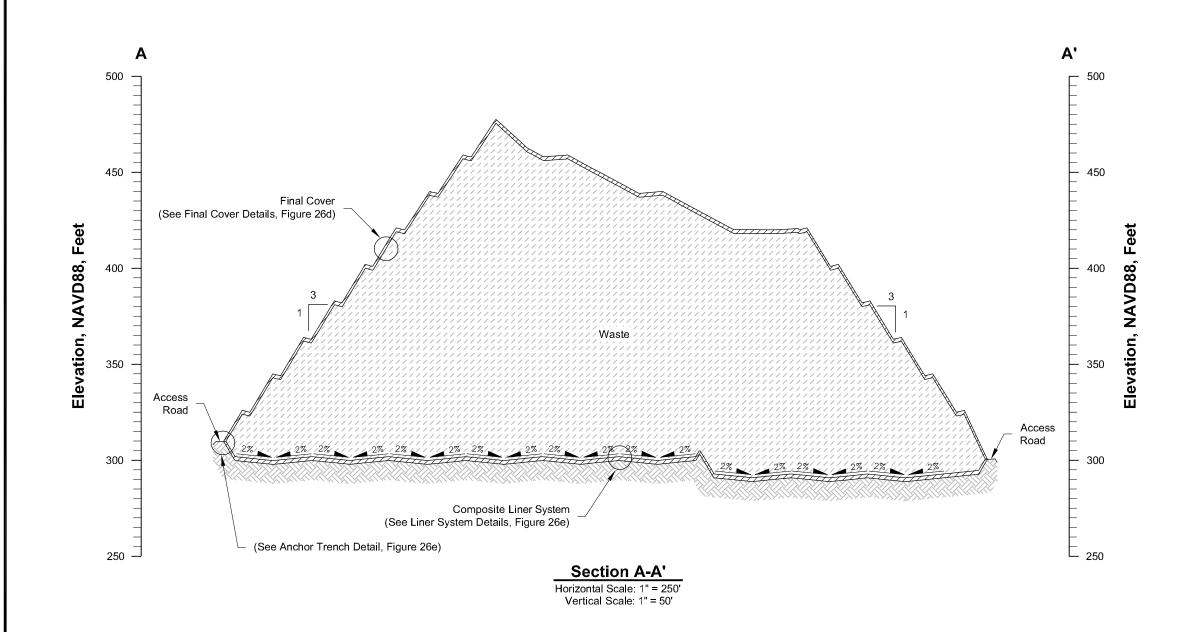
Attachmen

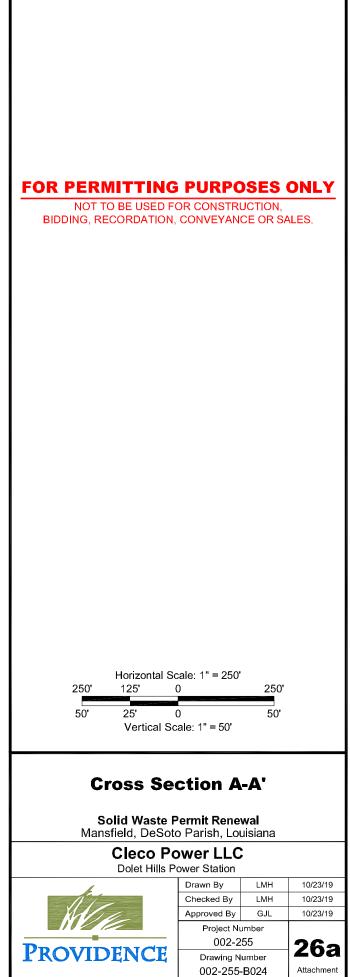
002-255-B023



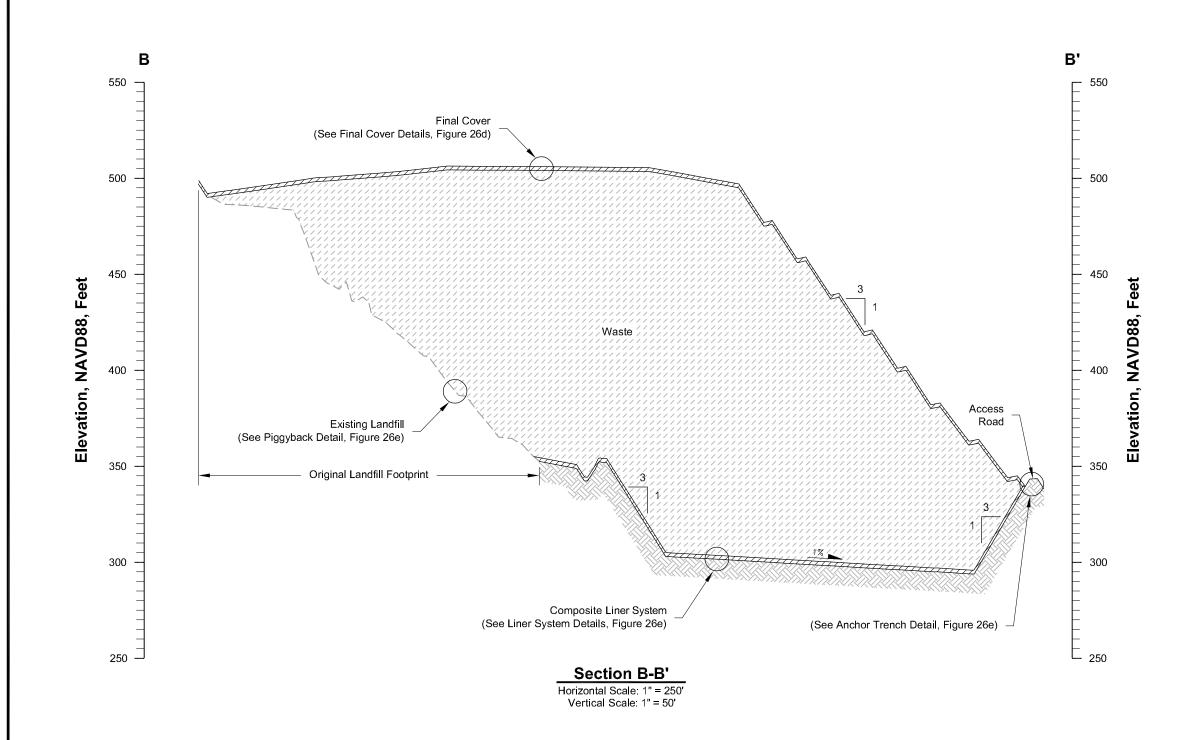
ATTACHMENT 26

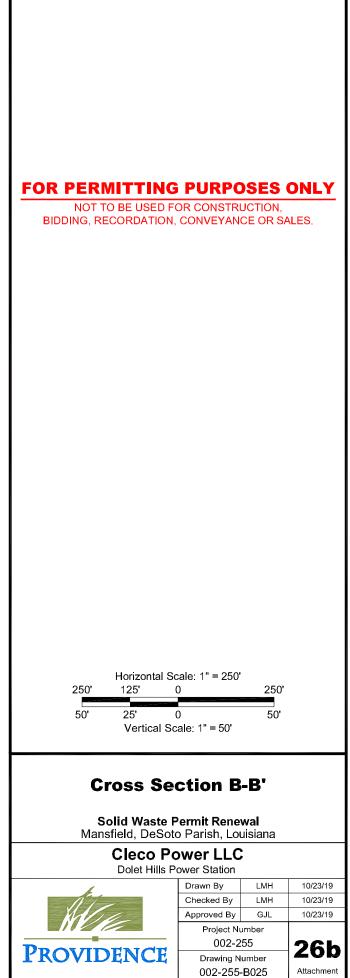
CROSS-SECTIONAL DRAWINGS SHOWING ORIGINAL CONTOURS, ELEVATIONS, DRAINAGE, LOCATION AND TYPE OF LINER, LEACHATE COLLECTION SYSTEM, AND OTHER PERTINENT FEATURES



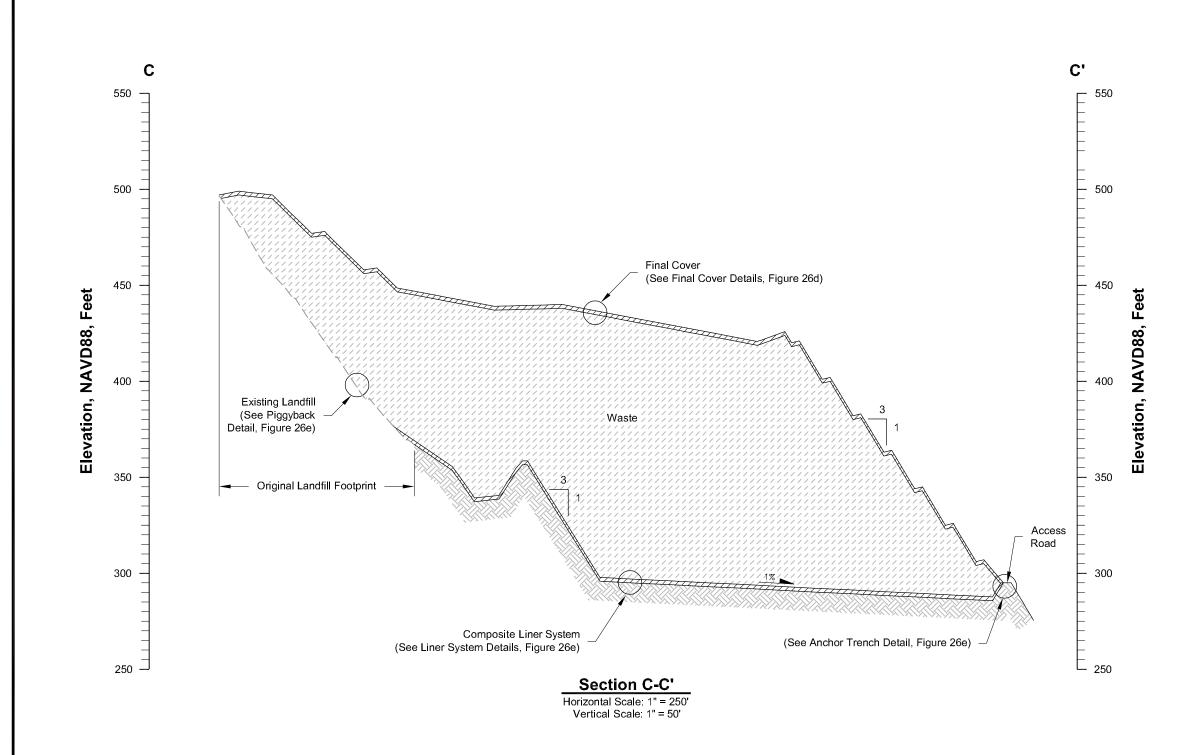


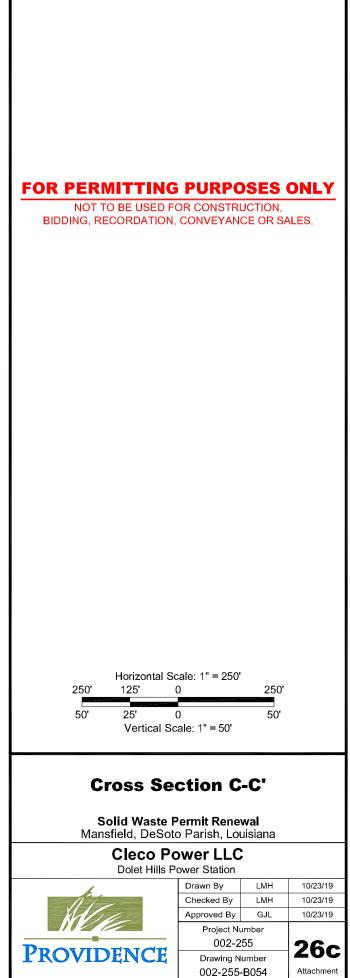
idence Engineering and Environmental Grou



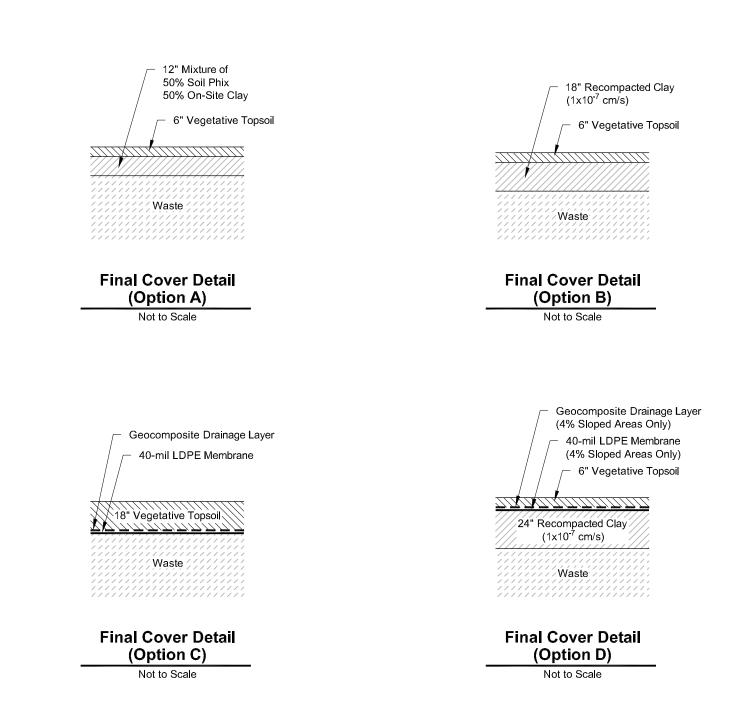


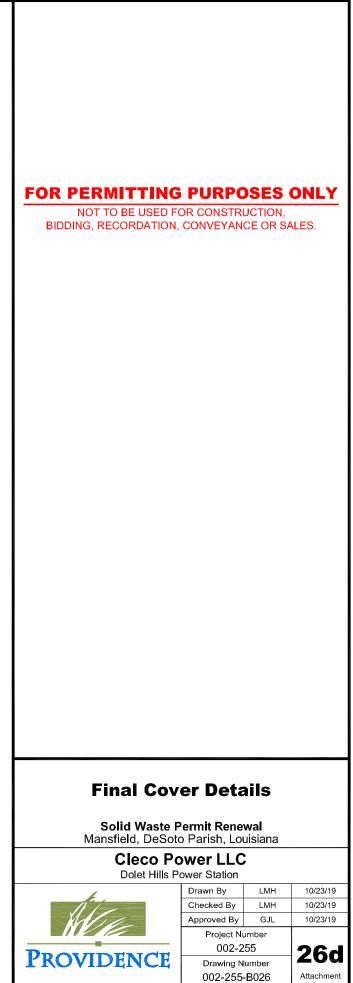
idence Engineering and Environmental Group



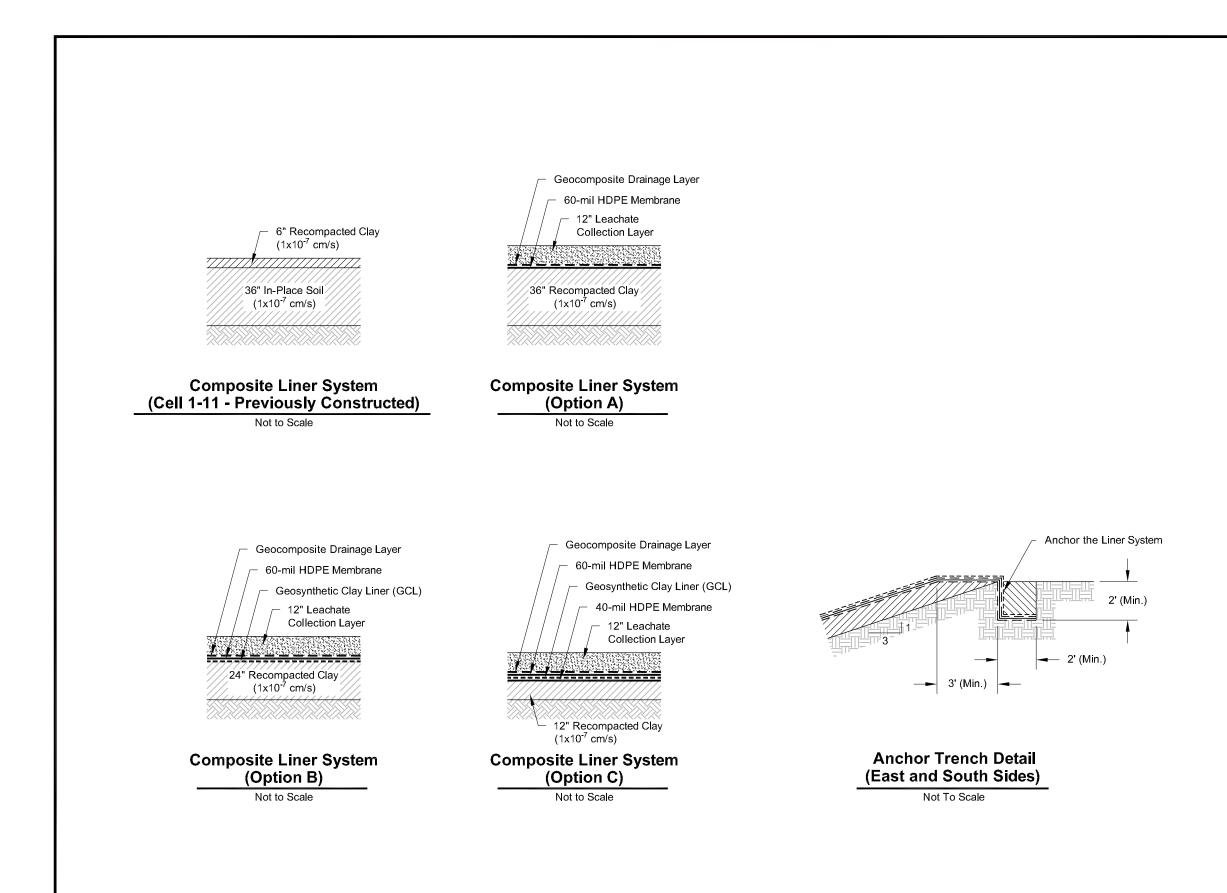


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idence Engineering and Environmental Group L



NOT TO BE USED FOR CONSTRUCTION, BIDDING, RECORDATION, CONVEYANCE OR SALES.

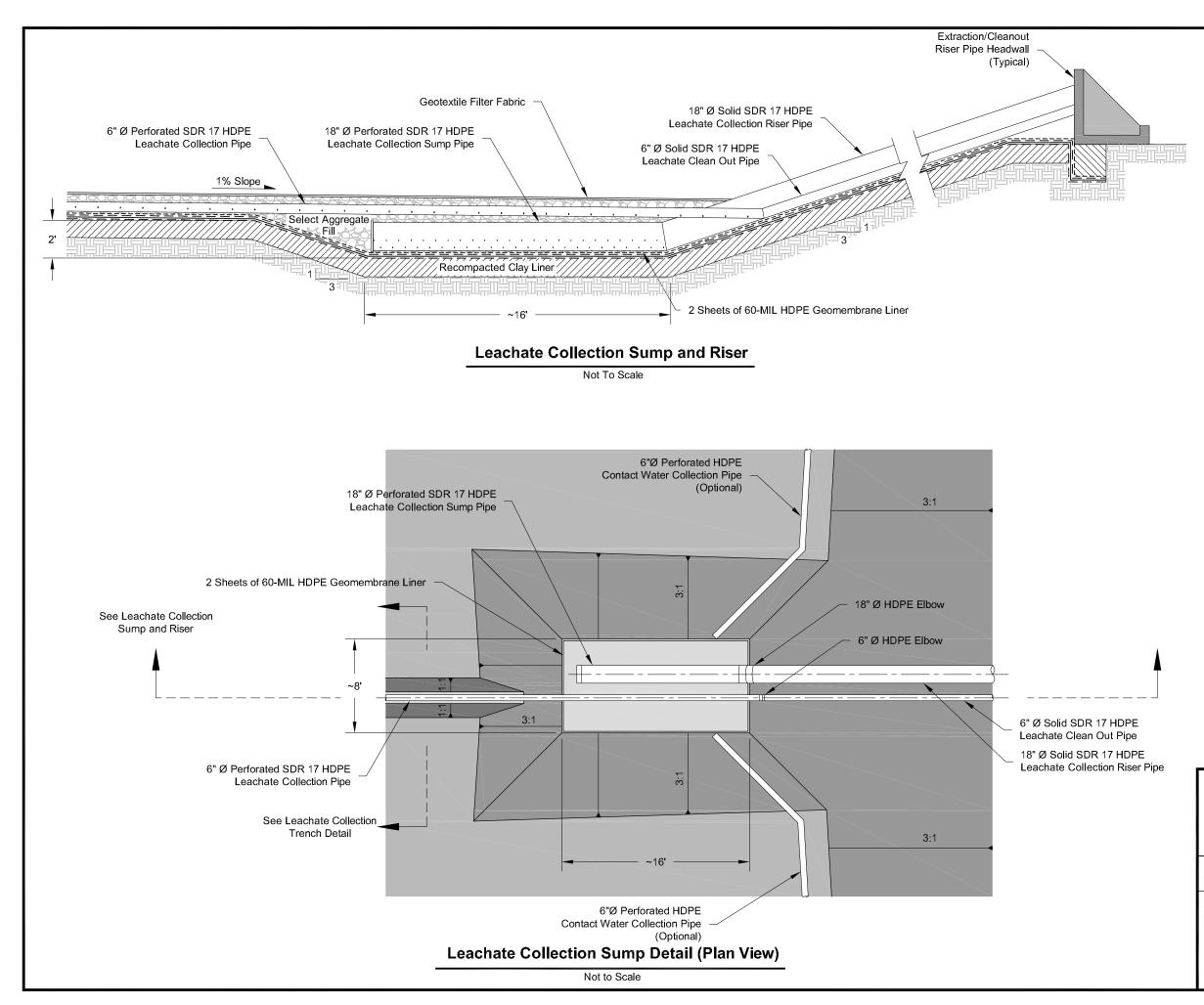
Liner	System	Details
-------	--------	---------

Solid Waste Permit Renewal Mansfield, DeSoto Parish, Louisiana

Cleco Power LLC Dolet Hills Power Station

	Drawn By	LMH	10/23/19
N	Checked By	LMH	10/23/19
No la	Approved By	GJL	10/23/19
	Project N	umber	
Decreation	002-2	255	26e
PROVIDENCE	Drawing N	umber	206
	002-255	-B027	Attachment

vidence Engineering and Environmental Group LLC



NOT TO BE USED FOR CONSTRUCTION, BIDDING, RECORDATION, CONVEYANCE OR SALES.

Leachate Collection Details

Solid Waste Permit Renewal Mansfield, DeSoto Parish, Louisiana

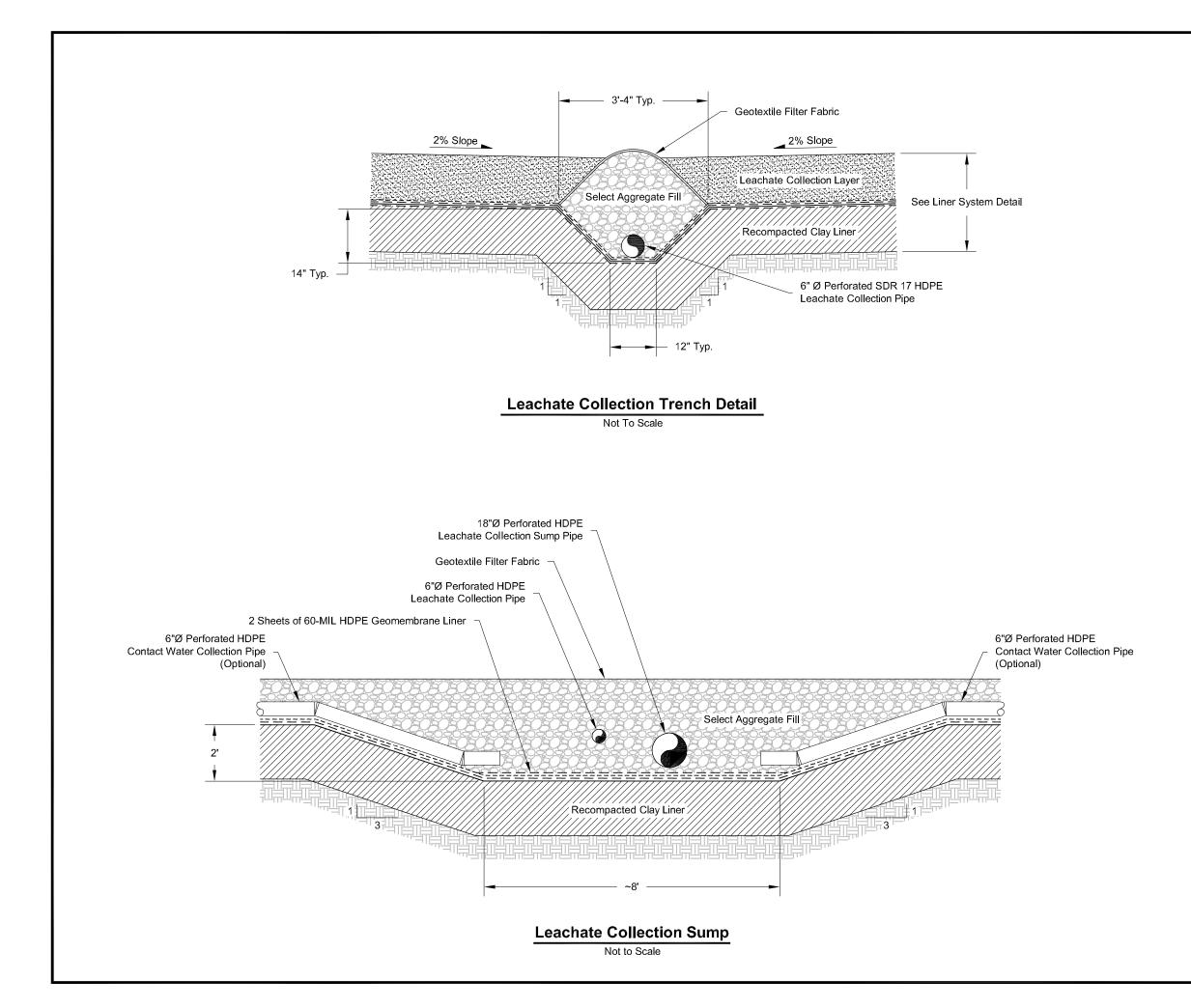
Cleco Power LLC Dolet Hills Power Station

Dolet mis r d		
	Drawn By	

PROVIDENCE

Drawn By	LMH	10/23/19
Checked By	LMH	10/23/19
Approved By	GJL	10/23/19
Project N		
002-2	26f	
Drawing N	201	
002-255-B028		Attachment

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Leachate Collection
Details

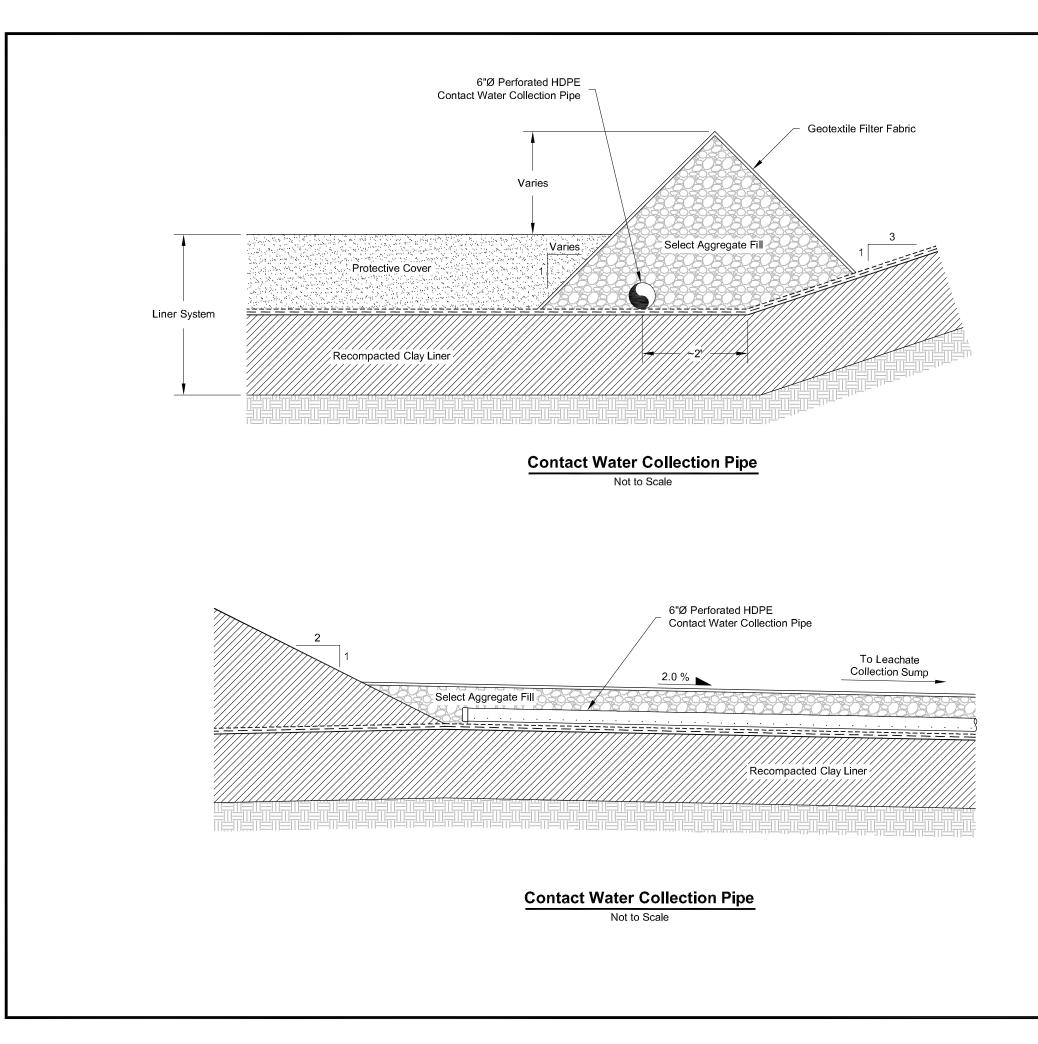
Solid Waste Permit Renewal Mansfield, DeSoto Parish, Louisiana

Cleco Power LLC Dolet Hills Power Station



5	ower Station		
	Drawn By	LMH	10/23/19
	Checked By	LMH	10/23/19
	Approved By	GJL	10/23/19
	Project N		
	002-2	26g	
	Drawing Number		209
	002-255-B029		Attachment

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Contact Water Collection Details				
Solid Waste P Mansfield, DeSoto				
Cleco Power LLC Dolet Hills Power Station				
	Drawn By	LMM	10/23/19	
N/~	Checked By	LMH	10/23/19	
XIII-	Approved By	GJL	10/23/19	
	Project N	umber		
PROVIDENCE 002-255 26h				
	002-255	-B030	Attachment	

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APPENDIX C

AS-BUILT DRAWINGS

Cleco Power LLC

Dolet Hills Power Station

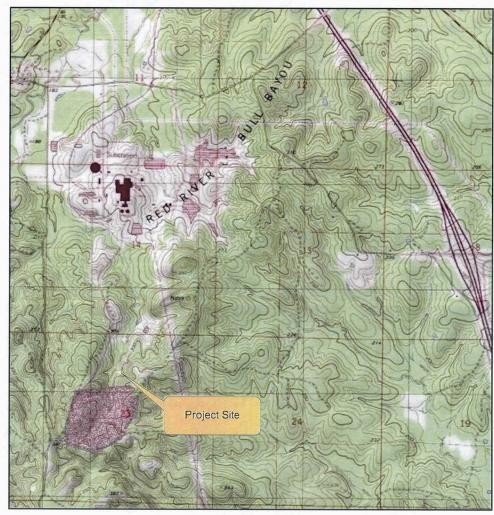
Mansfield, DeSoto Parish, Louisiana

Cell 11 As-Built Drawings

July 2016

and the second
Description Title Sheet
Subgrade Plan
Top of Clay
Details

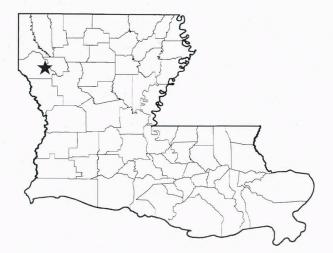
Index to Sheets

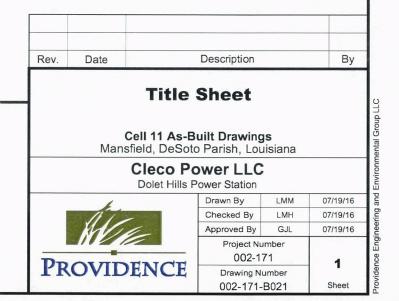


Site Location Map

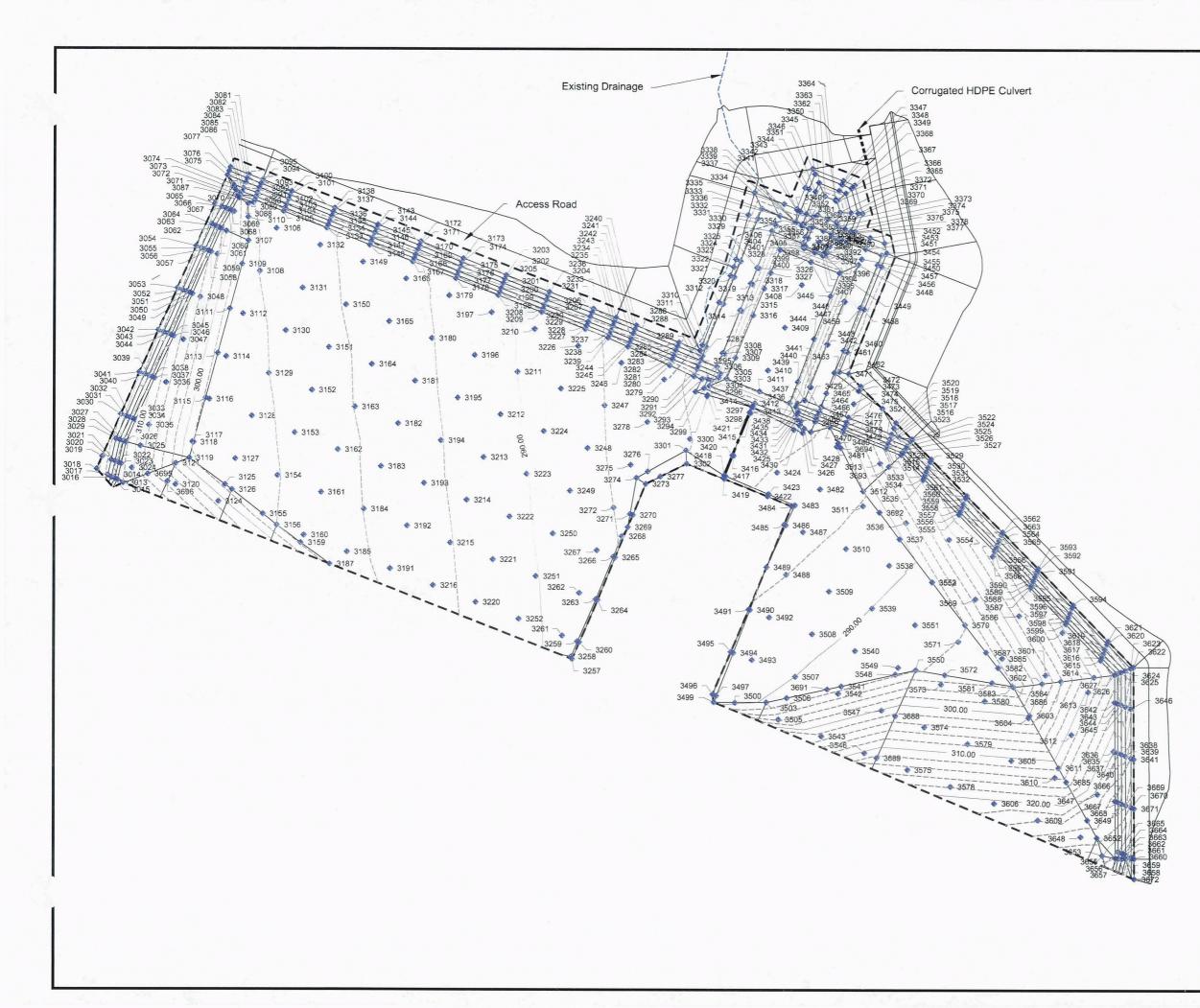
3000 3000 0 Scale: 1" = 3000'



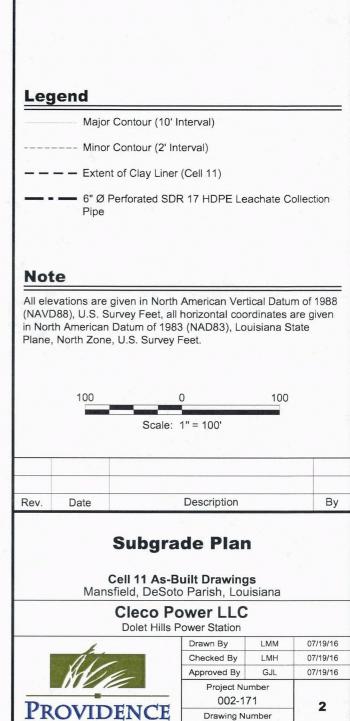




LDEQ-EDMS Document 10289846, Page 81 of 196



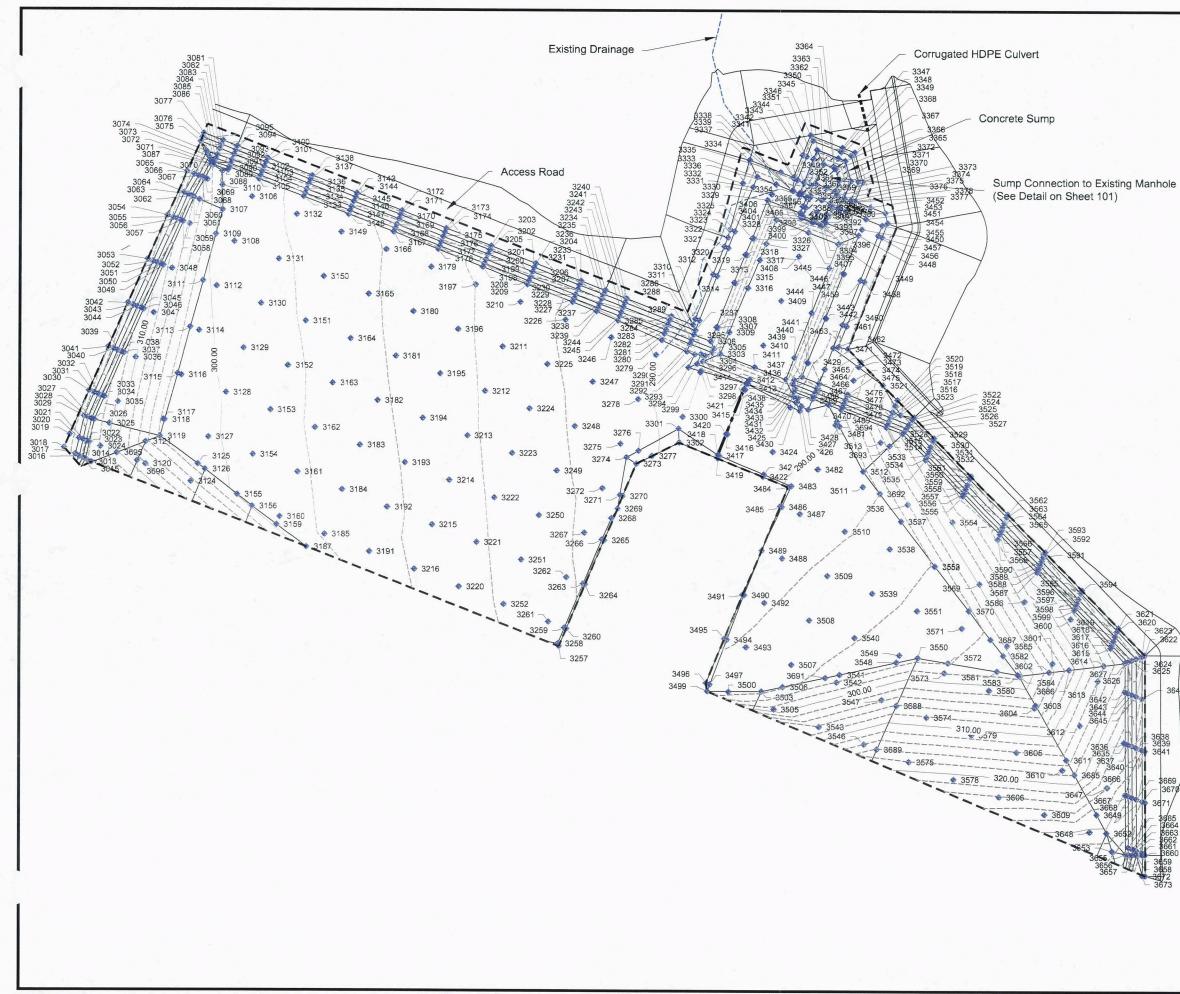
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Sheet



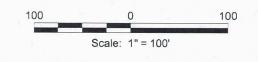


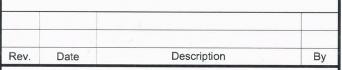
Major	Contour	(10)	Interval)
iviajoi	Contour	(10	intervary

- Minor Contour (2' Interval)
- Extent of Clay Liner (Cell 11)
 - 6" Ø Perforated SDR 17 HDPE Leachate Collection Pipe
- Concrete Sump (8" Thick)

Note

All elevations are given in North American Vertical Datum of 1988 (NAVD88), U.S. Survey Feet, all horizontal coordinates are given in North American Datum of 1983 (NAD83), Louisiana State Plane, North Zone, U.S. Survey Feet.





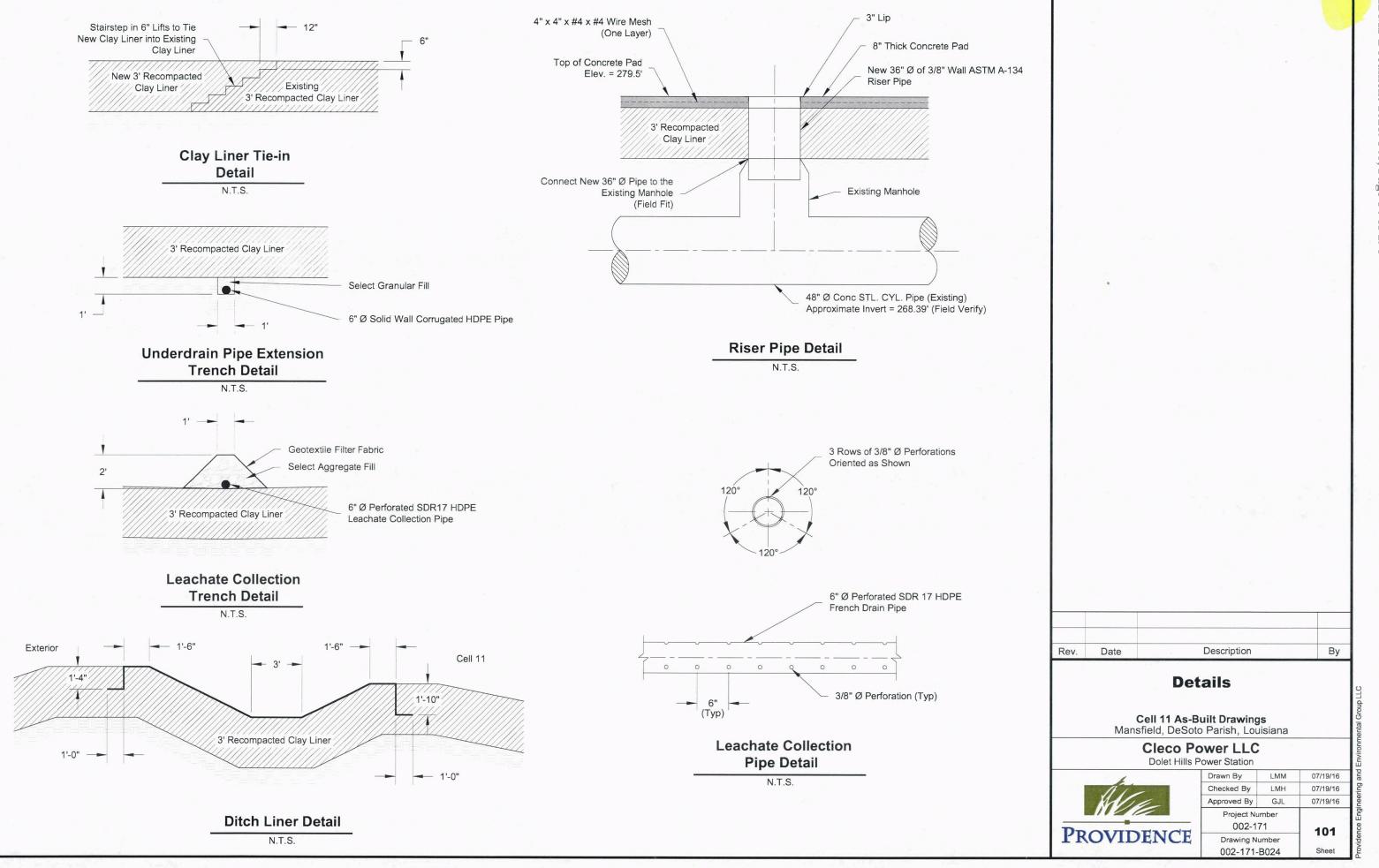
Top of Clay

Cell 11 As-Built Drawings Mansfield, DeSoto Parish, Louisiana

Cleco Power LLC Dolet Hills Power Station Drawn By LMM 07/19/16 Checked By LMH 07/19/16 Approved By GJL 07/19/16 Project Number 002-171 PROVIDENCE 3 Drawing Number

002-171-B023

Sheet



APPENDIX C – ENGINEERING CALCULATIONS

BURN	S MEDONNELL.		CLECO Corporation Run-on / Run-off Control Syste Dolet Hills BMcD Project Number : 909	
WORKSHE CREATED: PERFORM OBJECTIV	ED BY: A. MYERS	Hills Landfill kisting run-on and run-off controls	CALCULATION NO.: REVISION: REVIEWED BY:	135359 - C - 001 C J. Eichenberger
REFERENC 1	Natural Resources Conservation Service	e (June 1986). TR-55: Urban Hydro da.gov/Internet/FSE_DOCUMENT:		
2	US Department of Agriculture. (no dat			
		<u>pilsurvey.nrcs.usda.gov/app/WebS</u>		
3	National Oceanic and Atmospheric Ad (16-5874), US]. Retrieved from	ministration. (2021). NOAA Atlas 14 http://hdsc.nws.noaa.gov/hdsc/p		precipitation frequency estimates for Mansfield, LA, Station Mansfield r <u>k=la</u>
SOFTWAR	RE:			
1	Lipconceptor (Constraint) Constraint (Constraint) Constraint) Constraint (Constraint) Constraint (Constraint) Constr	www.hydrocad.net		
	Check For Update Copy to Clipboard	1 ОК		
2	Bentley® FlowMaster® V8i (SELECTseries 1)		
	Bentley Systems, Inc	Phane: +1-203-755-1666		
	27 Siemon Company Drive Ste 200W	Fax: +1-203-597-1488		
	Watertown, CT 06795 USA	Web: http://www.bentley.com Contact Technical Support		
	Registered To: User Name: Company: Serial Number: License: Commercial Is Checked Out: False Expiration Date:			
	SELECT Server Name: selectserver bentley.com Activation Key: VS-E254C09D30C24FFB881E3218 Site ID:	9676F8		
	Copyright @ 2009 Bentley Systems, Inc. All Rights F	Reserved		
	Including software, file formats, and audiovisual dis applicable software license agreement, contains co Bentley Systems. Incorporated and/or third parties secret law and may not be provided or otherwise m authorization.	plays; may only be used pursuant to infidential and proprietary information of which is protected by copyright and trade		
	TRADEMARK NOTICE			

TRADEMARK NOTICE Bentley, the "8" Bentley logo, and FlowMaster are all registered or non-registered trademarks of Bentley Systems, Incorporated. All other marks are the property of their respective owners.

ASSUMPTIONS:

1

- 1
- Reference 2 2
- 3
- DNS: Design storm is 25-yr, 24-hr (per CCR Rule) Solis (existing and cover solis) are generally fine sandy loam, Hydrologic Soil Group D CCR material in the open portion of the landfill will be modeled as Hydrologic Soil Group C Half the open landfill area will drain to western contact stormwater drainage channel and half will drain to eastern contact stormwater drainage channel. 4

MODEL INPUTS (see also HydroCAD report):

	Ingulocable	sport).		
Establish rainfall data (assume SCS Type III distribution)				
	SCS Storm	Depth (in)		
	25yr, 24hr	8.16	Reference 3	

Input CN data - see SK-CIVIL-002 in Appendix A for land cover assumptions 2

			Area (ac)	
Land Description	CN	Landfill	Runoff Pond	Outside Runoff
Open space, poor condition (ash)	86	31.207		
Open space, good condition (pasture)	80	10.722		
Open space, fair condition (pasture)	84		2.726	2.007
Impervious	98	1.528	3.003	
Gravel Road	96	0.146		
Dirt Road/Bare Soil	94	0.543		
Woods, good condition	77		1.988	2.017
		44.145	7.717	4.024

BURNS MEDONNELL

3

Input pond volume data

Cell 11 Sedimentation Pond							
EL	area* (ac)						
280	0.247						
282	0.289 0.334						
284							
286	0.383						
288	0.434						
*measured in Microstation,							
estimated based on as-built							
drawing.							

Cell 11 Overflow Sump							
EL	area* (sf)						
268.37	7						
279.5	7						
280	603						
285	2,311						
286 2,705							
*measured in Microstation, estimated based on as-built drawing.							

Runoff Pond						
EL	area* (ac)					
250	0.832					
252	1.016					
254	1.219					
256	1.434					
258	1.661					
260	1.898					
261	2.259					
262	2.652					
264	3.003 3.334					
266						
268	3.716					
270	4.143					
272	4.396					
273 4.525						
*measured in Microstation, elevations below the LiDAR water surface elevation were estimated by offsetting contours at 3H:1V.						

CLECO Corporation Run-on / Run-off Control System Plan Dolet Hills BMcD Project Number : 90965

RESULTS (see also HydroCAD report):

Subcatchment	Weighted CN	Runoff Depth (in)	Peak Runoff (cfs)
1S: Landfill	85	6.37	233.81
2S: Runoff Pond	88	6.72	44.99
3S: Outside Runoff	80	5.78	25.38

Pond	Initial EL (ft)	Peak Elevation (ft)	Peak Inflow (cfs)	Peak Discharge (cfs)	Peak Storage (ac-ft)
2P: Cell 11 Sedimentation Pond	286.00	287.81	233.81	229.92	2.721
3P: Cell 11 Overflow Sump	N/A	285.19	229.92	217.41	0.183
4P: Runoff Pond	259.00	268.52	253.91	0.00	38.913

CONCLUSION:

Under the modeled conditions, the landfill ponds can accept and control inflows from the design flood event without overtopping.

CHECK DITCH CAPACITIES

Use FlowMaster to determine velocity in the channels using HEC-HMS calculated peak discharge, above. Minimum channel depth is 2ft. Contact Stormwater Run-off: Assume a trapezoidal channel with roughness coefficient of 0.012 (geomembrane liner), channel slope 1%, bottom width of 8ft, and 3:1 side slopes. Non-Contact Stormwater Run-off: Assume a triangular channel with roughness coefficient of 0.025 (earth, clean and winding), channel slope 2%, and 3:1 side slopes.

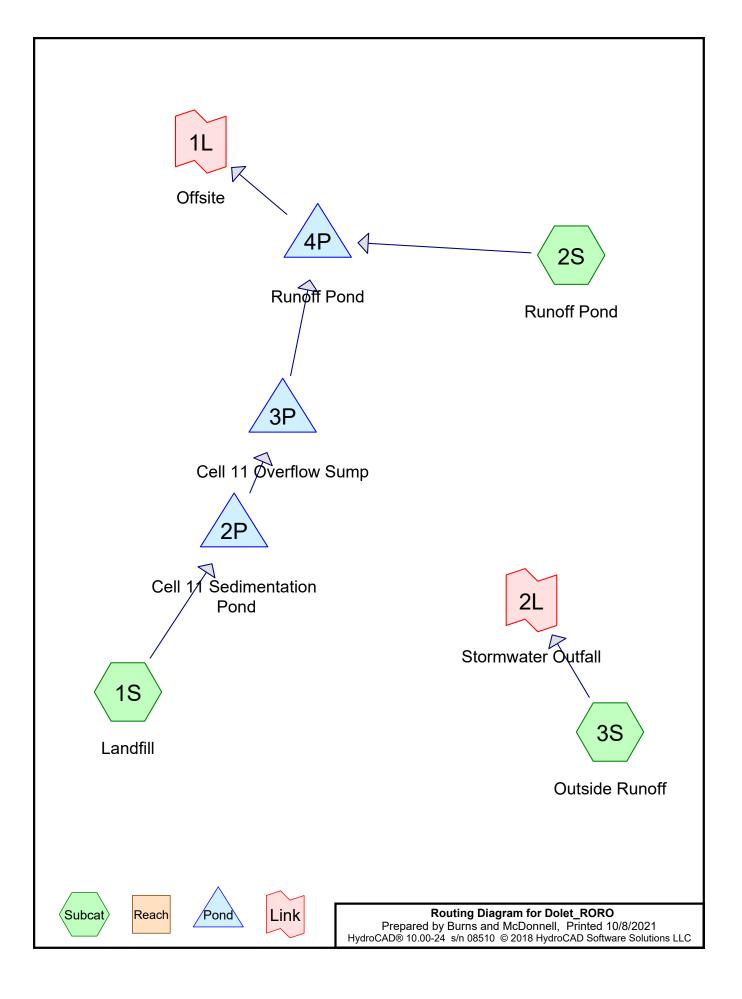
RESULTS:

1

Component	Discharge (cfs)	Normal Depth (ft)	Channel Velocity (ft/s)
Contact Stormwater Run-off 1/2 Landfill (Open)	116.91	1.02	10.46
Non-Contact Stormwater Run-off Outside Run-off	25.38	1.21	5.80

CONCLUSION:

Under the modeled conditions, the landfill diversion ditches can accept and control inflows from the design flood event without overtopping.



Area Listing (all nodes)

Area	CN	Description	
(acres)		(subcatchment-numbers)	
4.733	84	50-75% Grass cover, Fair, HSG D (2S, 3S)	
10.722	80	>75% Grass cover, Good, HSG D (1S)	
31.207	86	Ash (1S)	
0.543	94	Dirt road/bare soil, HSG D (1S)	
0.146	96	Gravel surface, HSG D (1S)	
4.531	98	Impervious (1S, 2S)	
4.005	77	Woods, Good, HSG D (2S, 3S)	

Dolet_RORO	Type III 24-hr 25-yr, 24-hr Rainfall=8.16"
Prepared by Burns and McDonnell	Printed 10/8/2021
HydroCAD® 10.00-24 s/n 08510 © 2018 HydroCAD Software S	Solutions LLC Page 3

Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Landfill	Runoff Area=44.146 ac 3.46% Impervious Runoff Depth=6.37" w Length=2,506' Tc=16.2 min CN=85 Runoff=233.81 cfs 23.426 af
Subcatchment 2S: Runoff Pond	Runoff Area=7.717 ac 38.91% Impervious Runoff Depth=6.72" Flow Length=880' Tc=13.7 min CN=88 Runoff=44.99 cfs 4.325 af
Subcatchment 3S: Outside Runoff Flow Length=1,3	Runoff Area=4.024 ac 0.00% Impervious Runoff Depth=5.78" 90' Slope=0.0200 '/' Tc=7.2 min CN=80 Runoff=25.38 cfs 1.937 af
Pond 2P: Cell 11 Sedimentation Pond	Peak Elev=287.81' Storage=2.721 af Inflow=233.81 cfs 23.426 af Outflow=229.92 cfs 23.038 af
Pond 3P: Cell 11 Overflow Sump 48.0" Round	Peak Elev=285.19' Storage=7,972 cf Inflow=229.92 cfs 23.038 af Culvert n=0.012 L=460.0' S=0.0069 '/' Outflow=217.41 cfs 23.038 af
Pond 4P: Runoff Pond	Peak Elev=268.52' Storage=38.913 af Inflow=253.91 cfs 27.362 af Outflow=0.00 cfs 0.000 af
Link 1L: Offsite	Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af
Link 2L: Stormwater Outfall	Inflow=25.38 cfs 1.937 af Primary=25.38 cfs 1.937 af

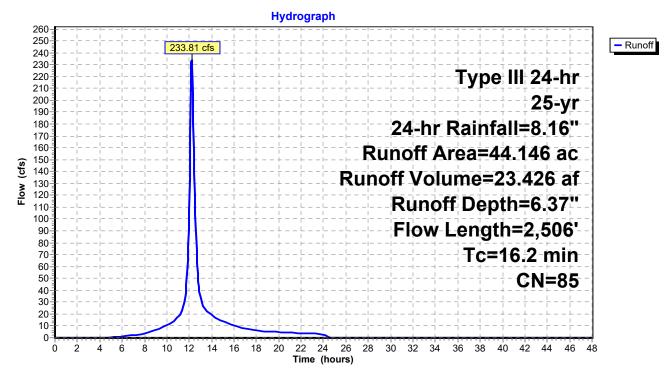
Summary for Subcatchment 1S: Landfill

Runoff = 233.81 cfs @ 12.22 hrs, Volume= 23.426 af, Depth= 6.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 25-yr, 24-hr Rainfall=8.16"

	Area	(ac)	CN Des	cription		
*	31.	207	86 Ash			
	10.	722	80 >75	% Grass co	over, Good,	, HSG D
*	1.	528		ervious		
	0.	146	96 Grav	vel surface	, HSG D	
*	0.	543	94 Dirt	road/bare :	soil, HSG D)
	44.	146	85 Wei	ghted Aver	ade	
		618		4% Pervio		
		528	3.46	% Impervi	ous Area	
				•		
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	1.2	31	0.0285	0.44		Sheet Flow,
						Fallow n= 0.050 P2= 4.39"
	1.7	169	0.3333	1.64		Sheet Flow,
						Fallow n= 0.050 P2= 4.39"
	1.3	457	0.3333	5.77		Shallow Concentrated Flow,
						Nearly Bare & Untilled Kv= 10.0 fps
	9.1	643	0.0140	1.18		Shallow Concentrated Flow,
						Nearly Bare & Untilled Kv= 10.0 fps
	2.9	1,206	0.0100	7.01	33.28	Trap/Vee/Rect Channel Flow,
						Bot.W=8.00' D=0.50' Z= 3.0 '/' Top.W=11.00'
						n= 0.012
	16.2	2,506	Total			

Subcatchment 1S: Landfill



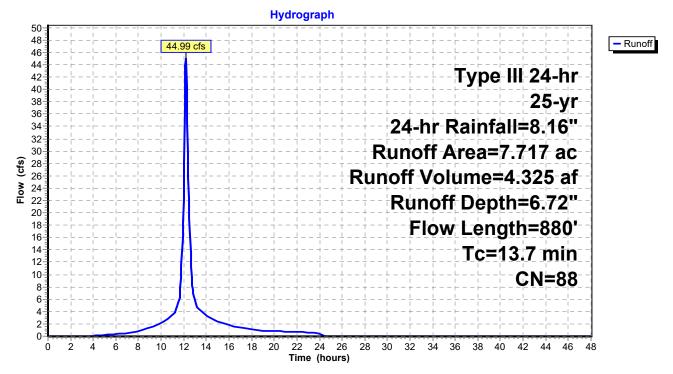
Summary for Subcatchment 2S: Runoff Pond

Runoff = 44.99 cfs @ 12.18 hrs, Volume= 4.325 af, Depth= 6.72"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 25-yr, 24-hr Rainfall=8.16"

_	Area	(ac) (N Des	cription		
	2.	726	84 50-7	5% Grass	cover, Fair	, HSG D
	1.	988	77 Woo	ds, Good,	HSG D	
*	3.	003	98 Impe	ervious		
_	7.	717	88 Weig	ghted Aver	age	
	4.	714	61.0	9% Pervio	us Area	
	3.	003	38.9	1% Imperv	/ious Area	
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	9.7	300	0.1250	0.52		Sheet Flow,
						Grass: Short n= 0.150 P2= 4.39"
	3.2	425	0.2000	2.24		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.8	155	0.2000	3.13		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	13.7	880	Total			

Subcatchment 2S: Runoff Pond



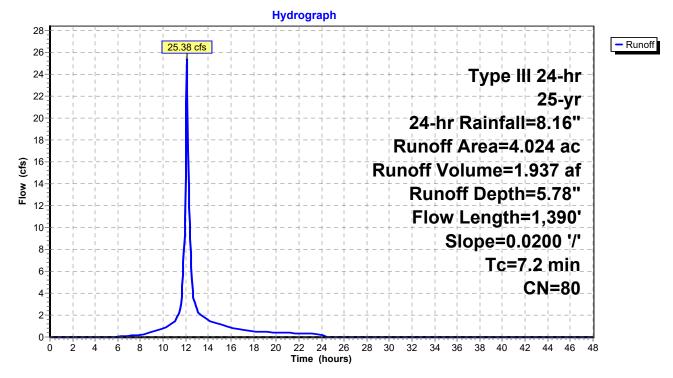
Summary for Subcatchment 3S: Outside Runoff

25.38 cfs @ 12.10 hrs, Volume= 1.937 af, Depth= 5.78" Runoff =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 25-yr, 24-hr Rainfall=8.16"

A	rea ((ac) C	N Des	scription		
	2.0	007	84 50-	75% Grass	cover, Fair	, HSG D
	2.0	017	77 Wo	ods, Good,	HSG D	
	4.(024	80 We	ighted Avei	age	
	4.(024	100	.00% Perv	ous Area	
	Та	Longth	Clana	Valacity	Conocity	Description
	Tc iin)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
	7.2	1,390	0.0200	3.22	2.42	Trap/Vee/Rect Channel Flow,
						Bot.W=0.00' D=0.50' Z= 3.0 '/' Top.W=3.00'
						n= 0.025 Earth, clean & winding

Subcatchment 3S: Outside Runoff



Summary for Pond 2P: Cell 11 Sedimentation Pond

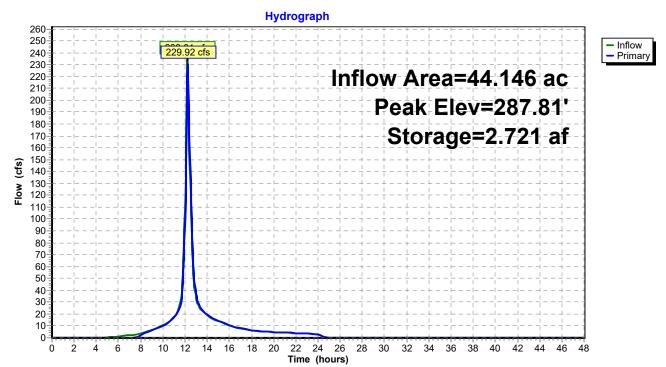
Inflow Area =	44.146 ac,	3.46% Impervious,	Inflow Depth = 6.3	37" for 25-yr, 24-hr event
Inflow =	233.81 cfs @	12.22 hrs, Volume=	= 23.426 af	
Outflow =	229.92 cfs @	12.25 hrs, Volume=	= 23.038 af,	Atten= 2%, Lag= 1.9 min
Primary =	229.92 cfs @	12.25 hrs, Volume=	= 23.038 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Starting Elev= 285.00' Surf.Area= 0.370 ac Storage= 1.511 af Peak Elev= 287.81' @ 12.25 hrs Surf.Area= 0.499 ac Storage= 2.721 af (1.210 af above start) Flood Elev= 288.00' Surf.Area= 0.509 ac Storage= 2.814 af (1.303 af above start)

Plug-Flow detention time= 71.7 min calculated for 21.527 af (92% of inflow) Center-of-Mass det. time= 12.4 min (811.6 - 799.3)

Volume	Invert	Avail.	Storage	Storage Des	cription	
#1	280.00'		3.832 af	Custom Stag	ge Data	(Prismatic)Listed below (Recalc)
- 1	0(A	la 01	0	0	
Elevatio		Area	Inc.Sto		Store	
(fee	t) (ad	cres)	(acre-fe	et) (acre	<u>e-feet)</u>	
280.0	0 0	.247	0.0	00	0.000	
282.0	0 0	.289	0.5	36	0.536	
284.0	0 0	.334	0.6	23	1.159	
286.0	0 0	.406	0.7	40	1.899	
288.0	0 0	.509	0.9	15	2.814	
290.0	0 0	.509	1.0	18	3.832	
Device	Routing	Inv	vert Out	et Devices		
#1	Primary	286	Hea	tom Weir/Or d (feet) 0.00 th (feet) 20.0	2.00	v= 2.62 (C= 3.28)

Primary OutFlow Max=229.33 cfs @ 12.25 hrs HW=287.81' TW=284.39' (Dynamic Tailwater) -1=Custom Weir/Orifice (Weir Controls 229.33 cfs @ 4.10 fps)



Pond 2P: Cell 11 Sedimentation Pond

Summary for Pond 3P: Cell 11 Overflow Sump

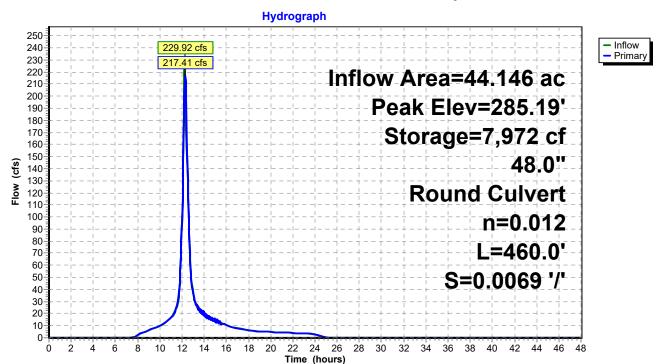
Inflow Area	=	44.146 ac,	3.46% Impervious, In	nflow Depth = 6.	26" for 25-yr, 24-hr event
Inflow =	=	229.92 cfs @	12.25 hrs, Volume=	23.038 af	-
Outflow =	=	217.41 cfs @	12.30 hrs, Volume=	23.038 af,	Atten= 5%, Lag= 3.2 min
Primary =	=	217.41 cfs @	12.30 hrs, Volume=	23.038 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 285.19' @ 12.30 hrs Surf.Area= 2,388 sf Storage= 7,972 cf Flood Elev= 286.00' Surf.Area= 2,705 sf Storage= 10,023 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 0.1 min (811.7 - 811.6)

Volume	Inve	ert Avail.Sto	rage Stora	ge Description	
#1	268.3	39' 10,02	23 cf Custo	om Stage Data (P	rismatic)Listed below (Recalc)
Elevatio (feet		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
268.3	9	7	0	0	
279.5	0	7	78	78	
280.0	0	603	153	230	
285.0	0	2,311	7,285	7,515	
286.0	0	2,705	2,508	10,023	
-	Routing	Invert	Outlet Devi		
#1	Primary	268.39'	L= 460.0' Inlet / Outle	et Invert= 268.39"/	e headwall, Ke= 0.500 265.21' S= 0.0069 '/' Cc= 0.900
Brimony	OutElow	Mov-217 41 of			hed, Flow Area= 12.57 sf $N=262, 70^{\circ}$ (Dynamic Tailwater)

Primary OutFlow Max=217.41 cfs @ 12.30 hrs HW=285.19' TW=263.70' (Dynamic Tailwater) -1=Culvert (Barrel Controls 217.41 cfs @ 17.30 fps)



Pond 3P: Cell 11 Overflow Sump

Summary for Pond 4P: Runoff Pond

Inflow Are	a =	51.863 ac,	8.74% Impervious, Inflow	Depth = 6.33" for 25-yr, 24-hr event
Inflow	=	253.91 cfs @	12.27 hrs, Volume=	27.362 af
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atten= 100%, Lag= 0.0 min
Primary	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af

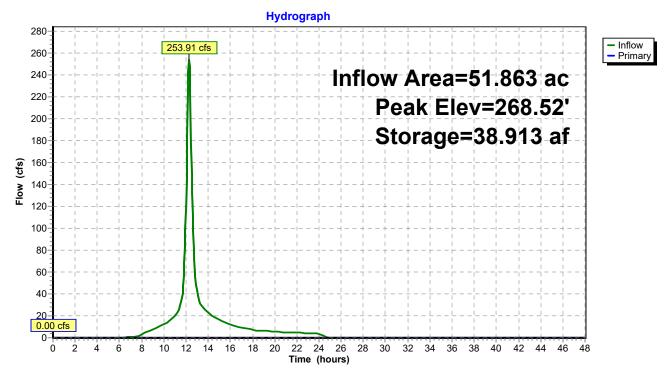
Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Starting Elev= 259.00' Surf.Area= 1.780 ac Storage= 11.551 af Peak Elev= 268.52' @ 48.00 hrs Surf.Area= 3.826 ac Storage= 38.913 af (27.362 af above start) Flood Elev= 273.00' Surf.Area= 4.525 ac Storage= 57.824 af (46.273 af above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no outflow)

Invert Av	ail.Storage	Storage	Description	
250.00'	57.824 af	Custom	Stage Data (Prismatic)Listed below (Recalc)
			-	
Surf.Area				
(acres)	(acre-f	eet)	<u>acre-feet)</u>	
0.832	0.	000	0.000	
1.016	1.	848	1.848	
1.219	2.	235	4.083	
1.434	2.	653	6.736	
1.661	3.	095	9.831	
1.898	3.	559	13.390	
2.259	2.	078	15.468	
2.652	2.	455	17.924	
3.003	5.	655	23.579	
3.334	6.	337	29.916	
3.716	7.	050	36.966	
4.143	7.	859	44.825	
4.396	8.	539	53.364	
4.525	4.	460	57.824	
outing	Invert Ou	Itlet Devic	S	
rimary 2	270.00' C ι	istom We	/Orifice, Cv= 2.62 (C=	3.28)
		, ,		
	250.00' Surf.Area (acres) 0.832 1.016 1.219 1.434 1.661 1.898 2.259 2.652 3.003 3.334 3.716 4.143 4.396 4.525 outing	250.00' 57.824 af Surf.Area Inc.Si (acres) (acre-fe 0.832 0.1 1.016 1.1 1.219 2.1 1.434 2.1 1.661 3.1 1.898 3.1 2.652 2.1 3.003 5.1 3.716 7.1 4.143 7.1 4.525 4.1 outing Invert Outing Invert Outing Invert Outing	250.00' 57.824 af Custom s Surf.Area Inc.Store C (acres) (acre-feet) (a 0.832 0.000 1.016 1.848 1.219 2.235 1.434 2.653 1.661 3.095 1.898 3.559 2.259 2.078 2.652 2.455 3.003 5.655 3.334 6.337 3.716 7.050 4.143 7.859 4.396 8.539 4.525 4.460 outing Invert Outlet Device Custom Weir rimary 270.00' Custom Weir Head (feet) 0	250.00' 57.824 af Custom Stage Data (Prismatic Surf.Area (acres) Inc.Store (acre-feet) Cum.Store (acre-feet) 0.832 0.000 0.000 1.016 1.848 1.848 1.219 2.235 4.083 1.434 2.653 6.736 1.661 3.095 9.831 1.898 3.559 13.390 2.259 2.078 15.468 2.652 2.455 17.924 3.003 5.655 23.579 3.334 6.337 29.916 3.716 7.050 36.966 4.143 7.859 44.825 4.396 8.539 53.364 4.525 4.460 57.824

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=259.00' TW=0.00' (Dynamic Tailwater)

Pond 4P: Runoff Pond

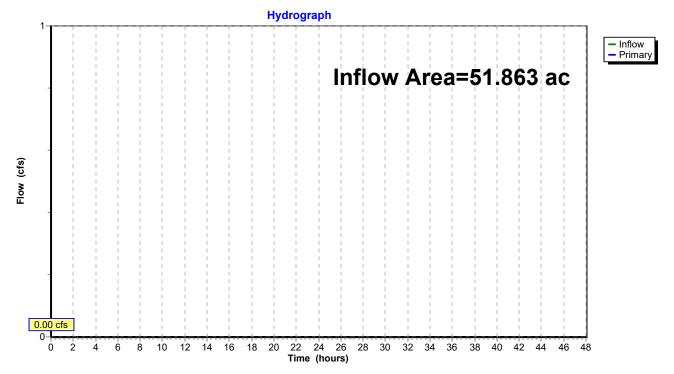


Summary for Link 1L: Offsite

Inflow Are	a =	51.863 ac,	8.74% Impervious, Inflow E	Depth = 0.00"	for 25-yr, 24-hr event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af	
Primary	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atte	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Link 1L: Offsite

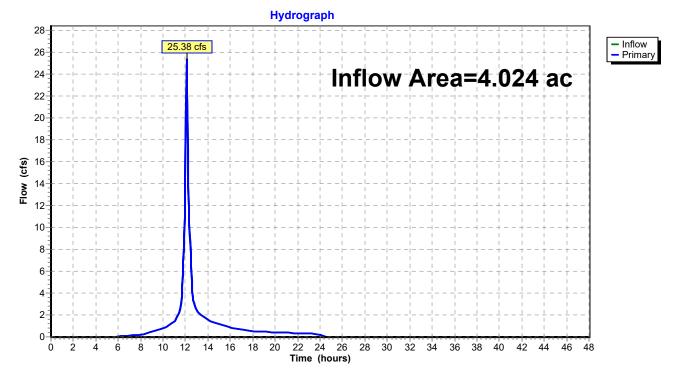


Summary for Link 2L: Stormwater Outfall

Inflow Are	a =	4.024 ac,	0.00% Impervious, Inflow E	Depth = 5.78"	for 25-yr, 24-hr event
Inflow	=	25.38 cfs @	12.10 hrs, Volume=	1.937 af	
Primary	=	25.38 cfs @	12.10 hrs, Volume=	1.937 af, Atte	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Link 2L: Stormwater Outfall



Project Description		
Friction Method	Manning Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.012	
Channel Slope	0.010	
Left Side Slope	3.000	
Right Side Slope	3.000	
Bottom Width	8.00	
Discharge	116.91	
Results		
Normal Depth	12.2	
Flow Area	11.2	
Wetted Perimeter	14.4	
Hydraulic Radius	9.3	
Top Width	14.08	
Critical Depth	18.5	
Critical Slope	0.002	
Velocity	10.46	
Velocity Head	1.70	
Specific Energy	2.71	
Froude Number	2.068	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0	
Length	0.0	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0	
Profile Description	N/A	
Profile Headloss	0.00	
Downstream Velocity	Infinity	
Upstream Velocity	Infinity	
Normal Depth	12.2	
Critical Depth	18.5	
Channel Slope	0.010	
Critical Slope	0.002	

Worksheet for Landfill Runoff - Trapezoidal Channel

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.025
Channel Slope	0.020
Left Side Slope	3.000
Right Side Slope	3.000
Discharge	25.38
Results	
Normal Depth	14.5
Flow Area	4.4
Wetted Perimeter	7.6
Hydraulic Radius	6.9
Top Width	7.25
Critical Depth	16.2
Critical Slope	0.011
Velocity	5.80
Velocity Head	0.52
Specific Energy	1.73
Froude Number	1.315
Flow Type	Supercritical
GVF Input Data	
Downstream Depth	0.0
Length	0.0
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0
Profile Description	N/A
Profile Headloss	0.00
Downstream Velocity	Infinity
Upstream Velocity	Infinity
Normal Depth	14.5
Critical Depth	16.2
Channel Slope	0.020
Critical Slope	0.011

Worksheet for Outside Runoff - Triangular Channel





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