

History of Construction Dolet Hills Ash Basin 2



CLECO Corporation

Dolet Hills Power Station Project No. 90965

Revision 0 10/13/2016

History of Construction Dolet Hills Ash Basin 2

prepared for

CLECO Corporation
Dolet Hills Power Station
DeSoto Parish, Louisiana

Project No. 90965

Revision 0 10/13/2016

prepared by

Burns & McDonnell Engineering Company, Inc. Kansas City, Missouri

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INDEX AND CERTIFICATION

CLECO Corporation History of Construction Dolet Hills Ash Basin 2 Project No. 90965

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Certification

I hereby certify, as a Professional Engineer in the state of Louisiana, that the information in this document was assembled under my direct personal charge. This report is not intended or represented to be suitable for reuse by the CLECO Corporation or others without specific verification or adaptation by the Engineer.

Randell L Sedlacek, P.E. Louisiana License #38408

Date: 6/13/16

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LIST OF ABBREVIATIONS

Abbreviation <u>Term/Phrase/Name</u>

BMcD Burns & McDonnell

CCR Coal Combustion Residual

CFR Code of Federal Regulations

CLECO Corporation

CY Cubic Yards

Dolet Hills Power Station

EPA Environmental Protection Agency

GPM Gallons per Minute

HUC Hydrologic Unit Code

LSU Louisiana State University

U.S.C United States Code

USGS United States Geological Survey

1.0 INTRODUCTION

On April 17, 2015, the Environmental Protection Agency (EPA) issued the final version of the federal Coal Combustion Residual (CCR) Rule to regulate the disposal of CCR materials generated at coal-fired units. The rule will be administered as part of the Resource Conservation and Recovery Act [RCRA, 42 United States Code (U.S.C.) §6901 et seq.], using the Subtitle D approach.

The existing CCR units at CLECO Corporation's (CLECO's) Dolet Hills Power Station (Dolet Hills) are subject to the CCR Rule, and as such CLECO must compile a History of Construction for each of the units per 40 CFR §257.73(c). This report serves as the History of Construction for Ash Basin 2 at Dolet Hills.

This history of construction is in addition to, not in place of, any other applicable site permits, environmental standards, or work safety practices.

2.0 PLAN OBJECTIVES

Per 40 CFR §257.73(c), the History of Construction must contain, to the extent feasible, the following items:

- The name and address of the owner/operator of the CCR unit, the name of the CCR unit, and the identification number of the CCR unit
- The location of the CCR unit on most recent United States Geological Survey (USGS) 7½ minute or 15 minute topographical map
- A statement of the purpose for which the CCR unit is being used
- The name and size of watershed within which the CCR unit is located
- A description of the physical and engineering properties of the foundation and abutment materials on which the CCR unit is constructed
- A statement of the type, size, range, and physical and engineering properties of the materials used
 in constructing each zone or stage of the CCR unit; the method of site preparation and
 construction of each zone or stage of the CCR unit; and the approximate dates of construction of
 each successive stage of construction of the CCR unit.
- Detailed dimensional drawings of the CCR Unit, including the following:
 - o Plan view and cross sections of the length and width of the CCR unit
 - o Foundation improvements
 - o Drainage provisions, spillways, diversion ditches, outlets
 - Instrumentation locations
 - o Slope protection
 - o Normal operating pool surface elevation
 - o Maximum pool surface elevation following peak discharge from the inflow design flood
 - o Expected maximum depth of CCR within the unit
 - Any identifiable natural or manmade features that could adversely affect operation of the
 CCR unit due to malfunction or mis-operation
- A description of the type, purpose, and location of existing instrumentation
- Area-capacity curves for the CCR unit
- A description of each spillway and diversion design features and capacities and calculations used in their determination
- The construction specifications and provisions for surveillance, maintenance, and repair of the CCR unit
- Any record or knowledge of structural instability of the CCR unit.

History of Construction

History of Construction

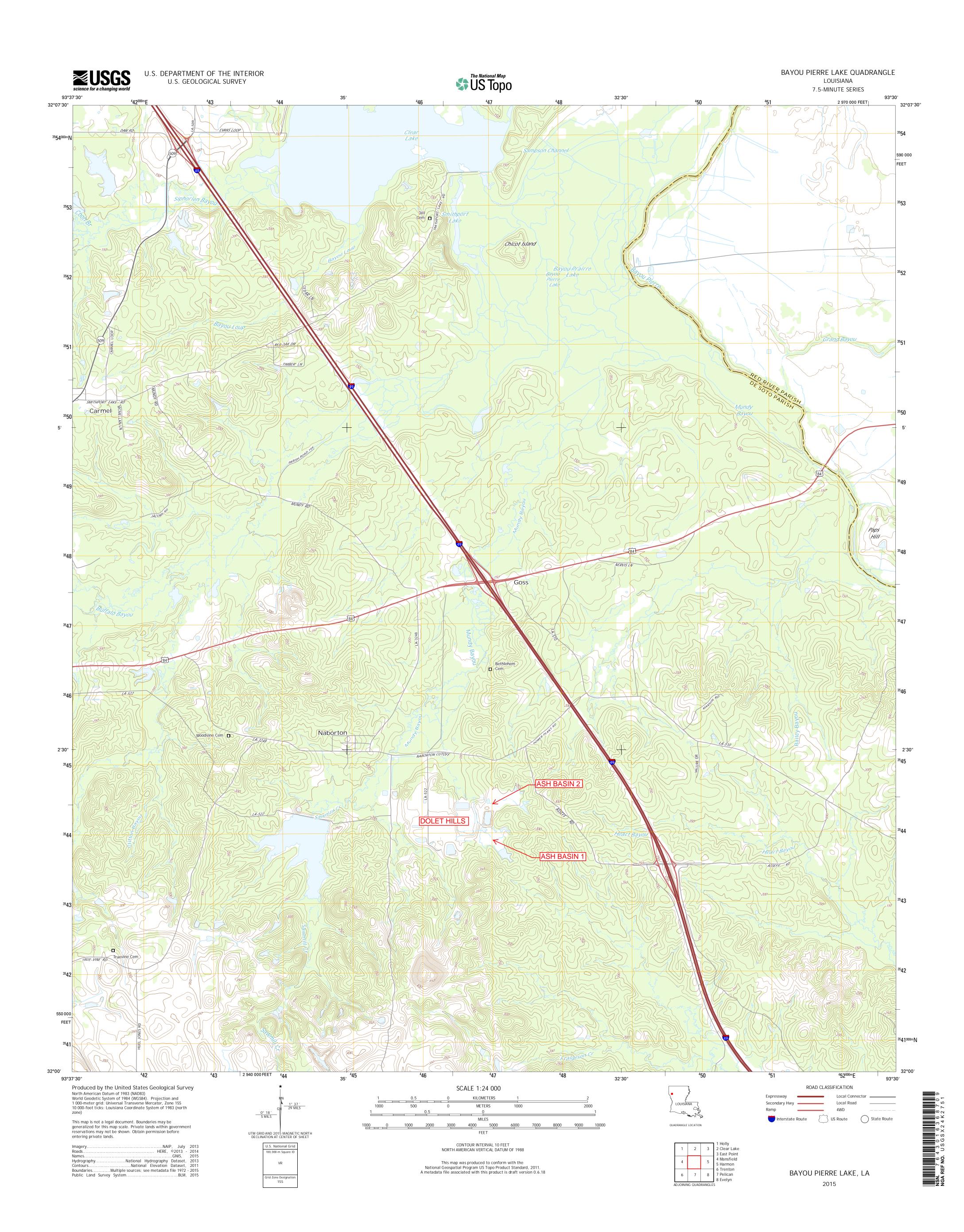
3.0 HISTORY OF CONSTRUCTION

Section		CCR Rule Description	Included	Information	Source
40 CFR §257.73 (c)(1)	(i)	Name and address of the owner/operator of the CCR unit		Cleco Corporation	Owner
			Υ	2030 Donahue Ferry Road	
				P.O. Box 5000	
		Name of the CCR units	Υ	Pineville, LA 71361-5000 Ash Basin 2	Owner
		Identification number of the CCR unit	Y	P-0037 (permit number)	Owner
40 CFR §257.73 (c)(1)	(ii)	Location of the CCR unit on most recent United States		See Appendix A	USGS Map
	()	Geological Survey (USGS) 7½ minute or 15 minute	Y	occ / (ppolicility /	o o o o i i ap
		topographical map			
40 CFR §257.73 (c)(1)	(iii)	Statement of the purpose for which the CCR unit is being used		Receives primarily bottom ash sluice water, as	Permit
				well as other plant inflows including Sanitary	
			Υ	Sewage Treatment Plant and demineralizer flush	
			·	effluent. Basins 1 and 2 are designed to be	
				alternately filled and cleaned with only one in	
40 CFR §257.73 (c)(1)	(iv A)	Name and size of watershed within which the CCR unit is		service at a time. HUC12 = 111402060602	HUC 12 Mapping
40 CFR 9257.73 (C)(I)	(iv)	located		Bayou Pierre Lake Watershed	LSU AGCenter.com
		located		Area = 18,174 acres	L30 Adderner.com
			Y	71104 10,17 1 40103	
				Only approximately 119 acres of this overall	
				watershed actually contributes runoff to Ash	
				Basin 2.	
40 CFR §257.73 (c)(1)	(v)	Description of the physical and engineering properties of the		Foundations soils consist of stiff silty clay	Permit
		foundation and abutment materials on which the CCR unit is		underlain by dense silty sand or hard silty clays.	
		constructed		Isolated areas of higher permeability materials	
			Υ	were covered with cohesive material having a	
				permeability no greater than 1x10 ⁻⁷ cm/s.	
				See Appendix C	
40 CFR §257.73 (c)(1)	(vi)	Statement of the type, size, range, and physical and engineering		Embankments and linings constructed of on-site	Permit
		properties of the materials used in constructing each zone or		clay from the Secondary Pond and Ash Basin	
		stage of the CCR unit		areas, as well as elsewhere on site. In-situ	
			Υ	cohesive materials varied between liquid limit of	
				23-65 and plasticity index of 6-44.	
				See Appendix C	
		The method of site preparation and construction of each zone		Pond constructed in cross-valley configuration.	Permit
		or stage of the CCR unit		Embankments compacted to a min 90%	
			Υ	modified Proctor dry density per ASTM D1557.	
				See Appendix C	
		The approximate dates of construction of each successive stage		Permit received Nov. 1985, operational in 1986	Permit Drawings / Owner
		of construction of the CCR unit	Υ	No major construction modifications have been	
				made since.	
40 CFR §257.73 (c)(1)	(vii)	Detailed dimensional drawings including the following:		made since.	
	(711)	Plan view and cross sections of the length and width of	V	See Appendix D	Permit
		the CCR unit	Y		
		Foundation improvements	N	N/A	Permit

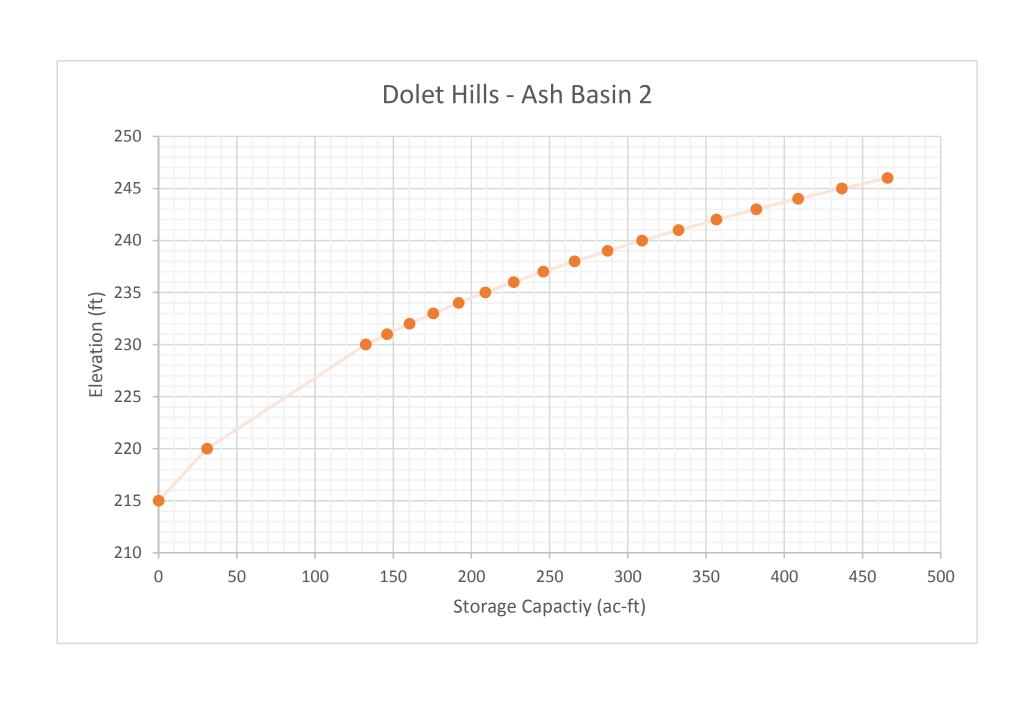
History of Construction

Section	CCR Rule Description	Included	Information	Source
	Drainage provisions, spillways, diversion ditches, outlets	Y	See Appendix E	Permit
	Instrumentation locations	Υ	See Appendix F	Permit
	Slope protection	Y	Exterior Slope: 3:1, Vegetated Interior Slope: 3:1, Vegetated above EL 243.5 and riprap 3' above and below EL 240.5	Permit / Design Drawings
	Normal operating pool surface elevation	Y	Maximum operating level at EL 240.5. Normal operating level not found in records review. See Appendix D	Permit / Design Drawings / Owner
	Maximum pool surface elevation following peak discharge from the inflow design flood	Y	Maximum pool surface level at EL 244.4 following peak discharge from the inflow design flood, assuming pond is 50% full of ash to top of dike and initial water level of EL 240.5.	Inflow Design Flood Control System Plan, Oct. 2016
	Expected maximum depth of CCR within the unit	Υ	Maximum ash level at EL 240.5. Depth of CCR is approximately 25.5 feet.	Permit / Design Drawings
	Any identifiable natural or manmade features that could		See Appendix D N/A	
	adversely affect operation of the CCR unit due to malfunction or mis-operation	N		
40 CFR §257.73 (c)(1) (viii)	Description of the type, purpose, and location of existing instrumentation	Y	Monitoring Wells - background and compliance monitoring. See Appendix F for locations. Surface water level gauge (measured manually	Permit / Owner
			at weir box location)	
40 CFR §257.73 (c)(1) (ix)	Area-capacity curves for the CCR unit	Y	See Appendix B	Measured in CAD based on Construction Drawings / aerial imagery
40 CFR §257.73 (c)(1) (x)	Description of each spillway and diversion design features and capacities and calculations used in their determination	Y	Auxiliary Spillway - EL 243.5 (designed for excess rainfall from the 100-yr flood)	Permit
			Weir Box - conveys overflow from normal operating procedures to Secondary Pond	
			See Appendix E for details	
40 CFR §257.73 (c)(1) (xi)	Construction specifications	N	Not found in records review	
	Provisions for surveillance, maintenance, and repair of the CCR unit	Y	Weekly and Annual Inspections per 40 CFR §257.83.	
40 CFR §257.73 (c)(1) (xii)	Any record or knowledge of structural instability of the CCR unit	N	N/A	











Laboratory permeability tests on ten cohesive soil samples from the basin area were performed, and the results are summarized in Table ABS 6.4.3.B-4.1. The liquid limit and the plasticity indices of in situ cohesive soils in the Ash Basin No. 1 area vary from 29 to 74 and 10 to 51, respectively, and the results are included in Table ABS 6.4.3.B.4-1.

Ash Basin No. 2

- a. A plan view and cross-sections through the dike and the basin are shown in Exhibits ABS 6.4.3.B.1-1 and ABS 6.4.3.B.1-2. These exhibits include illustration of soil types and other general features of Ash Basin No. 2.
- b. Twenty-two soil borings, B-3, B-53 through B-57, B-67 through B-76, and E-9 through E-14, were drilled in the Ash Basin No. 2 area. The locations of these borings are shown in Exhibit ABS 6.4.3.B.1-1 and the logs of these borings are presented in Appendix A.
- c. Laboratory tests were performed on soil samples obtained from this basin area and the results are summarized in Table ABS 6.4.3.B.4-2. Based on the information obtained from the boring logs and laboratory test results, the subsurface conditions in the basin area consist of stiff silty clay underlain by dense silty sand or hard silty clays. These silty clay deposits, in some locations, are overlain by approximately 2' of red, expansive silty to sandy clays. These surface soil deposits are underlain by hard, silty clays of the Porters Creek Formation which is approximately 800' thick.

As described above, the entire basin is located over impermeable cohesive soil deposits except in a few isolated instances. The log of Boring B-53 shows only one foot of clay material at the surface and the logs of Borings B-69 and B-71 show no clay at the surface.

Table ABS 6.4.3.B.4-2(Page 1 of 4) SUMMARY OF LABORATORY TEST RESULTS OF SOIL BORING SAMPLES RELATED TO ASH BASIN - 2

Barting Bample Supple Supple				Partic (cle Sire An	Particle Size Analysis (\$ Passing)		At	Atterberg Limits	inits					
SS-2 14,5-16.0 96 26 1 1 34 1 34 1 34 1 34 34 36 31 31 34 31 34 37 31 34 37 31 37 31 37 31 37 31 37 <th< th=""><th>oring</th><th>Sample</th><th>Sample Depth (Ft)</th><th>No. 4 Sieve</th><th>-</th><th>No. 40 Sieve</th><th>No. 200 Steve</th><th>Liguid Limit (%)</th><th>Plastic Limit (\$)</th><th>Plasticity Index (\$)</th><th>Unified Soil Classification System</th><th>Water Content</th><th>Weight (Pcf)</th><th></th><th>Unconfined Compressive Strength q</th></th<>	oring	Sample	Sample Depth (Ft)	No. 4 Sieve	-	No. 40 Sieve	No. 200 Steve	Liguid Limit (%)	Plastic Limit (\$)	Plasticity Index (\$)	Unified Soil Classification System	Water Content	Weight (Pcf)		Unconfined Compressive Strength q
SS-2 14,5-16.0 100 54 7 7 SH 94.6 7 7 84.6 94.6 7 7 84.6 94.6 13.7 113 7 113 7 113 8 8 8 8 8 9 10 9 10 9 10 8 10 10 10 10 9 10	£ 3	88-2	6.5-8.0			86	92				WS	6.6		(a) (a)	(ver)
87-2 2.0-4, 0 100 30 31 21 9 8C 13.7 113 88-4 6.5-8.0 20 20 15 19 26 CI 22.0 101 3.9ato-8 87-2 2.0-4.0 96 87 15 18 37 CH 25.2 100 3.9ato-8 87-2 2.0-4.0 96 87 15 18 37 CH 25.0 105 3.9ato-8 87-3 6.0-8.0 100 99 65 21 44 CH 27.9 3.9ato-8 87-10.0 100 16 16 25 17 8 CL 15.3 110-8 88-5 10.0 100 99 15 21 24 CL 15.3 110-8 89-5 10.0 100 99 15 21 24 CL 25.3 10 15.3 13.9ato-9 89-70.0 100 100	-1	SS-2	14.5-16.0			100	₹				SM	94.6			
85-4 6,5-8.0 96 20 45 19 26 CL 22.0 101 3.9410-8 87-2 2.0-4.0 96 45 19 26 CL 22.0 101 3.9410-8 87-4 6.0-8.0 100 99 45 21 44 CH 25.0 106 3.9410-8 87-4 6.0-8.0 100 99 65 21 44 CH 25.0 109 4.1310-8 87-2 2.0-4.0 100 18 7 17 8 77-9 15.0 106 1.1310-8 87-2 2.0-4.0 100 100 25 17 8 CL 15.3 110 1.1310-8 85-10.0 100 1	-53	ST-2	2.0-4.0			100	30	30	21	6	88	13.7	113		
PB-8 23.0-25.0 100 99 45 19 26 CL 22.0 101 3.9ato-8 8T-2 2.0-4.0 96 87 18 37 CH \$6.0 96 1.8 37 CH \$6.0 96 1.8ato-8 1.8ato-9		\$8-h	6.5-8.0	_		86	20				WS	12.0			
87-2 2.0-4.0 96 87 55 18 37 CH \$6.0 96 87-4 6.0-8.0 100 99 65 21 44 CH 20.2 109 85-5 8.5-10.0 100 48 7 8 77.9 97 85-7 2.0-4.0 100 99 45 21 8 CL 15.0 108 89-7 8.5-10.0 100 99 45 21 24 CL 25.3 110 89-7 28.0-30.0 100 <td></td> <td>PB-8</td> <td>23.0-25.0</td> <td></td> <td></td> <td>901</td> <td>8</td> <td>54</td> <td>19</td> <td>56</td> <td>TO</td> <td>22.0</td> <td>1001</td> <td>3.9410-8</td> <td>12.6</td>		PB-8	23.0-25.0			901	8	54	19	56	TO	22.0	1001	3.9410-8	12.6
ST-4 6.0-8.0 100 99 65 21 44 CH 20.2 32.0 109 97 SS-5 8.5-10.0 100 48 77.9 87.9 97 ST-2 2.0-4.0 99 60 25 17 8 CL 15.0 108 SS-5 8.5-10.0 100 99 45 21 24 CL 25.3 110 Pb-9 28.0-30.0 100 100 100 10 31 CL-CH 24.0 105	-54	ST-2	2.0-4.0			8	87	55	18	37	СЯ	0.98	8		
SS-5 8.5-10.0 46 25 17 8 CL 15.0 108 SS-5 8.5-10.0 100 45 21 24 CL 25.3 110 Pb-9 28.0-30.0 100 100 100 100 100 20 109 24.0 105		ST-4	6.0-8.0			100	8	65	23	73	СН	32.0	8.8	1.8×10-8	
ST=2 2.0-4.0 99 60 25 17 8 CL 15.0 108 SS=5 8.5-10.0 100 99 45 21 24 CL 25.3 110 Pb=9 28.0-30.0 100 100 50 19 31 CL-CH 24.0 105 24.0 102 24.0 102 24.0 102 24.0 102		88-5	8.5-10.0			100	84				WS	27.9			
8.5-10.0 100 99 45 21 24 CL 25.3 28.0-30.0 100 50 19 31 CL-CH 24.0 105	22	ST-2	2.0-4.0			8	8	25	17	80	ಕ	15.0	108	3.1210-8	
28.0-30.0 100 50 19 31 CL-CH 24.0 105 24.0		38-5	8.5-10.0			100	8	45	21	77	ij	25.3			
		PB-9	28.0-30.0			100	100	20	19	31	CL-CH	24.0	105	3.8x10-9	٥

Table ABS 6.4.3.B.4-2(Page 2 of 4) SUMMARY OF LABORATORY TEST RESULTS OF FOIL BORING SAMPLES RELATED TO ASH BASIN - 2

			Partic	Particle Size Analysis (% Passing)	()		Y	Atterberg Limits	inite					
Boring	Sample	Sample Depth (Ft)	No. 4 Sieve	No.10 Steve	No. 40 Steve	No. 200 Sleve	Liquid Limit (\$)	Plastic Limit (\$)	Plasticity Index (%)	Unified Soil Classification System	Water Content	Dry.Unit Weight (Pcf)	Leboratory Permeability (k,cm/sec)	Unconfined Compressive Strength q w'
B-36	ST-2	2.0-4.0			100	51				כר	15.4	111		
	PB-6	13.0-15.0			100	86	8	50	30	CL-CR	25.0	102	4.8x10-9	11.5
	PB-10	33.0-35.5			100	100	147	19	28	T)	21.7	110	8.6x10-9	10.4
B-57	ST-2	2.0-4.0			100	61	56	50	6	T)	16.1	108		
	8T-6	13.0-15.0			100	16	45	21	77	CL	25.1	8	2.6-10-8	
	PB-8	23.0-25.0	+:		100	100	94	19	7.2	13	24.0	105	0	11.5
6-3	ST-3	0.9-0.4			86	72	47	20	27	CL	23.0	56	6.1×10	
E-10	ST-3	0.9-0.4			100	76	643	20	23	CL	23.0	76	3.8×10	
E-11	ST-3	0.9-0.4				47	30	19	111	SC	15.4	116		3.8
	ST-5	8.0-10 0				52	27	17	10	CI.	27.0			
	ST-6	13.0 15.0			100	86				CL	15.0	116	6.6 10	
E-12	5T-4	0.8-0.9				26	52	20	32	СН	16.0	116	4.1×10-8	
	ST-6	13.0-15.0				46	20	19	31	но-то	23.4			
	ST-8	23.5-25.0				100	20	20	30	CL-CH	22.8			
E -13	ST-2	2.0-4.0				44	87	20	28	15	20.3	66		8.7
	ST-5	8.0-10.0				46	57	20	25	To	26.9	76		
	9-55	13.5-15.0			100	26	45	20	25	CL	23.8			
	88-8	23.5-25.0			100	86				CL	27.6			

Table ABS 6.4.3.B.4-2 (Page 3 of 4) SUMMARY OF LARORATORY TEST RESULTS OF SOIL BORING SAMPLES RELATED TO ASH BASIN - 2

Euch Size-				Partic	Particle Size Analysis (% Passing)	Analysis ()		A	Atterberg Limits	Limits					
ST-2 2.0-4.0 100 99 98 51 38 19 19 CCL 11.0 100 4.0-16.0 ST-3 4.0-6.0 100 100 100 100 12 37 37 38 11.0 100 100 100 100 100 100 98 42 21 21 CL 21.0 100 98 42 21 21 CL 21.0 98 22 10 21 21.0 100 98 42 21 CL 21.0 21.0 100 98 42 21 21 CL 21.0 98 20 21 21 CL 24.5 99 2.0 21 CL 24.5 99 2.0 21 CL 24.5 99 2.0 21 CL 24.5 39 3.0 10 10 10 10 10 10 10 10 10 10 10 10	Boring	Sample Fumber	Sample Depth (Ft)	No. 4 Sieve		No. 40 Sieve	No. 200 Sieve	Liquid Limit (%)	Plastic Limit (%)		Unified Soil Classification System	Water Content (%)	Dry Unit Weight (Pcf)		Unconfined Compressive Strength qu (Ksf)
5T-3 4.0-6.0 100 100 99 12 SPH SPH-SM S	E-14	ST-2	2.0-4.0	100	66	86	51	38	19	19	CL	11.0	104	4.1×10-8	6.7
ST-4 8.5-10.0 100 100 27 55 22 33 CH 21.5 106 ST-3 4.0-6.0 100 96 55 22 21 CH 21.5 106 ST-3 8.0-10.0 100 98 42 21 21 CL 21.0 98 ST-3 2.0-4.0 98 42 21 21 CL 21.0 98 SS-3 4.5-6.0 98 97 94 21 20 CL 21.0		ST-3	4.0-6.0	100	100	66	12				SP-SM				
ST-2 2.0-4.0 100 9% 55 22 33 CH 21.5 106 ST-3 4.0-6.0 100 98 4.2 21 21 CL 21.0 98 ST-3 8.0-10.0 98 4.1 20 21 CL 21.0 98 ST-3 4.5-6.0 98 97 96 21 15 CL 21.5 99 SS-3 6.5-8.0 98 97 96 21 12 SM 12.0 SM 18.9 18.9 ST-2 1.0-4.0 98 97 96 21 17 SM 18.9		7-LS	8.5-10.0	100	100	001	27				SM				
ST-3 4.0-6.0 100 98 42 21 21 CL 21.0 99 ST-2 2.0-4.0 100 62 34 19 15 CL 24.5 99 SS-3 4.5-6.0 98 97 96 21 2 CL 21.6 98 SS-4 6.5-8.0 98 97 96 21 SM 15 CL 21.6 98 SS-5 6.5-8.0 98 97 96 21 SM 15 SM 15.9 100 ST-2 1.0-4.0 8.5-10.0 46 30 18 12 SM 21.5 105 SS-4 6.5-8.0 100 44 29 17 12 SM 22.0 SS-4 6.5-8.0 100 44 29 17 12 SM 22.0 ST-3 4.0-6.0 2 2 2 2 2 2 2 2	B-67	ST-2	2.0-4.0			100	96	55	22	33	СН	21.5	106	2.6×10-9	
ST-2 8.0-10.0 99 41 20 21 CL 24.5 99 ST-2 2.0-4.0 100 62 34 19 15 CL 21.6 98 SS-3 4.5-6.0 98 97 96 21 SM 15 CL 21.6 98 SS-4 6.5-8.0 98 97 96 21 SM 12 SM 18.9 100 ST-2 1.0-4.0 100 46 30 18 12 SM 11.5 11.5 SC 19.7 105 ST-3 4.0-6.0 41 38 29 17 12 SC 13.3 88 ST-3 100 44 35 17 12 SM 22.0 ST-3 4.0-6.0 44 35 18 17 SC 105 ST-3 8.0-10.0 46 35 18 17 CH 25.6 97 <tr< td=""><td></td><td>ST-3</td><td>4.0-6.0</td><td></td><td></td><td>100</td><td>86</td><td>42</td><td>21</td><td>21</td><td>CL</td><td>21.0</td><td>86</td><td></td><td></td></tr<>		ST-3	4.0-6.0			100	86	42	21	21	CL	21.0	86		
\$5-3 \$1.00 \$62 \$34 \$19 \$15 \$CL \$21.6 \$98 \$5-4 \$6.5-8.0 \$98 \$97 \$96 \$21 \$54 \$15.9 \$100 \$5-5 \$6.5-8.0 \$98 \$97 \$96 \$21 \$54 \$54 \$15.9 \$100 \$5-5 \$6.5-8.0 \$100 \$46 \$30 \$18 \$12 \$56 \$1.5 \$100 \$5-4 \$6.5-8.0 \$100 \$41 \$29 \$17 \$12 \$56 \$13.3 \$88 \$5-4 \$6.5-8.0 \$100 \$44 \$29 \$17 \$12 \$50 \$13.3 \$88 \$5-5 \$6.5-8.0 \$100 \$44 \$29 \$17 \$12 \$50 \$105 \$5-7 \$6.0-6.0 \$6 \$35 \$18 \$17 \$20 \$105 \$7-3 \$6 \$35 \$12 \$17 \$25 \$25 \$25 \$25 \$25 \$25 \$		ST-5	8.0-10.0				66	17	20	21	CC	24.5	66		
SS-3 4,5-6.0 98 97 96 21 SM 15.9 100 SS-5 8,5-10.0 98 97 96 21 SM 12 SM 18.9 18.9 ST-2 2.0-4.0 100 46 30 18 12 SC 19.7 105 ST-3 4.0-6.0 100 46 30 18 12 SC 19.7 105 SS-4 6.5-8.0 100 41 29 17 12 SC 19.7 105 SS-5 8.5-10.0 100 44 29 17 12 SM 22.0 ST-2 2.0-4.0 100 54 29 17 12 CL 20.9 105 ST-3 4.0-6.0 54 35 18 17 SC 20.9 105 ST-3 8.0-10.0 79 55 22 33 CH 25.0 97	B-68	ST-2	2.0-4.0			100	62	34	19	15	75	21.6	86	2.9×10-7	
SS-4 6.5-8.0 98 97 96 21 SM 18.9 </td <td></td> <td>SS-3</td> <td>4.5-6.0</td> <td></td> <td></td> <td></td> <td>31</td> <td></td> <td></td> <td></td> <td>S</td> <td>15.9</td> <td>100</td> <td>1.4×10-7</td> <td></td>		SS-3	4.5-6.0				31				S	15.9	100	1.4×10-7	
SS-5 8,5-10.0 100 23 18 12 SG 11.5 11.5 SG 19.7 105 ST-2 2.0-4.0 100 46 30 18 12 SG 19.7 105 ST-3 4.0-6.0 100 41 29 17 12 SG 13.3 88 SS-4 6.5-8.0 100 44 29 17 12 SM 22.0 SS-5 8.5-10.0 100 44 35 18 17 SG CL 20.9 105 ST-3 4.0-6.0 99 55 22 33 CH 25.6 97 ST-5 8.0-10.0 99 55 22 33 CH 25.6 97		8S-4	6.5-8.0	86	46	96	21				SM	18.9			
ST-2 2:0-4.0 100 46 30 18 12 SC 19.7 105 ST-3 4,0-6.0 38 29 17 12 SC 13.3 88 SS-4 6.5-8.0 100 41 7 22.0 13.3 88 SS-5 8.5-10.0 100 44 29 17 12 CL 20.0 105 ST-3 4.0-6.0 54 35 18 17 SC 20.9 105 ST-3 8.0-10.0 99 55 22 33 CH 25.6 97		88-5	8.5-10.0			100	23				WS.	21.5			
ST-3 4,0-6.0 38 29 17 12 SC 13.3 88 SS-4 6,5-8.0 100 41 SM 22.0 SS-5 8,5-10.0 100 44 SM 22.0 ST-2 2.0-4.0 100 54 29 17 12 CL 20.9 105 ST-3 4.0-6.0 99 55 22 33 CH 25.6 97	69-8	ST-2	2.0-4.0			100	97	30	18	1.2	SC	19.7	105	1.4×10-8	
SS-4 6,5-8.0 100 41 SM 22.0 SS-5 8,5-10.0 100 44 29 17 12 CL 20.9 105 ST-2 2.0-4.0 100 54 29 17 12 CL 20.9 105 ST-3 4.0-6.0 46 35 18 17 SC 26.8 93 ST-5 8.0-10.0 99 55 22 33 CH 25.6 97		ST-3	0.9-0.4				38	56	17	1.2	SC	13.3	88		
SS-5 8.5-10.0 100 44 20.2 ST-2 2.0-4.0 100 54 29 17 12 CL 20.9 105 ST-3 4.0-6.0 46 35 18 17 SC 26.8 93 ST-5 8.0-10.0 99 55 22 33 CH 25.6 97	Ī	8S-4	6.5-8.0			100	17				SM	22.0			
ST-2 2.0-4.0 100 54 29 17 12 CL 20.9 105 ST-3 4.0-6.0 46 35 18 17 SC 26.8 93 ST-5 8.0-10.0 99 55 22 33 CH 25.6 97		SS-5	8.5-10.0			100	777				SM	22.2			
4.0-6.0 8.0-10.0 99 55 22 33 CH 25.6 97	02-1	ST-2	2.0-4.0			100	54	56	17	12	TO	20.9	105	1.8×10-8	
8.0-10.0 99 55 22 33 CH 25.6		ST-3	4.0-6.0				97	35	18	17	SC	26.8	93		
		ST-5	8.0-10.0				66	55	22	3.3	Н	25.6	76		

Table ABS 6.4.3.B.4-2 (Page 4 of 4)
SUMMARY OF LABORATORY TEST RESULTS OF
SOIL BORING SAMPLES RELATED TO ASH BASIN - 2

Boring Sample Sample (Ft) B-71 ST-1 ,0.0-2.0 SS-4 6.5.8.0 SS-4 6.5.8.0 SS-5 8.5-10.0 B-72 ST-2 2.0-4.0 ST-3 4.0-6.0 B-73 ST-2 2.0-4.0 ST-3 4.0-6.0 B-74 ST-1 0.0-2.0 ST-3 4.0-6.0 ST-3 4.0-6.0 ST-3 4.0-6.0 ST-4 8.5-10.0 ST-5 2.0-4.0 ST-7 1 0.0-2.0 ST-7 2 2.0-4.0 ST-7 2 2.0-4.0 ST-7 3 4.0-6.0 ST-7 3 4.0-6.0 ST-7 4.0-6.0 ST-7 4.0-6.0 ST-7 4.0-6.0	No. 4 No.10	(% Passing)		At	Atterberg Limits	inite					
ST-1 SS-4 SS-4 ST-2 ST-2 ST-3 ST-3 ST-1 ST-1 ST-3		o No. 40	No. 200 Sieve	Liguid Limit (%)	Plastic Limit (%)	Plasticity Index (%)	Unified Soil Classification System	Water Content (%)	Dry Unit Weight (Pcf)	Laboratory Permeability (k,cm/sec)	Unconfined Compressive Strength qu (Ksf)
ST-2 SS-4 SS-4 ST-2 ST-2 ST-1 ST-1 ST-3 ST-3		100	20	23	17	9	SC	21.4	63		
SS-4 SS-5 ST-2 ST-3 ST-1 ST-1 ST-1 ST-3	_	100	38	26	17	6	SC	19.3	100	9.0×10-6	
SS-5 ST-2 ST-3 ST-2 ST-1 ST-1 ST-3 ST-5		100	24	23	11	9	SC	20.7	,		
ST-2 SS-4 ST-2 ST-3 ST-1 ST-1 ST-3 ST-5		100	23	,			SM	24.4	,		
ST-3 SS-4 ST-2 ST-3 ST-1 ST-1 ST-5 ST-5 ST-5	-	100	99	07	19	21	CL	21.4	105	2.5×10-7	
SS-4 ST-2 ST-3 SS-4 ST-1 ST-3 ST-5 ST-5		100	96	62	22	07	H2)	24.3	9.5	9.Cx10-8	
ST-2 ST-3 SS-4 ST-1 ST-3 ST-5 ST-5		100	66	20	20	30	CL-CH	22,3	102		
ST-3 SS-4 ST-1 ST-3 ST-5 SS-6 ST-2		100	7.5	777	21	23	CL	16.5	113.5	3.2×10-8	
SS-4 ST-1 ST-3 ST-5 SS-6 ST-2 ST-3	_	100	77	50	21	29	HD-TD	25.2	93		
ST-1 ST-5 SS-6 ST-2 ST-3			23	56	1.7	6	SC	12.4			
ST-3 ST-5 SS-6 ST-2 ST-3		100	63	28	18	10	CL	21.4	101	1.2×10-7	
SS-6 ST-2 ST-3			47	33	61	14	SC	25.4	76	2.9×10-8	
SS-6 ST-2 ST-3	_		97	07	20	20	CL	27.8	89		
ST-2 ST-3		100	21		•		SCorSM	27.4		1-0. 0	
_	_	100	70	34	61	15	CL	22.4	68	(disturbed)	
	_		53	34	18	16	CL	27.1	95	1.8×10-8	
_			57	97	21	2.5	CL	8.02	46		
_	-	100	86	99	21	35	СН	28.2	93	6.5×10-9	
ST-3 4.0-6.0	_		66	43	21	22	CL	26.8	92		
ST-5 8.0-10.0			100	17	21	26	CL	23.8	101		

Boring B-53 is along the dike alignment (see Exhibits ABS 6.4.3.B.1-1 and ABS 6.4.3.B.1-2). Even though there is only one foot of CL material at this location, Borings B-67 and B-70, which are in the vicinity of Boring B-53, indicate 20' and 4' of CL at the surface, respectively.

Therefore, the thickness of the surface clays at Boring B-53 is an isolated condition. In addition, this area will be covered with cohesive material when the dike is constructed.

Boring B-69 indicates 6' of clayey fine sand (SC) material at the surface. However, the coefficient of permeability (k) of this material is 1.4 x10^{-B} cm/sec (the requirement is $k<1 \times 10^{-7}$ cm/sec). In addition to this very low k value, Borings B-73 ad B-68, which are in the vicinity of 8-69, indicate 6' and 4' of CL material. Therefore, the soil conditions at Boring B-69 will not cause any problem with regard to contamination of groundwater. As part of the Construction Verification Program to be instituted by SWEPCO (see Appendix B), this area will be investigated to verify that a barrier equivalent to 3' of natural clay having a coefficient of permeability no greater than 1×10^{-7} cm/sec has been provided. If this investigation determines that any existing barrier material does not meet this permeability requirement, action will be taken to replace the unsuitable material with an acceptable non-synthetic lining material.

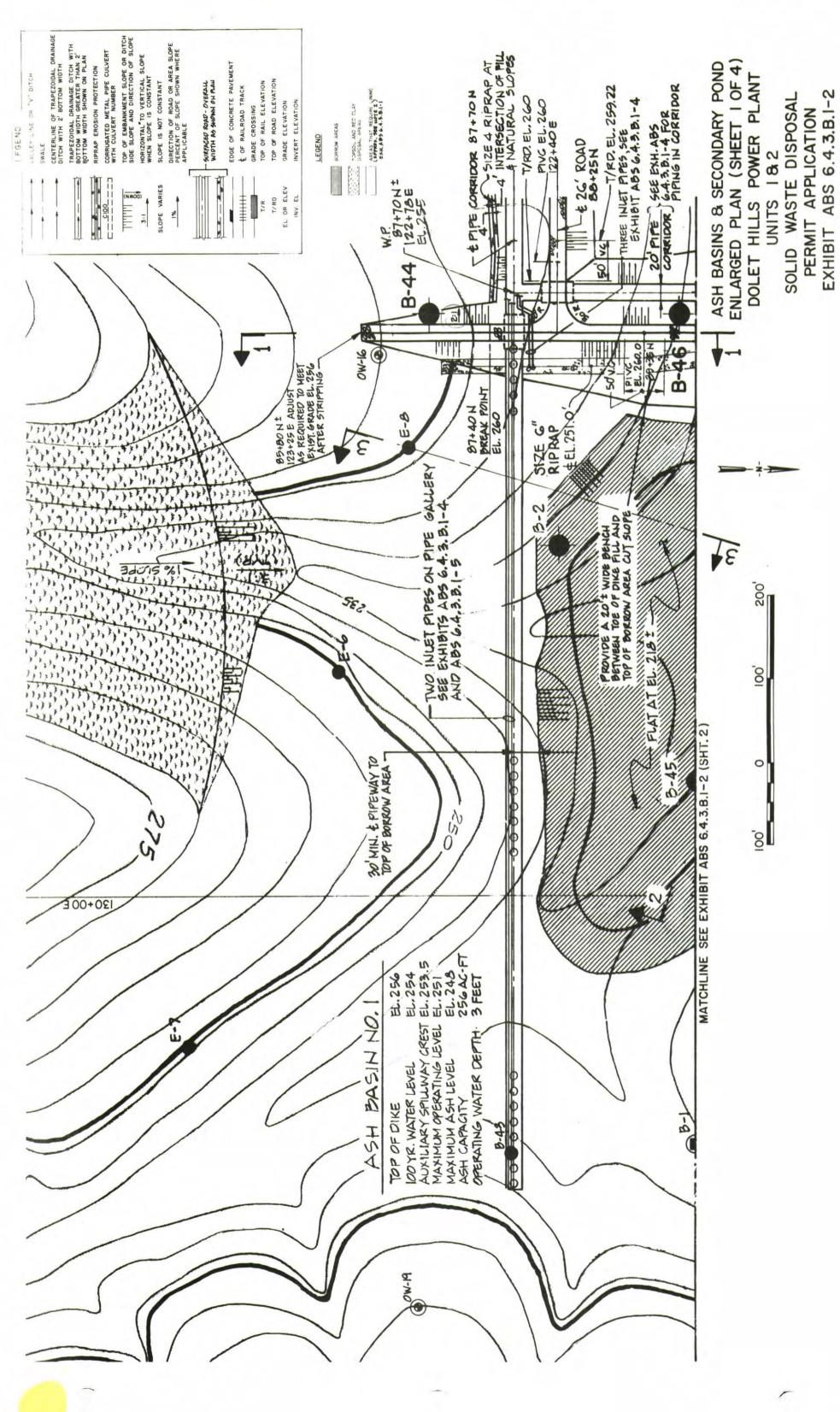
Boring B-71 indicates 8' of SC material with high k value $(90 \times 10^{-7} \text{ cm/sec})$. Two borings, B-72 and B-68, in the vicinity of Boring B-71, indicate 20' and 4' of clay (CL) material. Therefore, the surface soil condition at Boring B-71 is an isolated condition. As part of the Construction Verification Program (see Appendix B) this area will be investigated to verify that a barrier equivalent to 3' of natural clay having a coefficient of permeability no greater than 1×10^{-7} cm/sec has been provided. If this investigation determines that any existing barrier material does not meet this permeability requirement, action will be taken to replace the unsuitable material with an acceptable non-synthetic lining material.

The fill material required for construction of the dike with side slopes of three horizontal to one vertical, will be obtained from the excavation for the Secondary Pond and from suitable borrow areas within the Ash Basins (Exhibits ABS 6.4.3.B.1-1 and ABS 6.4.3.B.1-2). The borrow sources are identified in Exhibit ABS 6.4.3.B.1-1. The dike fill will be compacted to a minimum 90% modified Proctor maximum dry density per ASTM D1557.

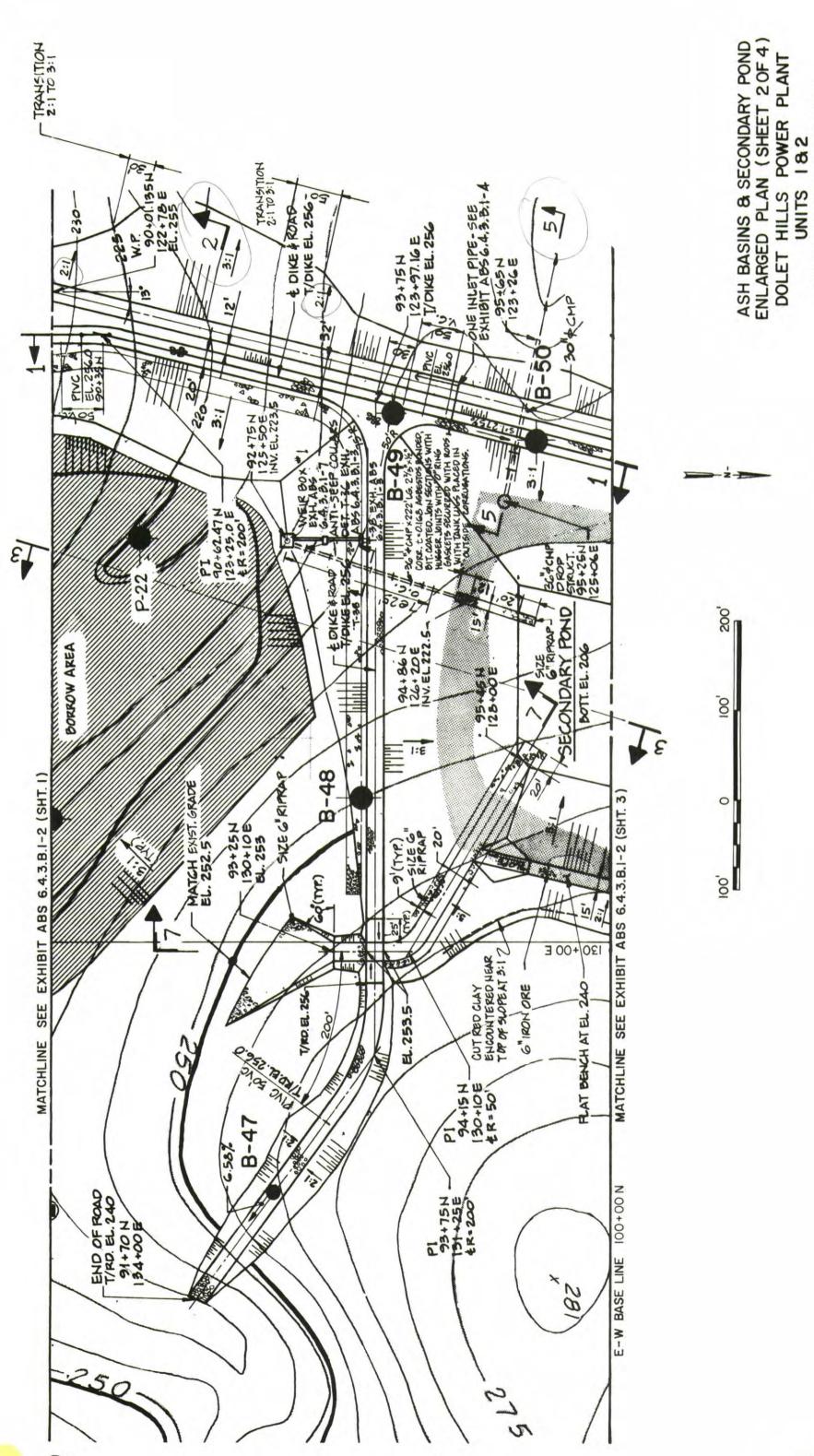
Laboratory permeability tests on twenty-six cohesive soil samples obtained from the borings in the basin area were performed, and the results are summarized in Table ABS 6.4.3.B.4-2. The liquid limit and plasticity indices of in situ cohesive soils in the Ash Basin No. 2 area vary from 23 to 65 and 6 to 44, respectively. These test results are also included in Table ABS 6.4.3.B.4-2.

Secondary Pond

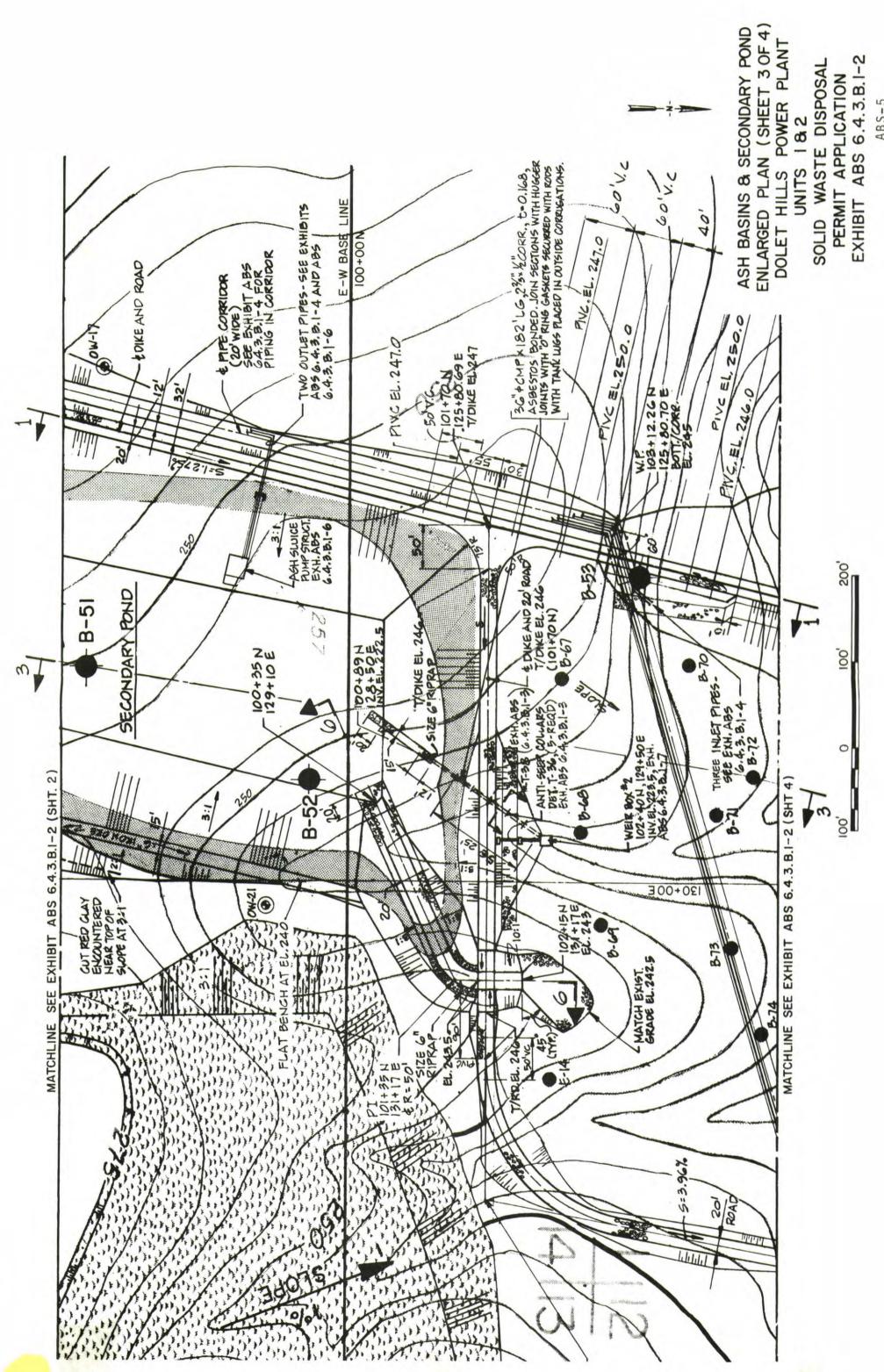
a. A plan view and cross sections through the dike and the pond are shown in Exhibits ABS 6.4.3.8.1-1 and ABS 6.4.3.8.1-2. These exhibits include illustration of

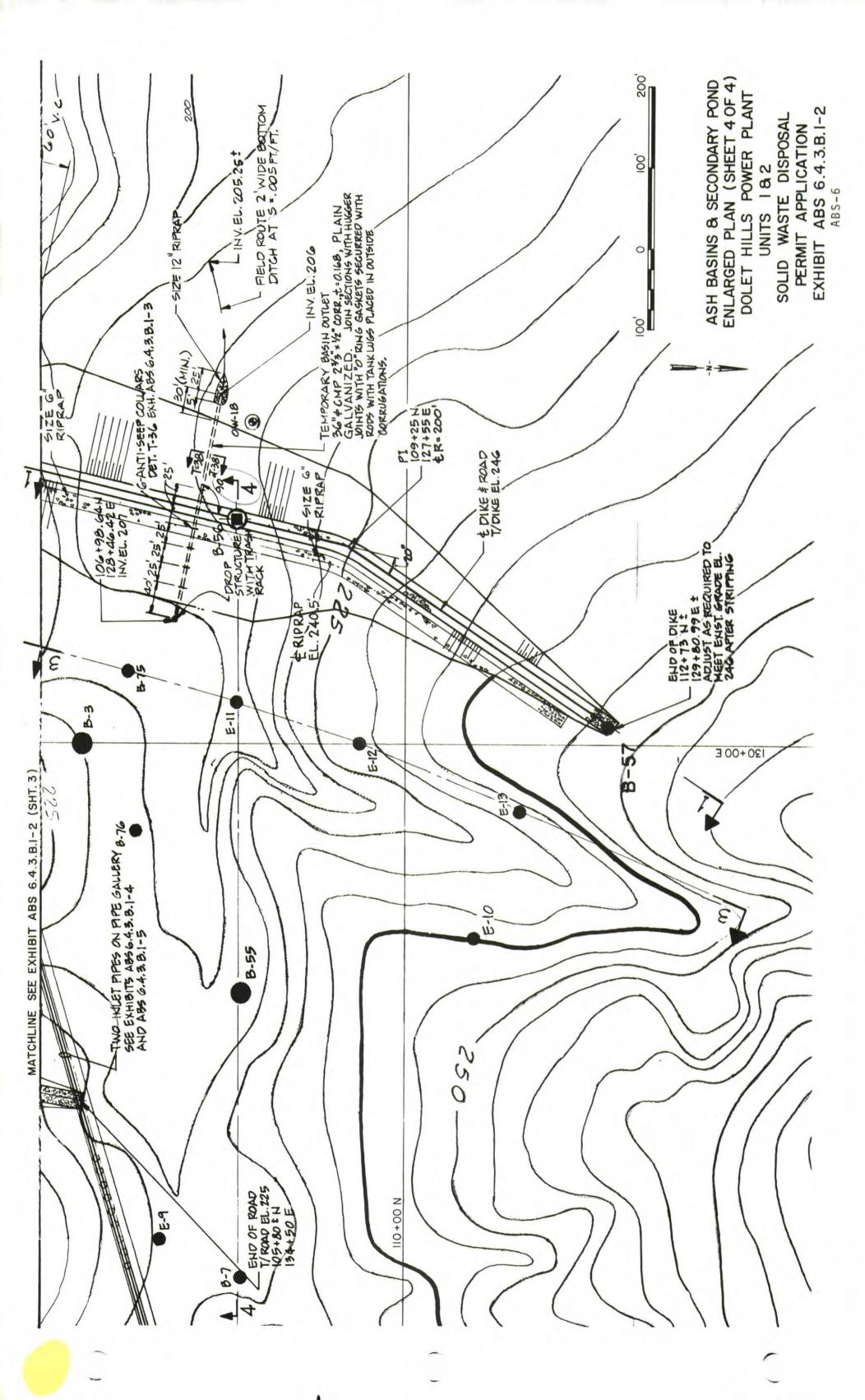


ABS-3

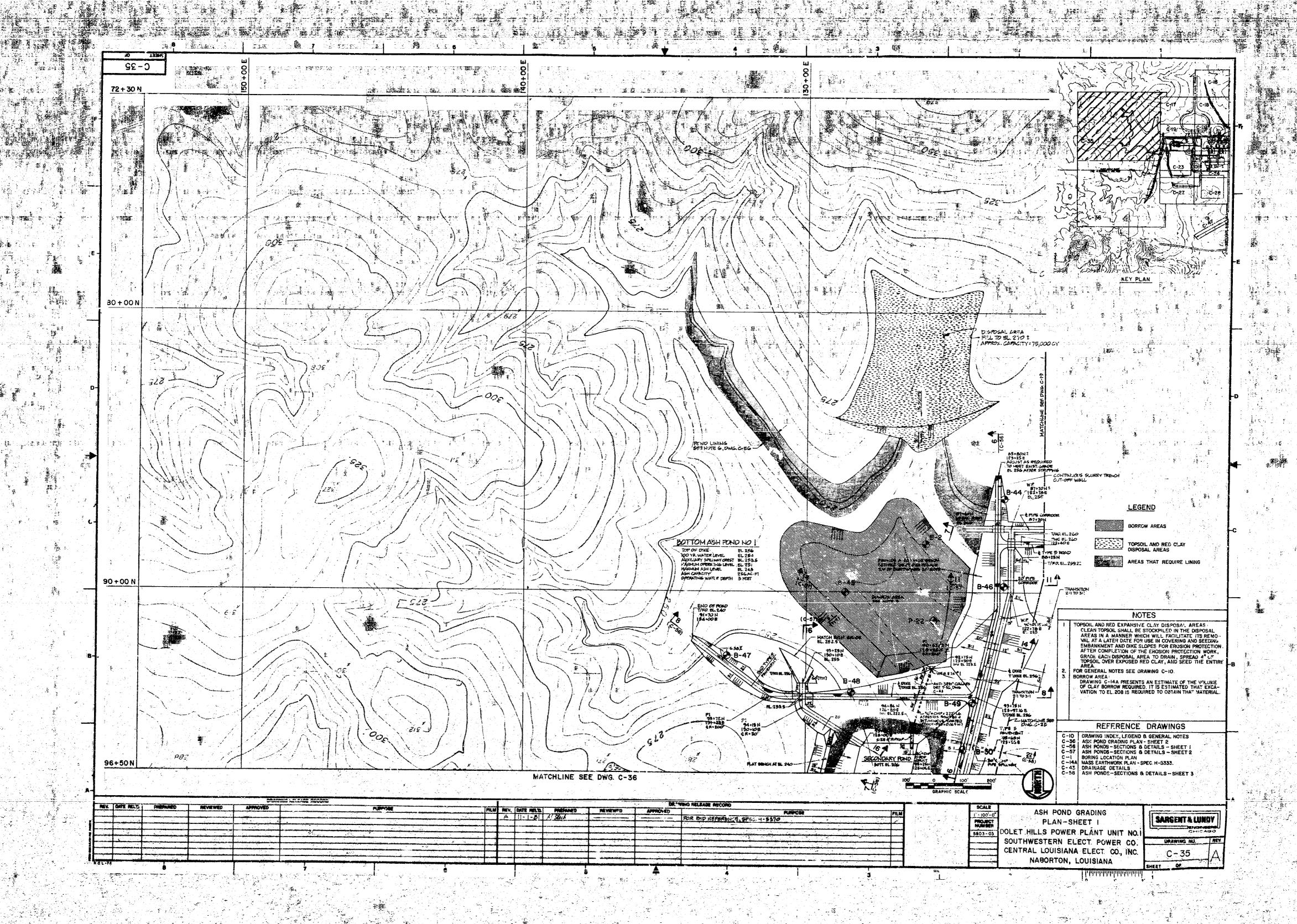


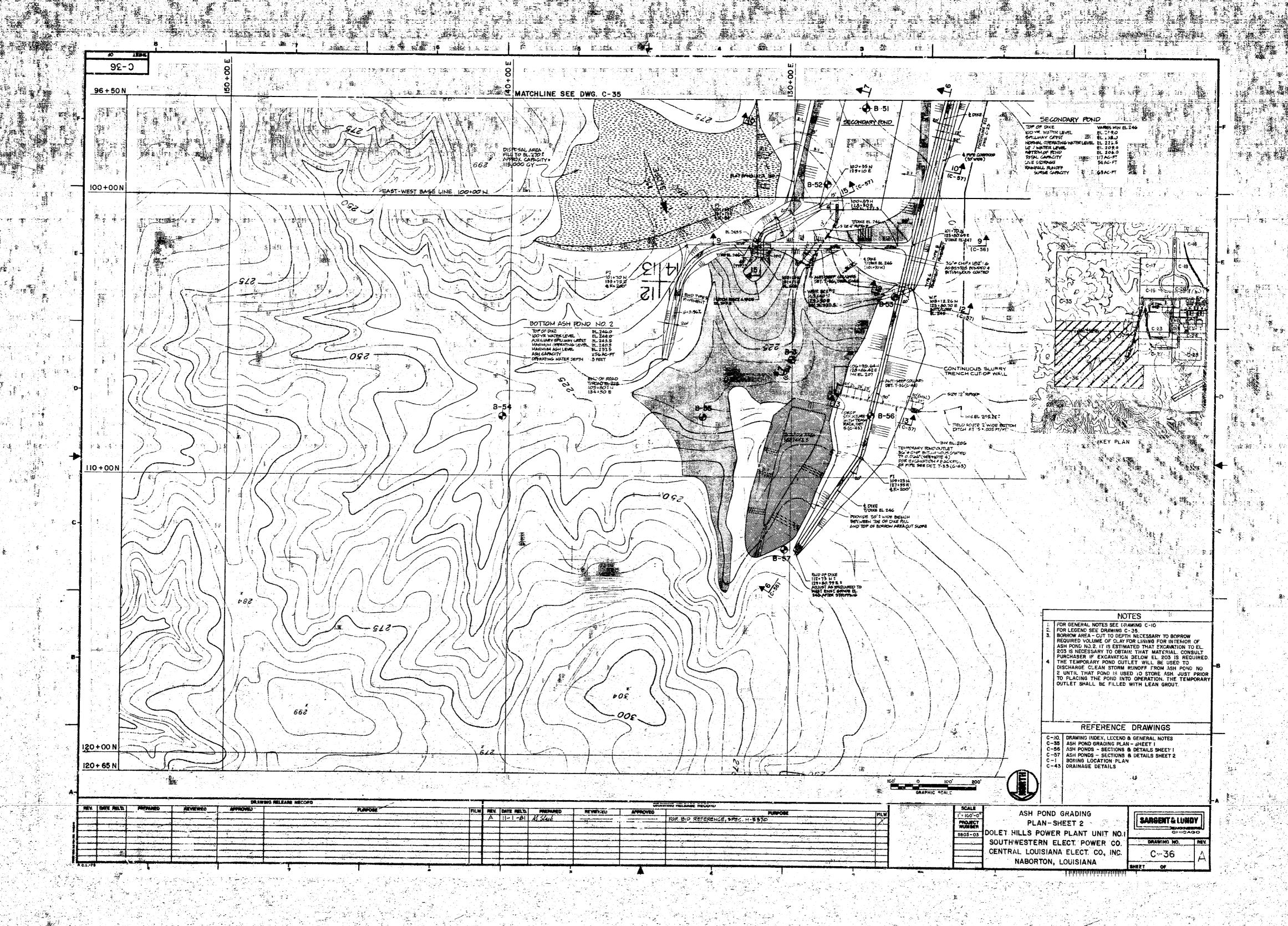
ASH BASINS & SECONDARY FOND
ENLARGED PLAN (SHEET 20F4)
DOLET HILLS POWER PLANT
UNITS 18.2
SOLID WASTE DISPOSAL
PERMIT APPLICATION
EXHIBIT ABS 6.4.3.B.1-2
ABS-4

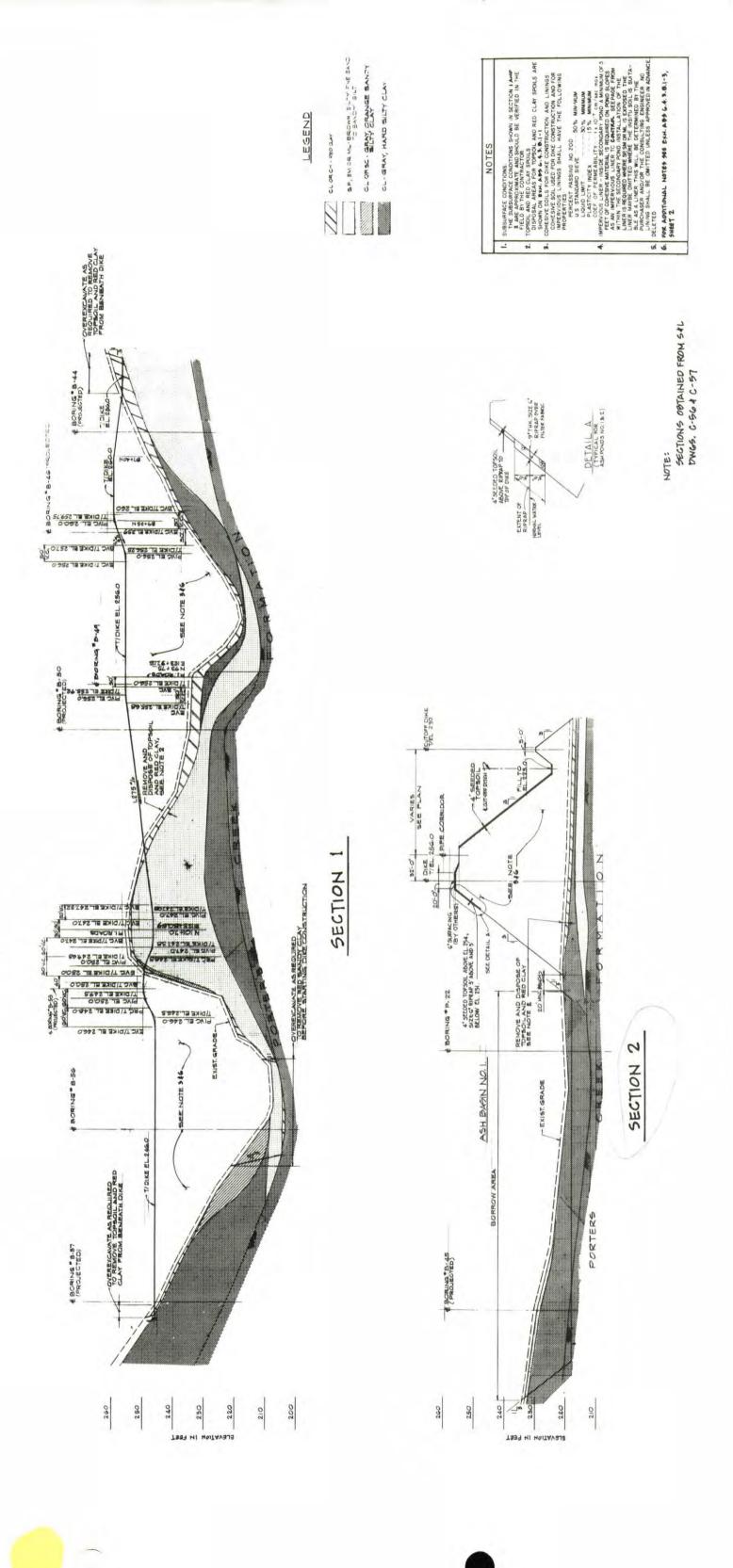








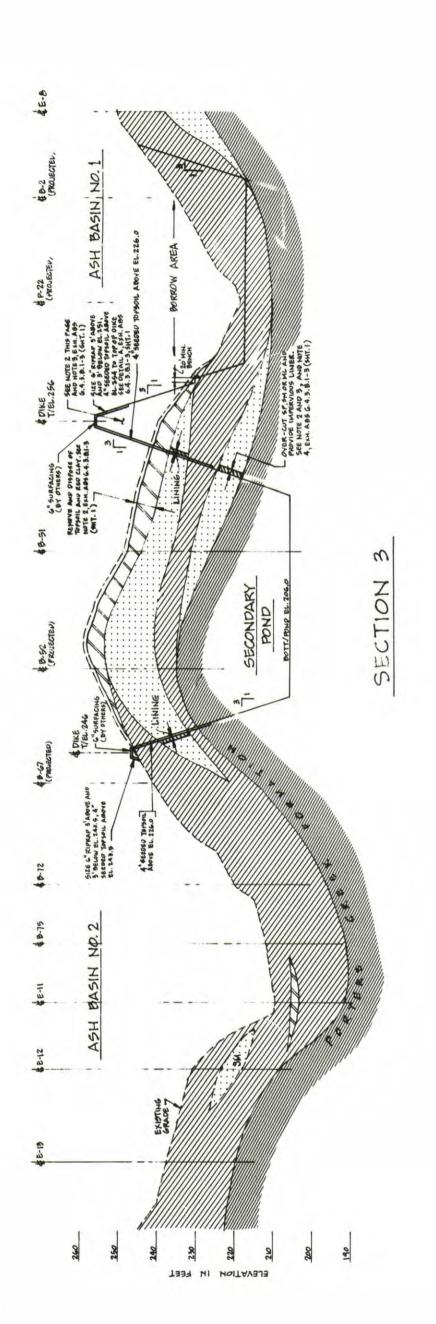


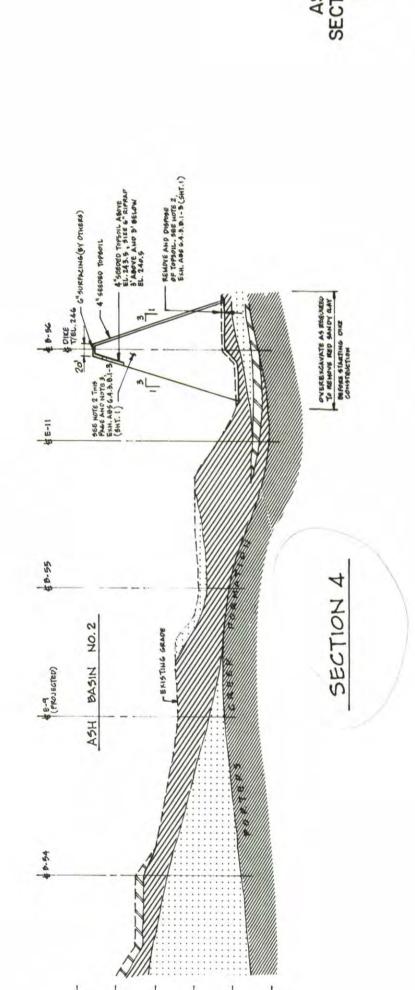


ASH BASINS & SECONDARY POND
SECTIONS AND DETAILS (SHEET 10F3)
DOLET HILLS POWER PLANT
UNITS 1 & 2
SOLID WASTE DISPOSAL
PERMIT APPLICATION
EXHIBIT ABS 6.4.3.B.1-3

EXHIBIT ABS 6.4.3.B.I-3

PERMIT APPLICATION





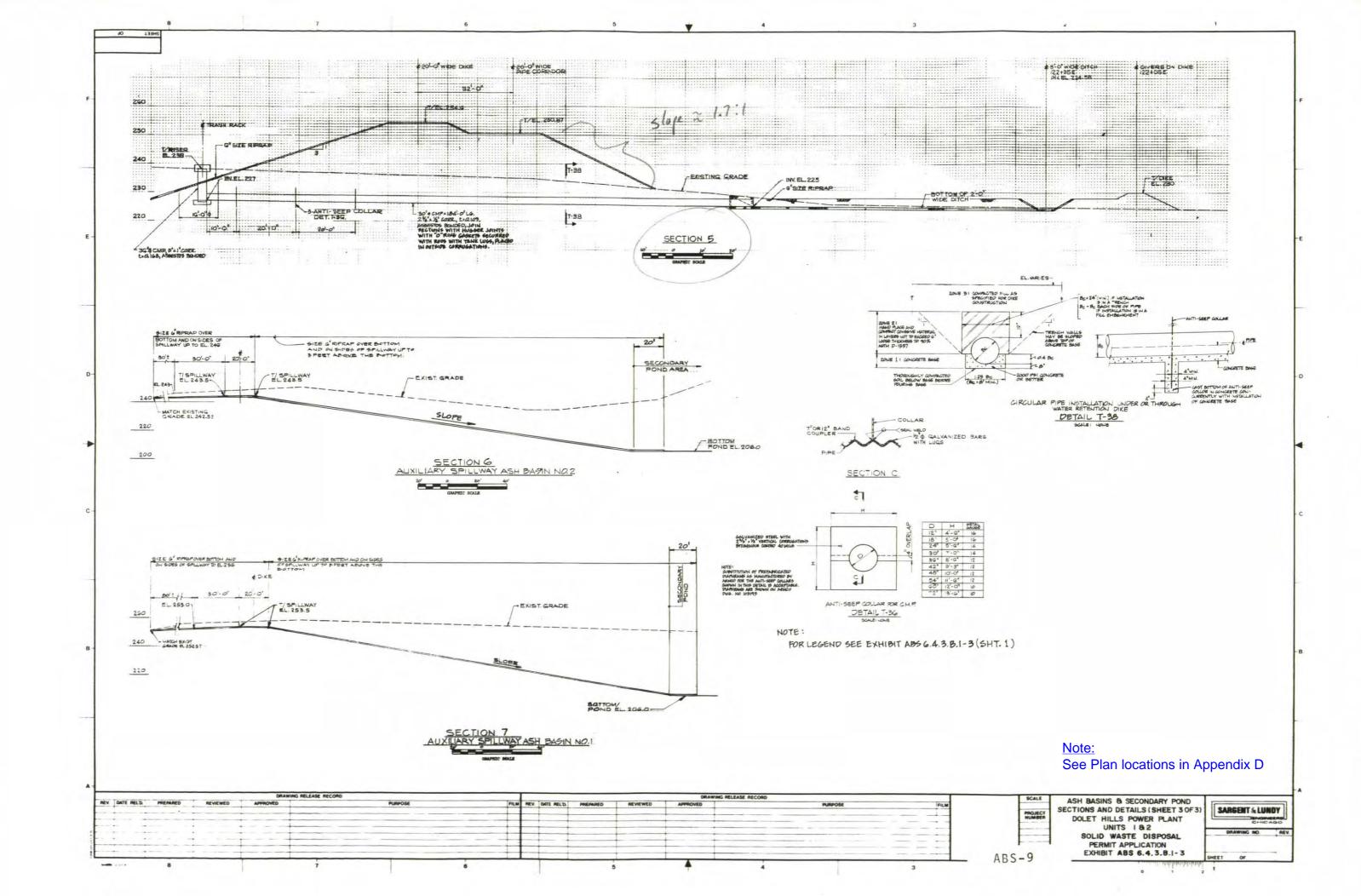
ELEVATION IN PEET

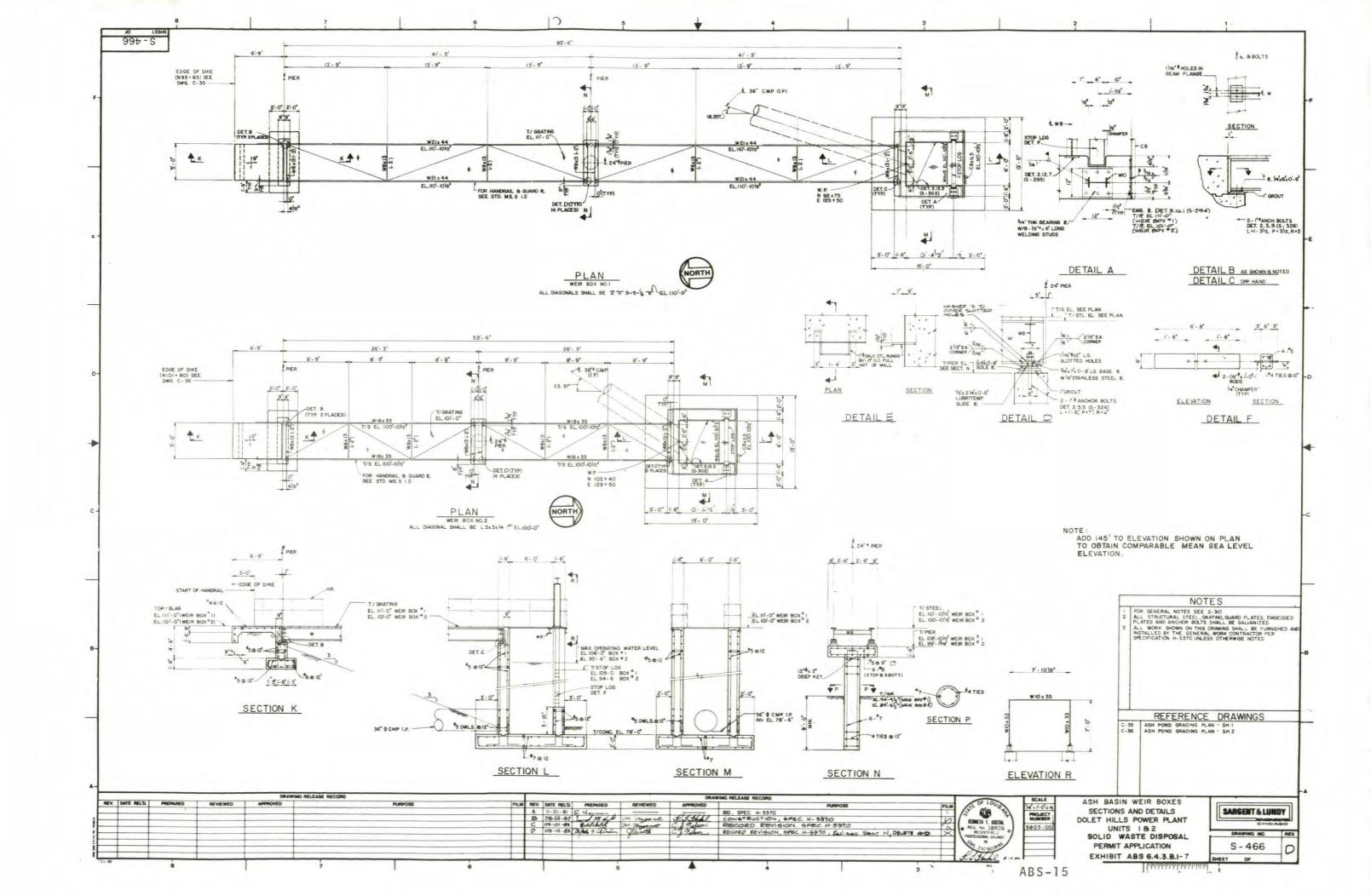
SUBSURFACE CONDITIONS SHOWN IN SECTIONS 3 AND 4.
ARE APPROXIMATE AND SHOULD BE VERTIED IN THE FIELD.

N.

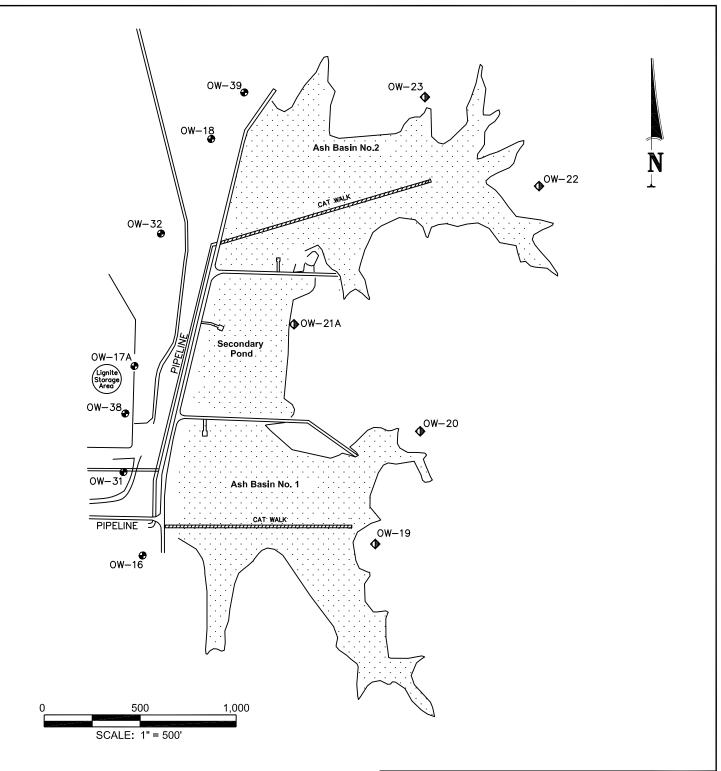
ASH BASINS & SECONDARY POND
SECTIONS AND DETAILS (SHEET 20F3)
DOLET HILLS POWER PLANT
UNITS I & 2
SOLID WASTE DISPOSAL











Legend

⊕ 0W−16

Zone 4 Compliance Monitoring Well Location

♦ 0W-23

Zone 4 Background Monitoring Well Location

.

Permitted Facility



Dolet Hills Power Station

Zone 4 Monitoring Wells Location Map

DeSoto Parish, Louisiana



Dwg. No.:	01-16-0159-A004
Date:	10/4/16
Approved:	JM
Checked:	JM
Drawn:	JP

Figure 2



CREATE AMAZING.

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