



# History of Construction

## Brame Bottom Ash Pond



CLECO Corporation

Rodemacher Unit 2  
Project No. 90965

Revision 0  
10/14/2016



# **History of Construction**

## **Brame Bottom Ash Pond**

**prepared for**

**CLECO Corporation  
Rodemacher Unit 2  
Rapides Parish, Louisiana**

**Project No. 90965**

**Revision 0  
10/14/2016**

**prepared by**

**Burns & McDonnell Engineering Company, Inc.  
Kansas City, Missouri**

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## INDEX AND CERTIFICATION

CLECO Corporation  
History of Construction  
Brame Bottom Ash Pond  
Project No. 90965

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### Certification

I hereby certify, as a Professional Engineer in the state of Louisiana, that the information in this document was assembled under my direct personal charge. This report is not intended or represented to be suitable for reuse by the CLECO Corporation or others without specific verification or adaptation by the Engineer.

Randell Sedlacek  
Randell L Sedlacek, P.E.  
Louisiana License #38408

Date: 10/14/16

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## LIST OF ABBREVIATIONS

<u>Abbreviation</u>	<u>Term/Phrase/Name</u>
BMcD	Burns & McDonnell
Brame	Brame Energy Center
CCR	Coal Combustion Residual
CFR	Code of Federal Regulations
CLECO	CLECO Corporation
CY	Cubic Yards
EPA	Environmental Protection Agency
GPM	Gallons per Minute
HUC	Hydrologic Unit Code
LSU	Louisiana State University
U.S.C	United States Code
USGS	United States Geological Survey

## 1.0 INTRODUCTION

On April 17, 2015, the Environmental Protection Agency (EPA) issued the final version of the federal Coal Combustion Residual (CCR) Rule to regulate the disposal of CCR materials generated at coal-fired units. The rule will be administered as part of the Resource Conservation and Recovery Act [RCRA, 42 United States Code (U.S.C.) §6901 et seq.], using the Subtitle D approach.

The existing CCR surface impoundments at CLECO Corporation's (CLECO's) Brame Energy Center (Brame) are subject to the CCR Rule and as such CLECO must compile a History of Construction for each CCR surface impoundment per 40 CFR §257.73(c). This report serves as the History of Construction for the Brame Bottom Ash Pond.

This history of construction is in addition to, not in place of, any other applicable site permits, environmental standards, or work safety practices.

## 2.0 PLAN OBJECTIVES

Per 40 CFR §257.73(c), the History of Construction must contain, to the extent feasible, the following items:

- The name and address of the owner/operator of the CCR unit, the name of the CCR unit, and the identification number of the CCR unit
- The location of the CCR unit on most recent United States Geological Survey (USGS) 7½ minute or 15 minute topographical map
- A statement of the purpose for which the CCR unit is being used
- The name and size of watershed within which the CCR unit is located
- A description of the physical and engineering properties of the foundation and abutment materials on which the CCR unit is constructed
- A statement of the type, size, range, and physical and engineering properties of the materials used in constructing each zone or stage of the CCR unit; the method of site preparation and construction of each zone or stage of the CCR unit; and the approximate dates of construction of each successive stage of construction of the CCR unit.
- Detailed dimensional drawings of the CCR Unit, including the following:
  - Plan view and cross sections of the length and width of the CCR unit
  - Foundation improvements
  - Drainage provisions, spillways, diversion ditches, outlets
  - Instrumentation locations
  - Slope protection
  - Normal operating pool surface elevation
  - Maximum pool surface elevation following peak discharge from the inflow design flood
  - Expected maximum depth of CCR within the unit
  - Any identifiable natural or manmade features that could adversely affect operation of the CCR unit due to malfunction or mis-operation
- A description of the type, purpose, and location of existing instrumentation
- Area-capacity curves for the CCR unit
- A description of each spillway and diversion design features and capacities and calculations used in their determination
- The construction specifications and provisions for surveillance, maintenance, and repair of the CCR unit
- Any record or knowledge of structural instability of the CCR unit

### 3.0 HISTORY OF CONSTRUCTION

Section	CCR Rule Description	Included	Information	Source
40 CFR §257.73 (c)(1) (i)	Name and address of the owner/operator of the CCR unit	Y	Cleco Corporation 2030 Donahue Ferry Road P.O. Box 5000 Pineville, LA 71361-5000	Owner
	Name of the CCR unit	Y	Bottom Ash Pond	Owner
	Identification number of the CCR unit	Y	P-0005 (permit number)	Owner
40 CFR §257.73 (c)(1) (ii)	Location of the CCR unit on most recent United States Geological Survey (USGS) 7½ minute or 15 minute topographical map	Y	See Appendix A	USGS Map
40 CFR §257.73 (c)(1) (iii)	Statement of the purpose for which the CCR unit is being used	Y	The pond receives bottom ash, economizer ash, sluice water, and other process flows from Rodemacher Unit 2. CCR material is sluiced to the pond at 2.16 MGD for approximately 12 hours each day. Overflow from the adjacent Fly Ash Pond is also pumped directly to the Bottom Ash Pond.	Owner
40 CFR §257.73 (c)(1) (iv)	Name and size of watershed within which the CCR unit is located	Y	HUC12 = 111402070703 Jacks Creek Watershed Area = 9,407 acres  Only approximately 46 acres of this overall watershed actually contributes runoff to the Bottom Ash Pond.	HUC 12 Mapping LSU AGCenter.com
40 CFR §257.73 (c)(1) (v)	Description of the physical and engineering properties of the foundation and abutment materials on which the CCR unit is constructed	Y	Foundation Soils include soft to medium stiff clay and silty clay.  See Appendix C	Permit
40 CFR §257.73 (c)(1) (vi)	Statement of the type, size, range, and physical and engineering properties of the materials used in constructing each zone or stage of the CCR unit	Y	Embankment constructed of on-site material and includes minimum 3-ft compacted clay. 3-ft compacted clay liner constructed with high-plasticity clay with average Plasticity Index of 41 and average Liquid Limit of 62.  See Appendices C & D	Permit
	The method of site preparation and construction of each zone or stage of the CCR unit	Y	Embankment constructed with 3:1 side slopes. Liner was constructed in 8-10 in. horizontal lifts compacted with sheepfoot compaction.  See Appendices C & D	Permit
	The approximate dates of construction of each successive stage of construction of the CCR unit		Began construction in 1978, operational in 1982.  No major construction modifications have been made since.	Permit Drawings / Owner
40 CFR §257.73 (c)(1) (vii)	Detailed dimensional drawings including the following:  Plan view and cross sections of the length and width of the CCR unit	Y	See Appendix E	Permit
	Foundation improvements	N	N/A	
	Drainage provisions, spillways, diversion ditches, outlets	Y	24-in CMP, invert EL = 102.6 (discharges to ditch on NW embankment via pumping)	Owner / Design Drawings

Section	CCR Rule Description	Included	Information	Source
	Instrumentation locations	Y	See Appendix E See Appendix F	Permit
	Slope protection		Exterior Slope: 3:1, vegetated Interior Slope: 3:1, vegetated	Design Drawings
	Normal operating pool surface elevation		Normal operating level between EL 93-94	Owner
	Maximum pool surface elevation following peak discharge from the inflow design flood		Maximum pool surface level at EL 100.5 following peak discharge from the inflow design flood, assuming pond is 50% full of ash to the top of the dike and initial water level of EL 94.	Inflow Design Flood Control System Plan, Oct. 2016
	Expected maximum depth of CCR within the unit		At EL 105, depth of CCR is approximately 20 feet.	Measured in CAD based on Construction Drawings / aerial imagery
	Any identifiable natural or manmade features that could adversely affect operation of the CCR unit due to malfunction or mis-operation	Y	Three pumps capable of 5,000 GPM operate on a float to maintain consistent water levels in the pond.	Owner
40 CFR §257.73 (c)(1) (viii)	Description of the type, purpose, and location of existing instrumentation	Y	Pumps - control pond overflow  Monitoring wells - monitor uppermost aquifer (compliance and background monitoring). See Appendix F for location.  Surface water level gauge (measured manually)  See Appendix F for locations and additional information	Permit / Owner
40 CFR §257.73 (c)(1) (ix)	Area-capacity curves for the CCR unit	Y	See Appendix B	Measured in CAD based on Construction Drawings / aerial imagery
40 CFR §257.73 (c)(1) (x)	Description of each spillway and diversion design features and capacities and calculations used in their determination	Y	Perimeter interceptor ditch off of NW embankment.  See Appendix D for details	Permit
40 CFR §257.73 (c)(1) (xi)	Construction specifications Provisions for surveillance, maintenance, and repair of the CCR unit	N Y	Not found in records review  Weekly and Annual Inspections per 40 CFR §257.83.	
40 CFR §257.73 (c)(1) (xii)	Any record or knowledge of structural instability of the CCR unit	N	N/A	

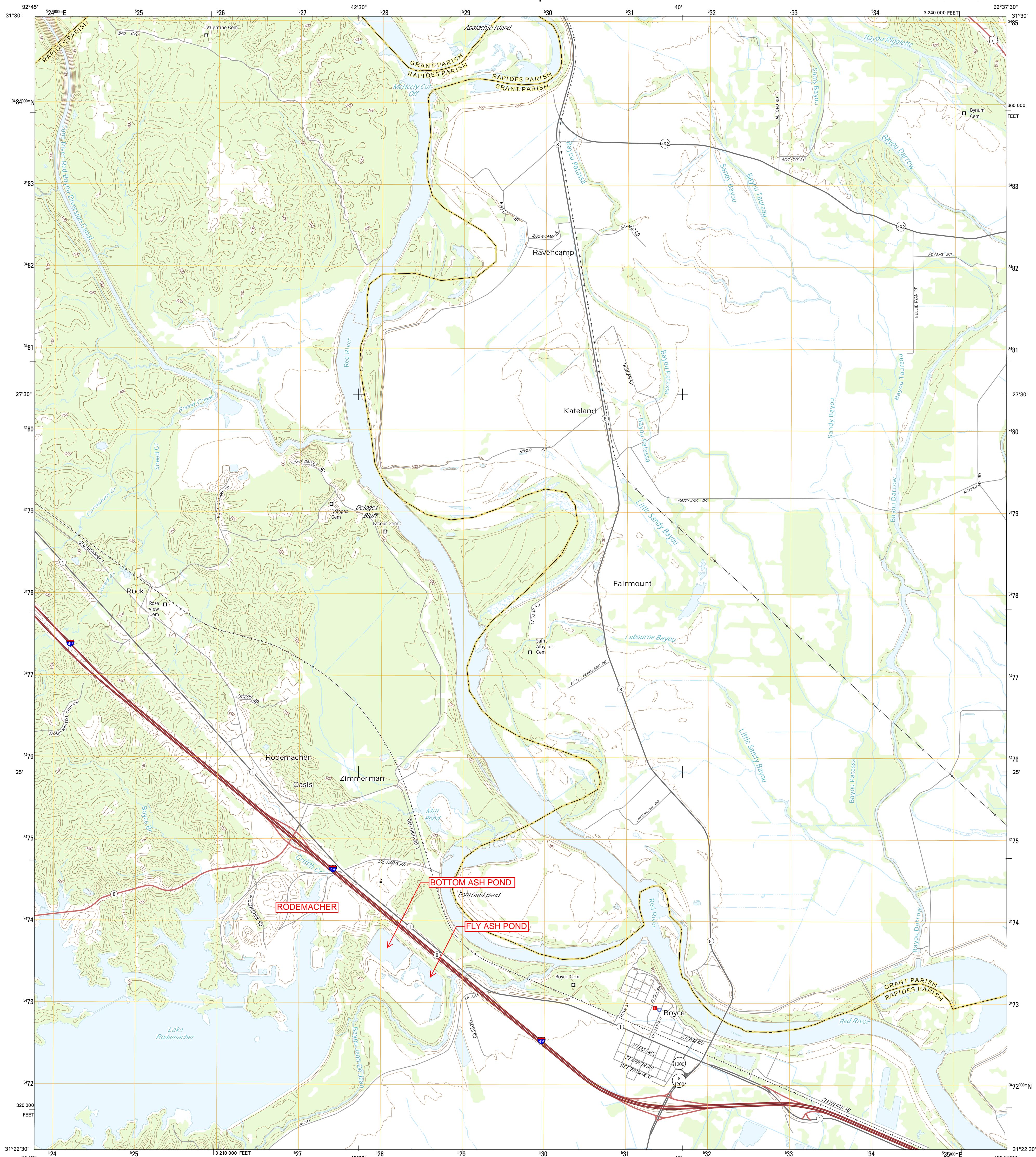
**APPENDIX A - USGS TOPOGRAPHICAL MAP**



U.S. DEPARTMENT OF THE INTERIOR  
U.S. GEOLOGICAL SURVEY



BOYCE QUADRANGLE  
LOUISIANA  
7.5-MINUTE SERIES



Produced by the United States Geological Survey

North American Datum of 1983 (NAD83)  
World Geodetic System of 1984 (WGS84), Projection and  
1000-meter grid: Universal Transverse Mercator, Zone 15R  
10,000-foot ticks: Louisiana Coordinate System of 1983 (north  
zone)

This map is not a legal document. Boundaries may be  
generalized for this map scale. Private lands within government  
reservations may not be shown. Obtain permission before  
entering private lands.

Imagery: NAIP, June 2013  
Roads: HERE, ©2013 - 2014  
Names: GNIS, 2015  
Hydrography: National Hydrography Dataset, 2013  
Contour: National Elevation Dataset, Ellipsoid Height, 10' (15' grid)  
Boundaries: Multiple sources; see metadata file 1972 - 2015  
Public Land Survey System: BLM, 2015

MN  
0° 10' 19.5 MILES  
0° 10' 3 MILS  
UTM GRID AND 2015 MAGNETIC NORTH  
DECLINATION AT CENTER OF SHEET

U.S. National Grid  
100,000 m Square ID  
WO  
Grid Zone Designation  
15R

SCALE 1:24 000  
1 0.5 0 1 KILOMETERS  
1000 500 0 1000 METERS  
1 0.5 0 1 MILES  
1000 0 1000 2000 FEET

CONTOUR INTERVAL 10 FEET  
NORTH AMERICAN VERTICAL DATUM OF 1988

This map was produced to conform with the  
National Geospatial Program US Topo Product Standard, 2011.  
A metadata file associated with this product is draft version 0.6.18



QUADRANGLE LOCATION

ROAD CLASSIFICATION  
Expressway ————— Local Connector —————  
Secondary Hwy ————— Local Road —————  
Ramp ————— 4WD —————  
Interstate Route ■ US Route ○ State Route

1	2	3
4		5
6	7	8
7	Gardner	Rapides

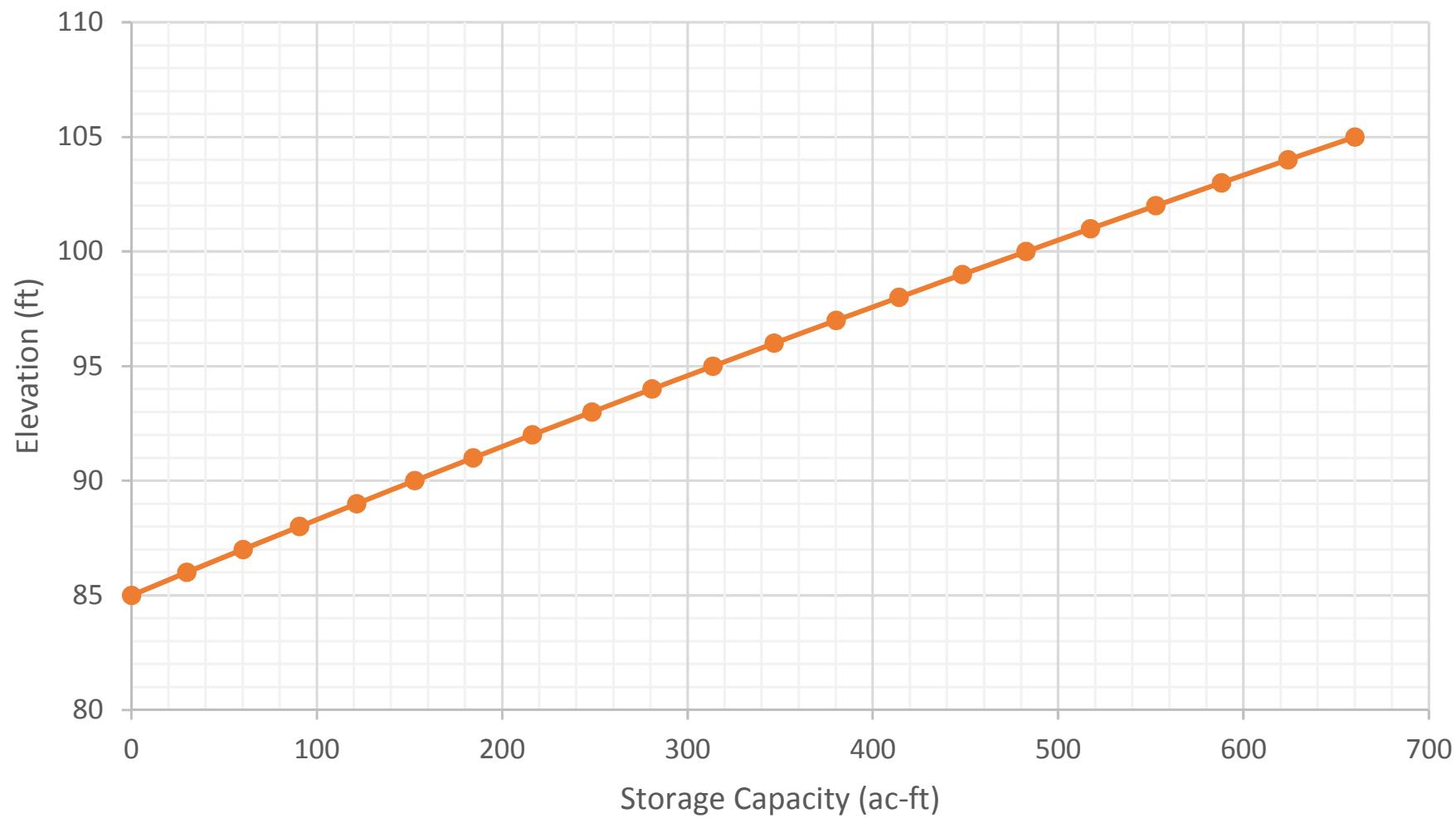
ADJOINING QUADRANGLES

BOYCE, LA  
2015

NSN 76-3016368754  
NGA REF NO. USGS X 24 K 5 12

## **APPENDIX B - AREA-CAPACITY CURVE**

## Brame - Bottom Ash Pond



## **APPENDIX C - GEOLOGIC DATA**

## S21.D. FACILITY GEOLOGY

### 1. INFORMATION REQUIRED FOR TYPE I AND II FACILITIES

#### 1.a. Isometric Profiles and Cross-Sections

Exhibits 13 and 14 present the generalized soil conditions beneath the Bottom Ash Pond. The depth to ground water varies from 6 to 10 feet below grade. There is a very soft to medium stiff clay which extends to 20 feet (terminal depth of borings) in all of the borings except Boring 244. In that boring, the clay extended to 12 feet with a silty sand to sandy silt beneath.

#### 1.b. Soil Boring Logs

Exhibits 13 and 14 presents generalized logs of the soil.

#### 1.c. Soil Test Results

The laboratory coefficient of permeability for the in situ clay varies from  $1.3 \times 10^{-8}$  to  $3.5 \times 10^{-8}$  cm/sec. As was shown in Exhibit 13, the approximate limit of the in situ clay barrier is about midway of the Bottom Ash Pond. A 3-foot thick compacted clay layer was placed over the exposed granular soils on the bottom of the Bottom Ash Pond. The extent of the clay blanket was determined in the field by ensuring that the in situ clay had a minimum thickness of 3 feet. Laboratory permeability tests on recompacted samples of the clay varied from  $1.1 \times 10^{-7}$  to  $2.1 \times 10^{-8}$  cm/sec. and the Plasticity Index averaged 41 with an average liquid limit of 62 which classifies the soil as CH according to the Unified Soil Classification System. The clay liner was placed in horizontal lifts of 8 to 10 inches and was compacted with "sheeps foot" compaction equipment. The 3-foot compacted clay liner coupled with the in situ clay layer should form an effective barrier to liquid waste migration to the ground water.

A summary of the laboratory test results is presented in Appendix F.

#### 1.d. Geologic Cross-Sections

Exhibit 5 contains geologic cross-sections which extend to a depth greater than 200 feet below ground surface.

#### 1.e. Faults

There has been no information obtained which would indicate that there exist faults at the facility.

#### 1.f. Seismic Impact Zone

The facility is not located within a seismic impact zone.



Pond, the Coal Sedimentation Pond, and the Unit 2 Metal Cleaning Waste Pond are situated on the Terrace aquifer, while the Fly Ash Pond, Bottom Ash Pond, and Ash Management Area are situated on the aquifer recharge area for the Alluvial aquifer.

- e. if the facility is located in a flood plain, a plan to ensure that the facility does not restrict the flow of the 100-year base flood or significantly reduce the temporary water-storage capacity of the flood plain, and documentation indicating that the design of the facility is such that the flooding does not affect the integrity of the facility or result in the washout of solid waste.

The Fly Ash Pond is the only facility that is constructed within an area previously permitted through the Army Corps of Engineers (COE) under permit number LMNOD-SP dated March 29, 1977. Cleco currently holds a solid waste permit from the LDEQ for this area to manage ash for future plant expansions.

**D. Facility Geology.** Standards governing facility geology are contained in LAC 33:VII.709.C (Type I and II facilities), LAC 33:VII.717.D (Type I-A and II-A facilities), and LAC 33:VII.719.D (Type III facilities).

**l. The following information regarding geology is required for Type I and Type II facilities:**

- a. isometric profile and cross-sections of soils, by type, thickness, and permeability;

Isometric soil profiles and geologic cross sections have been constructed for the facilities from available data. The locations of the profiles for the cross sections are shown in Appendix G. Five (5) isometric soil profiles and sixteen (16) geologic cross sections, A-A' through P-P', were constructed from available data and are included in this appendix. Historical geologic cross sections constructed for the facilities are included in Appendix H.

- b. logs of all known soil borings taken on the facility and a description of the methods used to seal abandoned soil borings;

A copy of the logs of soil borings is included in Appendix I. Please note that the soil boring logs performed by Aquaterra (2004) and Eagle (2005) are included in this appendix. Soil boring logs were not available for the drilling activities performed by Sargent & Lundy (1981); however, geologic cross sections illustrating these logs are available and are included. Design and construction of the units began before the Louisiana Solid Waste Rules and Regulations were established and the units were initially under interim status prior to the standard permits being issued.

Abandoned soil borings were sealed in accordance with applicable methods at the time of drilling according to available records reviewed. Since May 1993, soil

borings have been sealed in accordance with applicable portions of "Construction of Geotechnical Boreholes and Groundwater Monitoring Systems Handbook" dated December 2000 (LDEQ and LDOTD, 2000).

- c. **results of tests for classifying soils (moisture contents, Atterberg limits, gradation, etc.), measuring soil strength, and determining the coefficients of permeability, and other applicable geotechnical tests;**

A copy of available geotechnical testing used for soil classification is included in Appendix I.

- d. **geologic cross-section from available published information depicting the stratigraphy to a depth of at least 200 feet below the ground surface;**

A fence diagram illustrating Rapides Parish geology to approximately 3,000 feet below ground surface is included as Appendix F. (Plate 4, Water Resources of Rapides Parish, Louisiana, Water Resources Bulletin No. 8, Department of Conservation, Louisiana Geological Survey, and Louisiana Department of Public Works, April 1966).

- e. **for faults mapped as existing through the facility, verification of their presence by geophysical mapping or stratigraphic correlation of boring logs. If the plane of the fault is verified within the facility's boundaries, a discussion of measures that will be taken to mitigate adverse effects on the facility and the environment;**

There are no known faults within the facility or within one mile of the perimeter of the facility. The review of available published information did not reveal information on faulting near the facility.

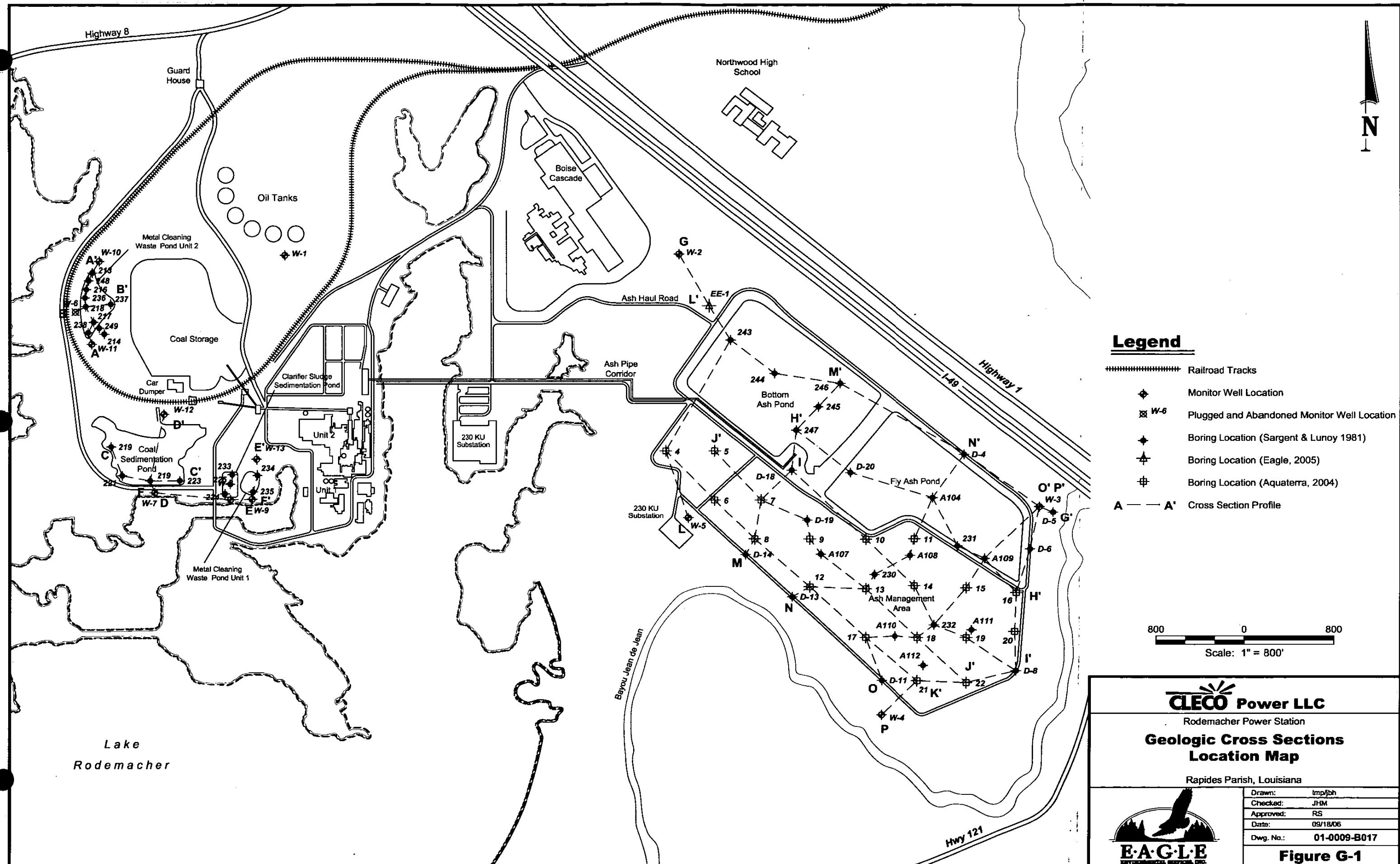
- f. **for a facility located in a seismic impact zone, a report with calculations demonstrating that the facility will be designed and operated so that it can withstand the stresses caused by the maximum ground motion, as provided in LAC 33:VII.709.C.2; and**

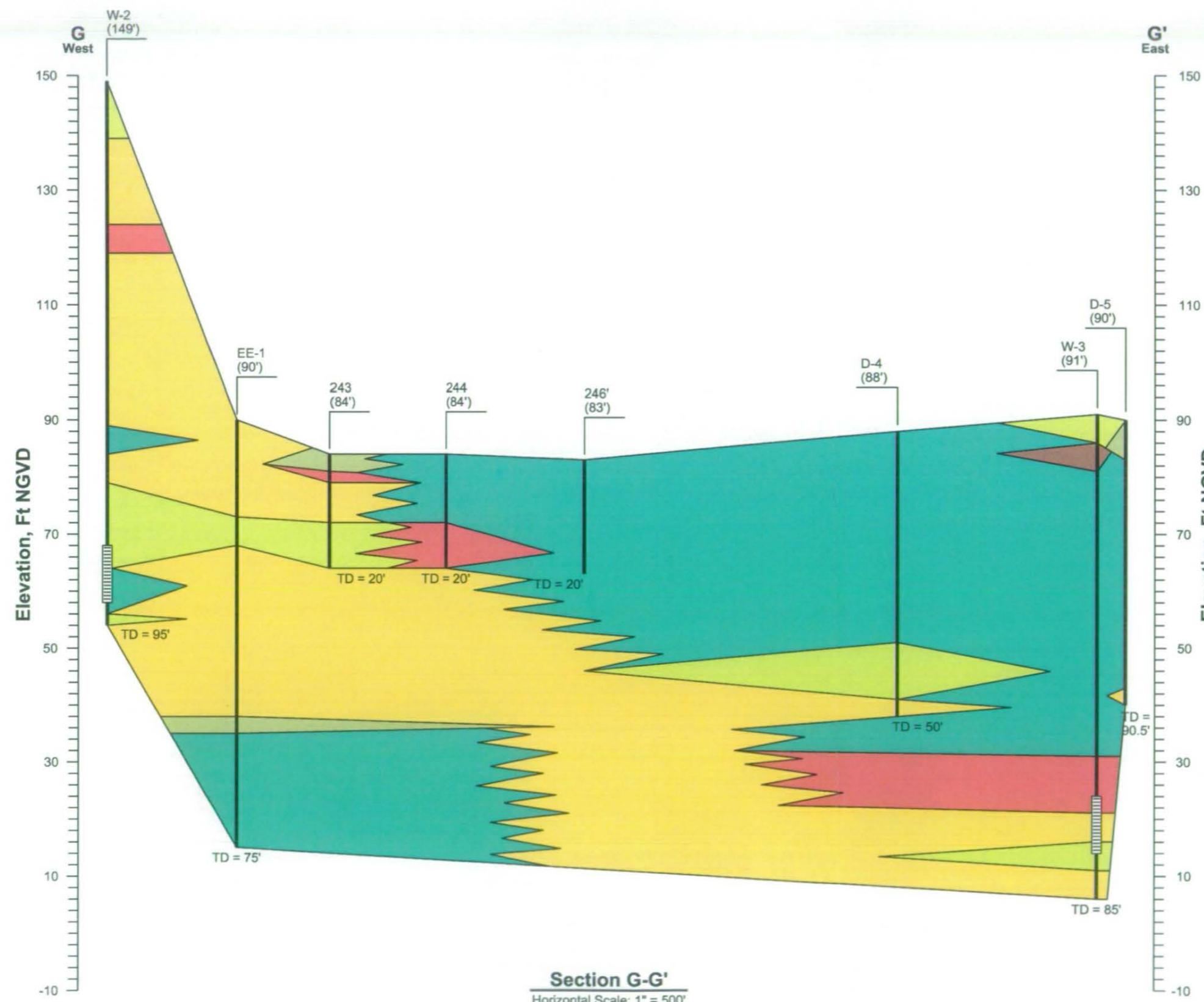
Not applicable. Review of the "Seismicity Map of the State of Louisiana" (Map MF-1081, Stover and others, United States Geological Survey, 1987) does not indicate seismic activity in the area of the Rodemacher Power Station.

- g. **for a facility located in an unstable area, a demonstration of facility design as provided in LAC 33:VII.709.C.3.**

Not applicable. The RPS is not located in an unstable area.

2. **The following information regarding geology is required by Type III wood waste, and construction/demolition-debris facilities:**



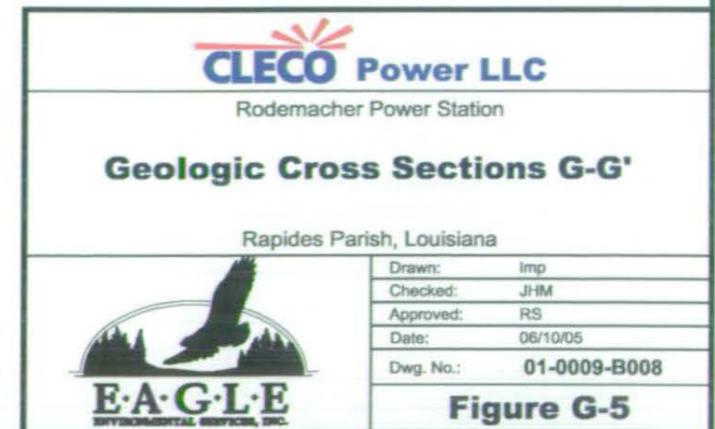


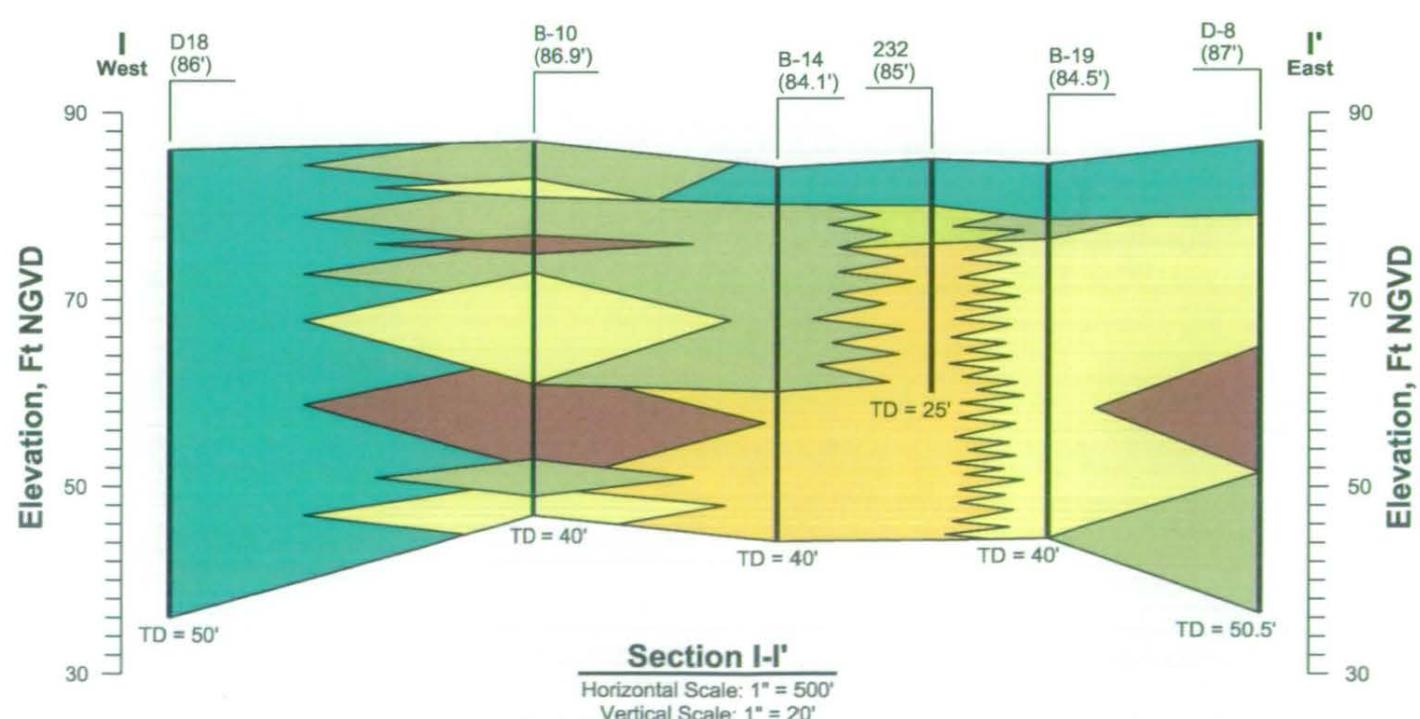
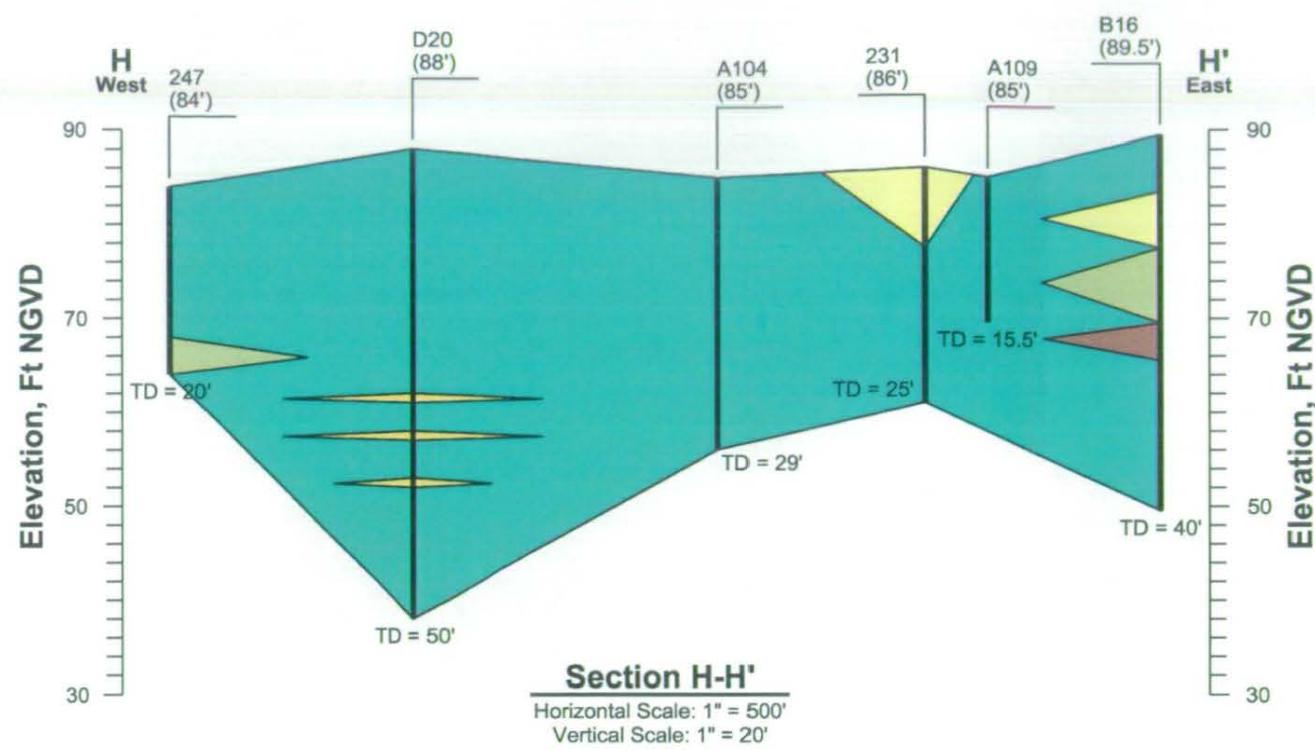
### Legend

- Sand
- Silty Sand / Sandy Silt / Silt
- Sandy Clay
- Silty Clay
- Clay
- Clayey Silt
- Clayey Sand
- Screen Interval
- (114') Elevation, Ft NGVD
- TD Total Depth

### Note:

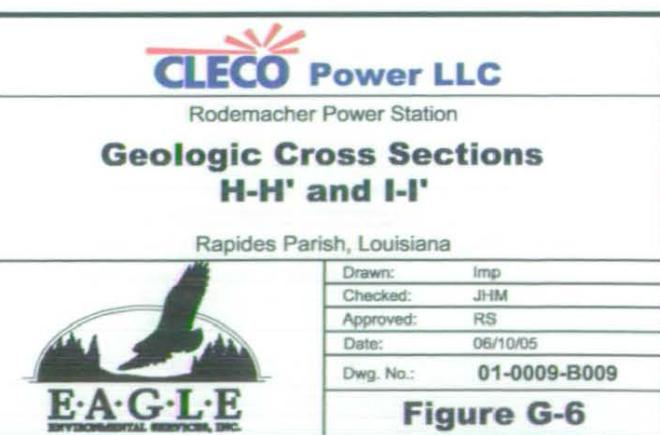
Stratigraphy between boring are inferred. Actual conditions may vary.

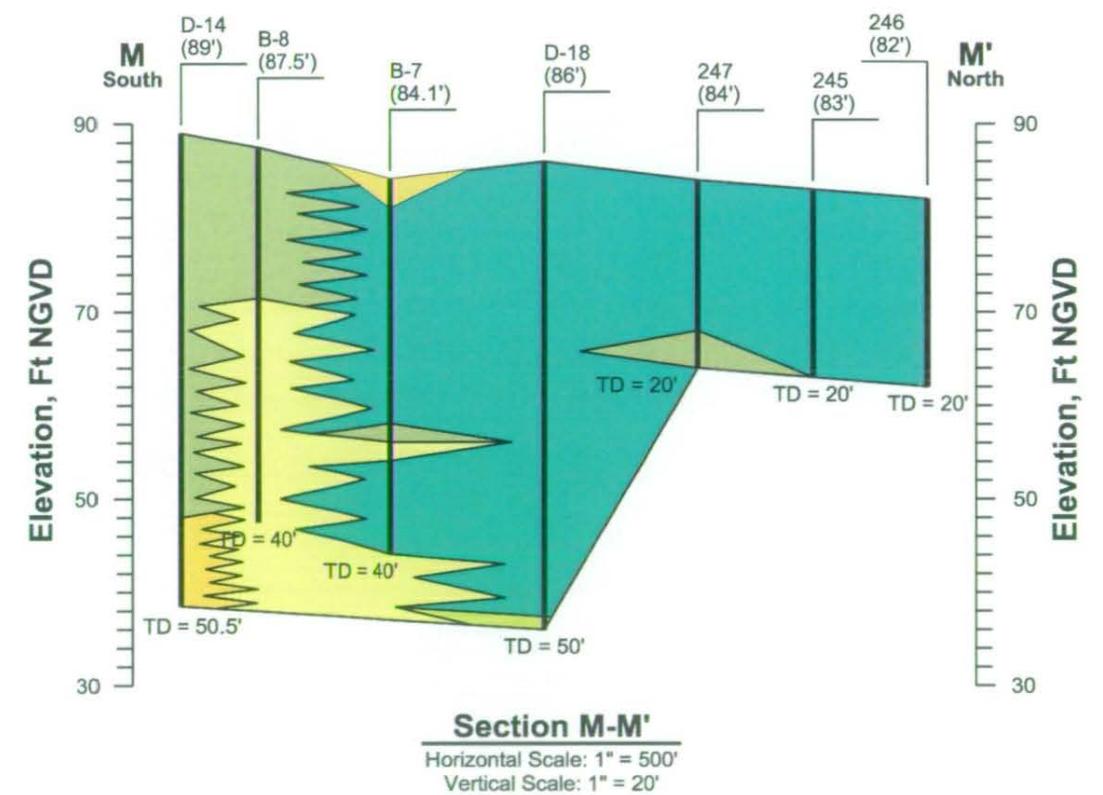




<b>Legend</b>	
Sand	(Yellow)
Silty Sand / Sandy Silt / Silt	(Light Yellow)
Sandy Clay	(Light Green)
Silty Clay	(Green)
Clay	(Teal)
Clayey Silt	(Brown)
Clayey Sand	(Red)
Screen Interval	(Hatched)
(114') Elevation, Ft NGVD	
TD Total Depth	

**Note:**  
Stratigraphy between boring are inferred. Actual conditions may vary.

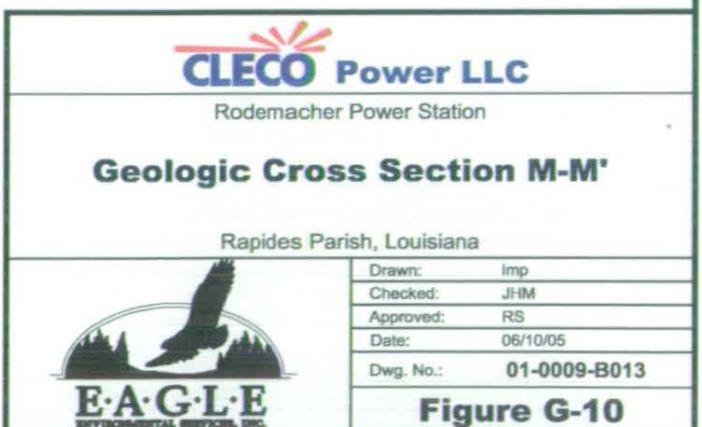


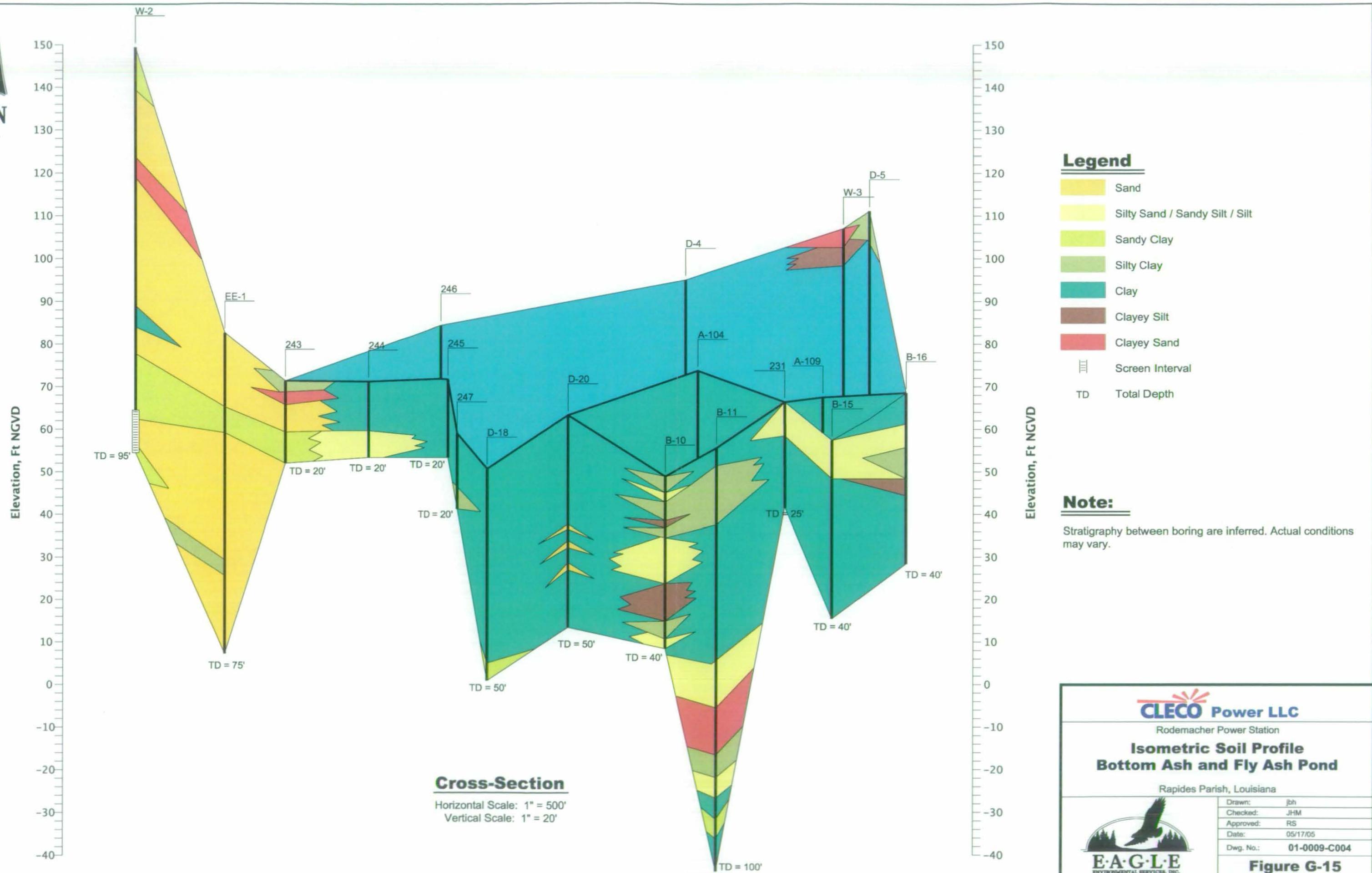


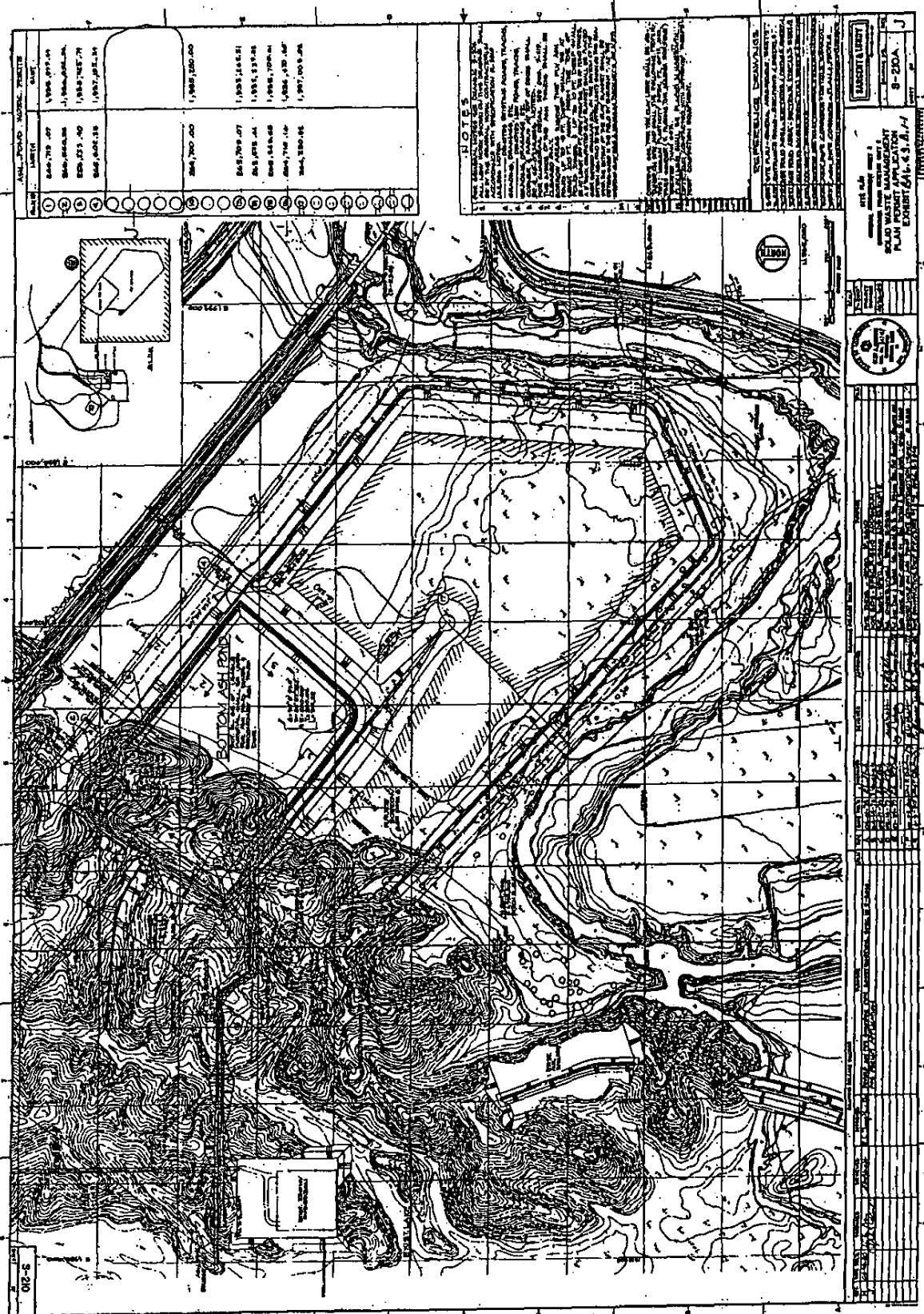
<b>Legend</b>	
	Sand
	Silty Sand / Sandy Silt / Silt
	Sandy Clay
	Silty Clay
	Clay
	Clayey Silt
	Clayey Sand
	Screen Interval
(114')	Elevation, Ft NGVD
TD	Total Depth

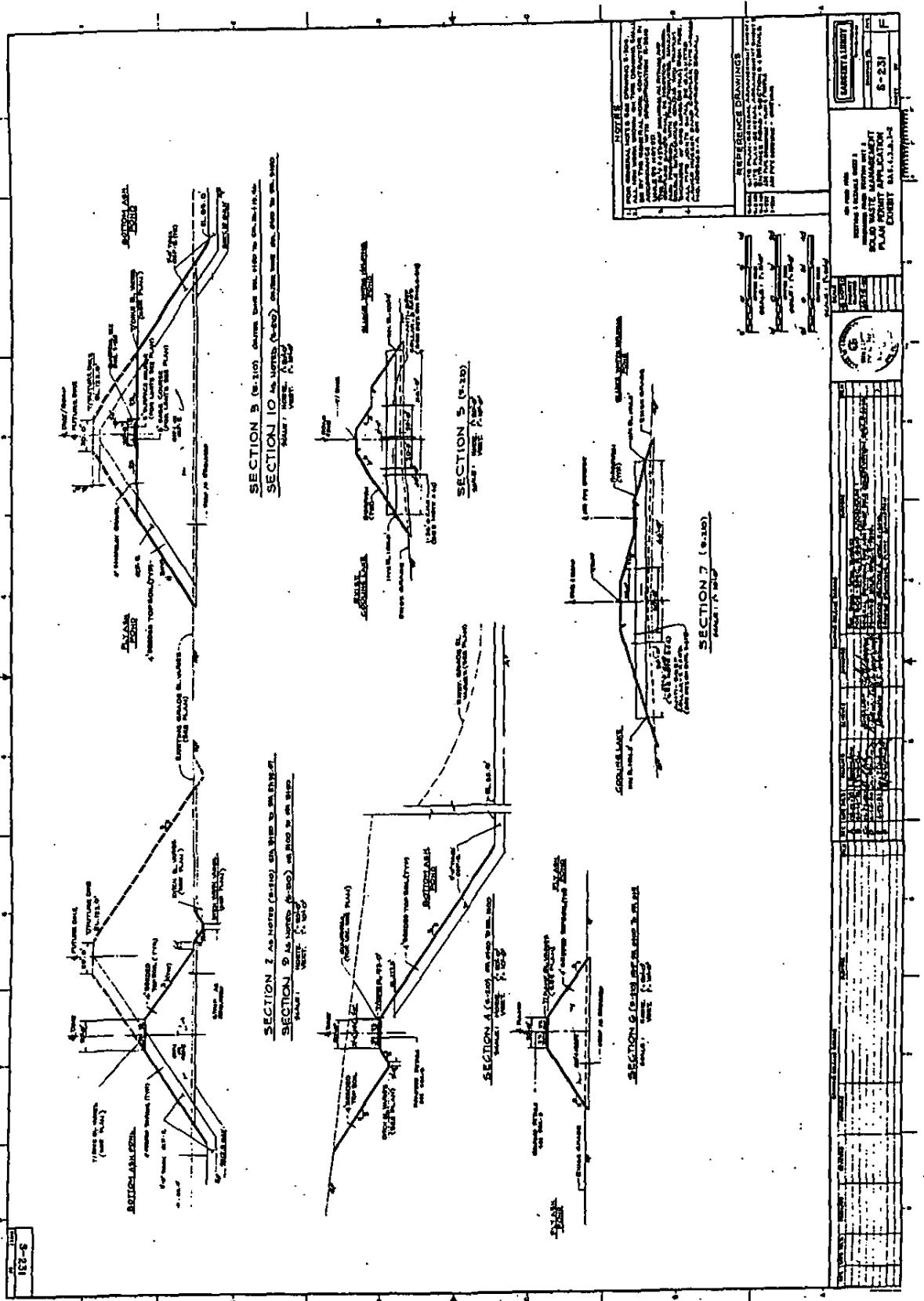
**Note:**

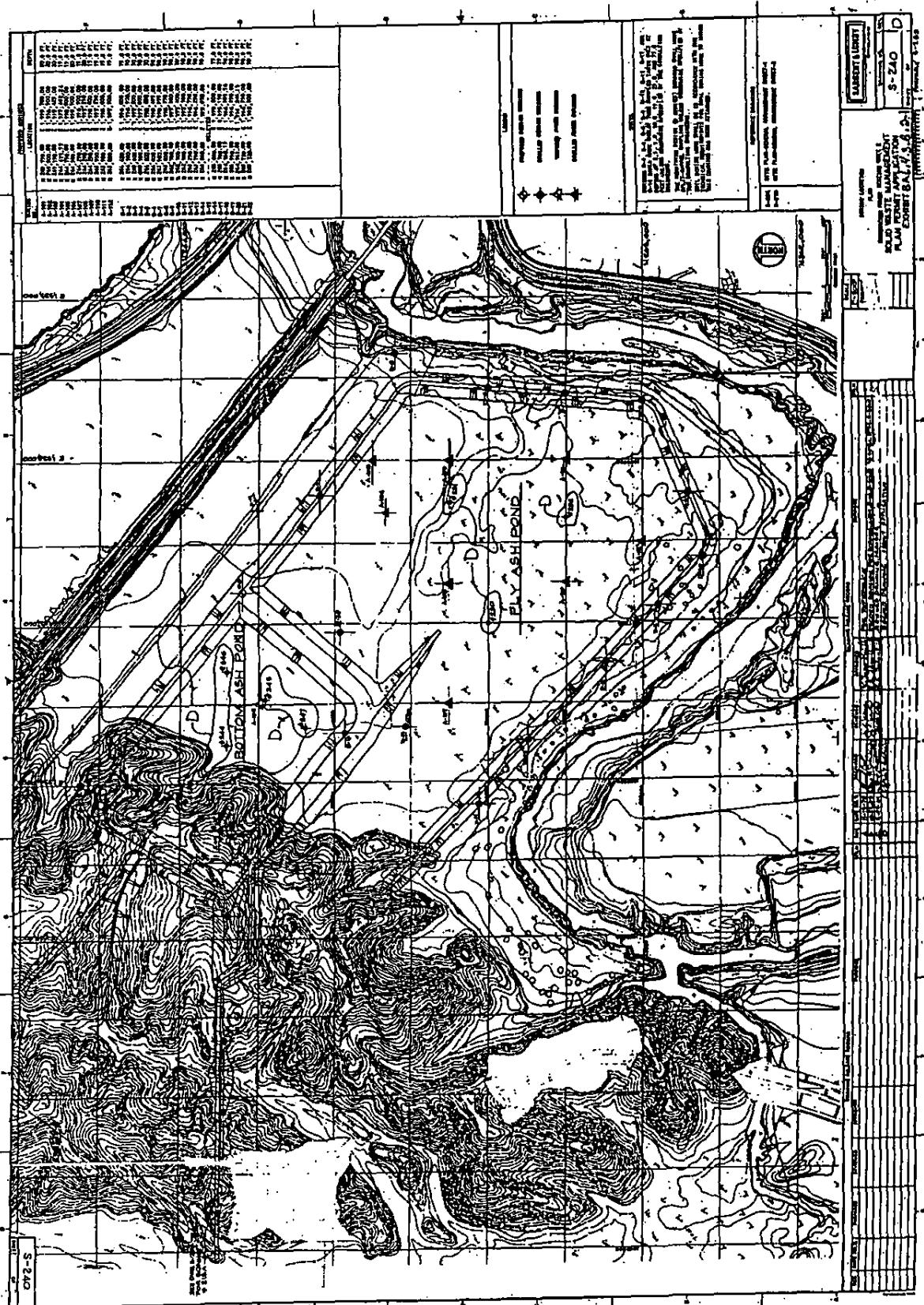
Stratigraphy between borehole are inferred. Actual conditions may vary.

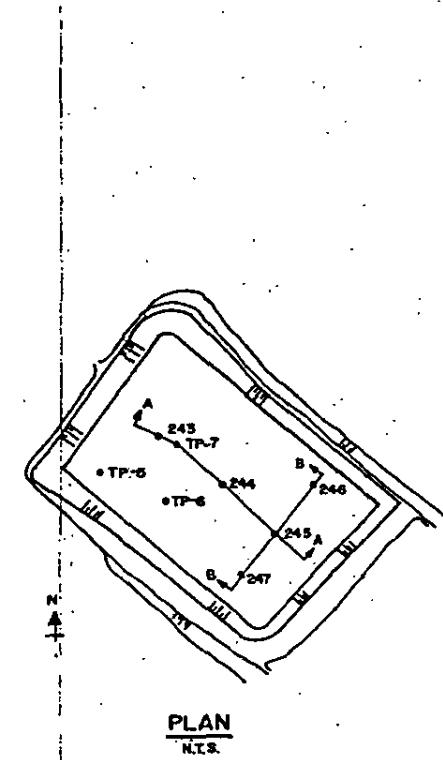
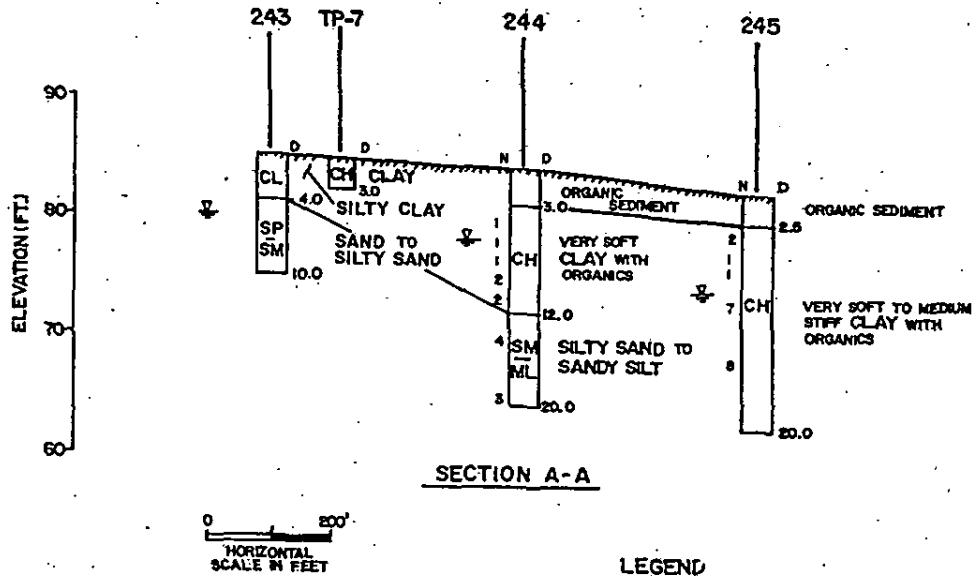








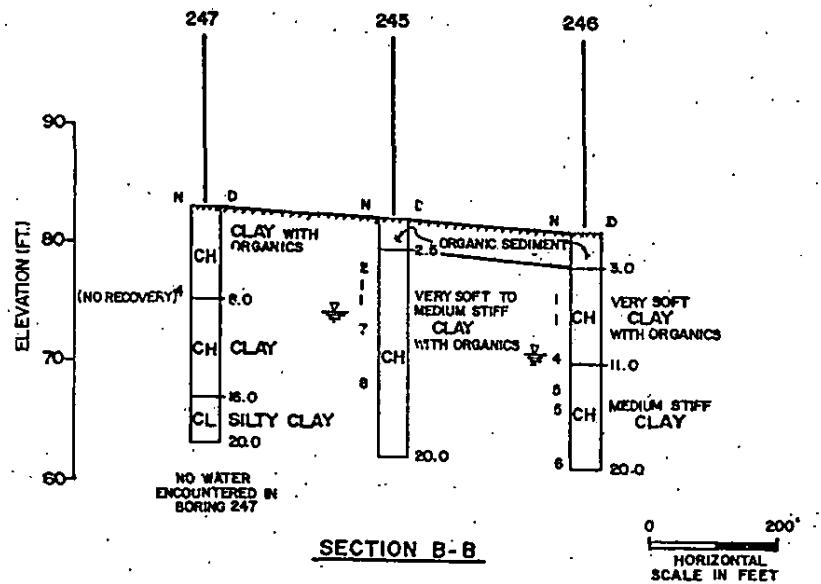




GENERALIZED SUBSURFACE DIAGRAM -  
SECTION A-A  
BOTTOM ASH POND

RODEMACHER POWER STATION UNIT 2  
SOLID WASTE MANAGEMENT PLAN  
PERMIT APPLICATION

EXHIBIT BA 6.4.3.B.2-2



LEGEND

- D = DEPTH IN FEET
- N = STANDARD PENETRATION TEST, BLOWS PER FOOT
- ▽ = GROUND WATER LEVEL
- = BOTTOM OF POND (TOP OF BORINGS)

NOTE

1. FOR BORING LOCATION PLAN, SEE SECTION A-A.

GENERALIZED SUBSURFACE DIAGRAM — SECTION B-B. BOTTOM ASH POND
RODEMACHER POWER STATION UNIT 2 SOLID WASTE MANAGEMENT PLAN PERMIT APPLICATION
EXHIBIT BA 6.4.3.B.2-3

TABLE BA 6.4.3.B.4-1  
SUMMARY OF LABORATORY TESTS  
BOTTOM ASH POND

Feature	Boring No. Sample No.	Bottom of Sample Depth, Ft.	Particle Size Analysis (% Passing)				Atterberg Limits (1)			Unified Soil Classification Symbol	Natural Water- Content (%) (4)	Dry Density lbs/ft <sup>3</sup>	Laboratory Permeability (5) cm/sec
			No. 4 Sieve	No. 10 Sieve	No. 40 Sieve	No. 200 Sieve	Liquid Limit (%)	Plastic Limit (%)	Plasticity Index				
Bottom Ash Pond	243	1.5			91		47	20	27	CL SP-CH	21.8		
		3.0			89		47	19	28		21.7		
		7.5			9		21	N.P.	N.P.		24.6		
244, 2	4.5		96		69	22	47			CH	97.8	?	
	6.0		97		81	23	58				78.1		
	7.5		94		77	23	54				79.2		
	9.0		96		69	22	47				63.3		
	10.5		97		71	23	48				65.4		
	15.0		50		20	17	3				18.2		
	20.0		50		19	N.P.(6)	N.P.				18.0		
	245, 2	4.0	93		81	22	59						
245, 3	5.5		94		74	22	52			CH			
	7.0		100		65	21	44						
	10.0		98		82	23	57						
	15.0		98		-	-	-				63.3		
	20.0												
	246, 2	6.5	95		70	23	47				82.3		
246, 3	8.0		97		60	21	39				98.2		
	9.5		95		85	23	62				40.9		
	11.0		?		69	22	47				32.6	78.0	$3.3 \times 10^{-6}$
	15.0		99		64	22	42				32.5		
	20.0		100		69	22	47				39.6		
	247, 2	4.0	100		78	21	57						
247, 3	6.0		100		67	26	63			CH	45.0		$2.3 \times 10^{-6}$
	10.0		98		54	20	34				66.0		$3.3 \times 10^{-6}$
	15.0		87		70	23	47				60.8		
	20.0		98		40	20	20				30.6		
											61.8		

TABLE BA 6.4.3.B.4-1 (Continued)

SUMMARY OF LABORATORY TESTS  
BOTTOM ASH POND

Feature	Boring No. Sample No.	Bottom of Sample Depth, Ft.	Particle Size Analysis (% Passing) (2)				Atterberg Limits (3)			Unified Soil Classification Symbol	Natural Water Content (%) (4)	Dry Density lbs/ft <sup>3</sup>	Laboratory Permeability (5) cm/sec
			No. 4 Sieve	No. 10 Sieve	No. 40 Sieve	No. 200 Sieve	Liquid Limit (%)	Plastic Limit (%)	Plasticity Index				
Bottom Ash Pond (CONT'D.)	TP-3, 1	1.0	-	-	-	96	60	20	40	CH	26.4	-	-
	2	2.0	-	-	-	96	64	21	43	CH	28.0	-	-
	3	3.0	-	-	-	99	60	21	39	CH	27.6	-	-
TP-4, 1	1	1.0	-	-	-	99	65	20	45	CH	24.8	-	-
	2	2.0	-	-	-	99	61	22	39	CH	25.1	-	-
	3	3.0	-	-	-	99	60	21	39	CH	22.4	-	-
TP-7, 1	1	1.0	-	-	-	93	58	21	37	CH	26.1	-	-
	2	2.0	-	-	-	99	70	24	46	CH	33.4	-	-
	3	3.0	-	-	-	93	65	22	43	CH	32.8	-	-
230, 2	3	3.0	100	100	100	100	58	20	38	CH	25.6	-	-
	4	6.0	-	-	-	-	-	-	-	-	-	-	-
	6	9.0	-	-	-	-	-	-	-	-	-	-	-
	8	13.0	-	-	100	66	27	19	8	CL	27.4	-	-
	231, 2	3.0	-	-	-	37	N.P. <sup>(6)</sup>	N.P.	N.P.	SM	17.7	-	-
	4	6.0	-	-	-	15	N.P.	N.P.	N.P.	SC	25.1	-	-
	9	20.0	-	-	-	99	61	20	41	CH	38.9	-	-
	232, 1	1.5	-	-	-	100	62	20	42	CH	35.3	-	-
3	4.5	100	100	100	98	58	19	39	CH	36	83	$1.1 \times 10^{-8}$	-
	5	7.5	-	-	-	89	29	18	21	CL	24.1	-	-

$2.1 \times 10^{-8}$  (A)  
 $1.1 \times 10^{-7}$  (A)

NOTE: A) Two Permeability Tests performed on composite material of all samples from TP-3, TP-6, and TP-7.

## GENERAL NOTES:

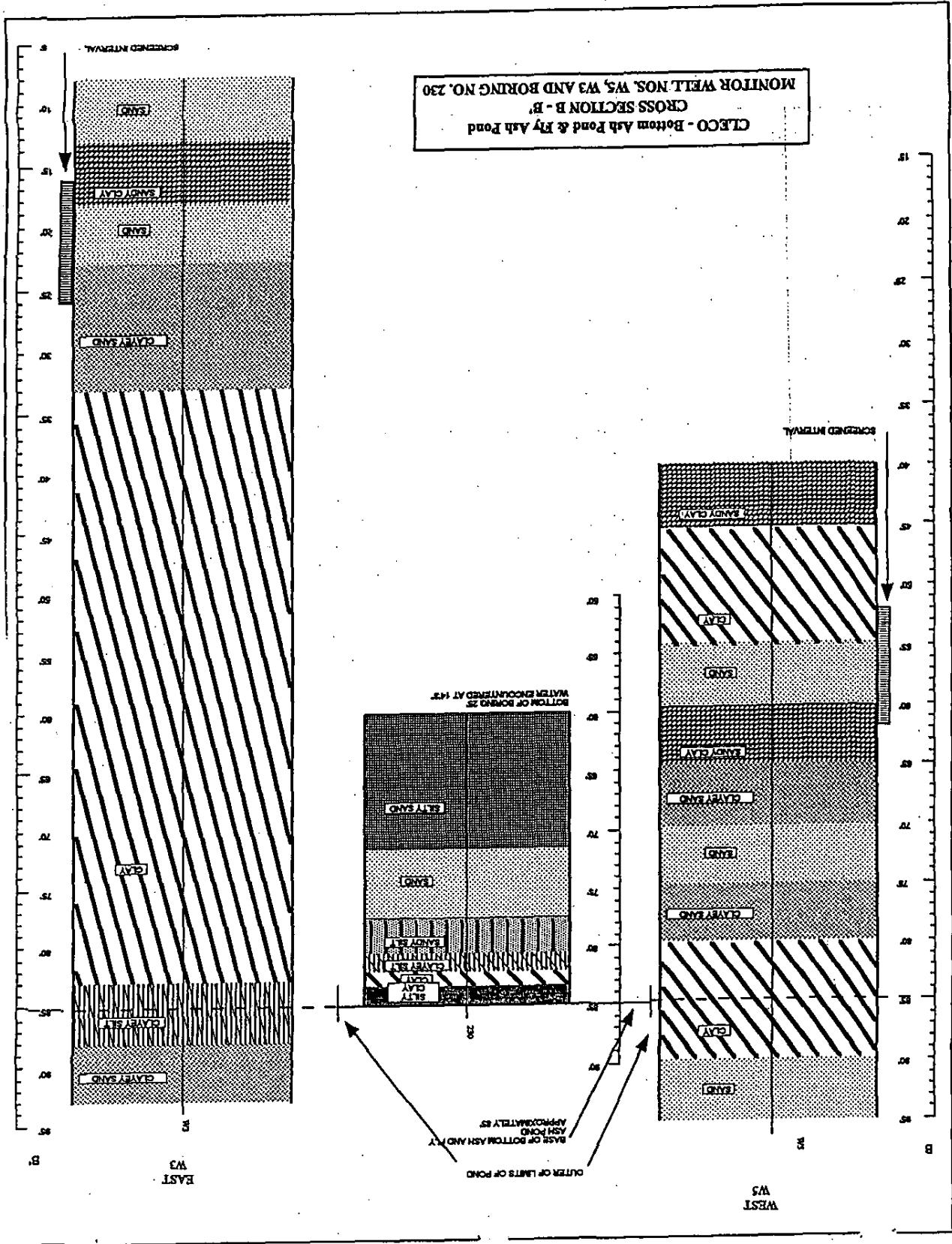
(1) Laboratory testing performed by Southwestern Laboratories, Inc., Shreveport, Louisiana.

(2) Laboratory Particle-Size Analysis Tests performed in accordance with ASTM D422 and ASTM D1140.

(3) Laboratory Atterberg Limit Tests performed in accordance with ASTM D423 and ASTM D424.

(4) Laboratory Water Content Tests of Soils performed in accordance with ASTM D2216. Most of Water Content Tests performed on split-specimen samples.

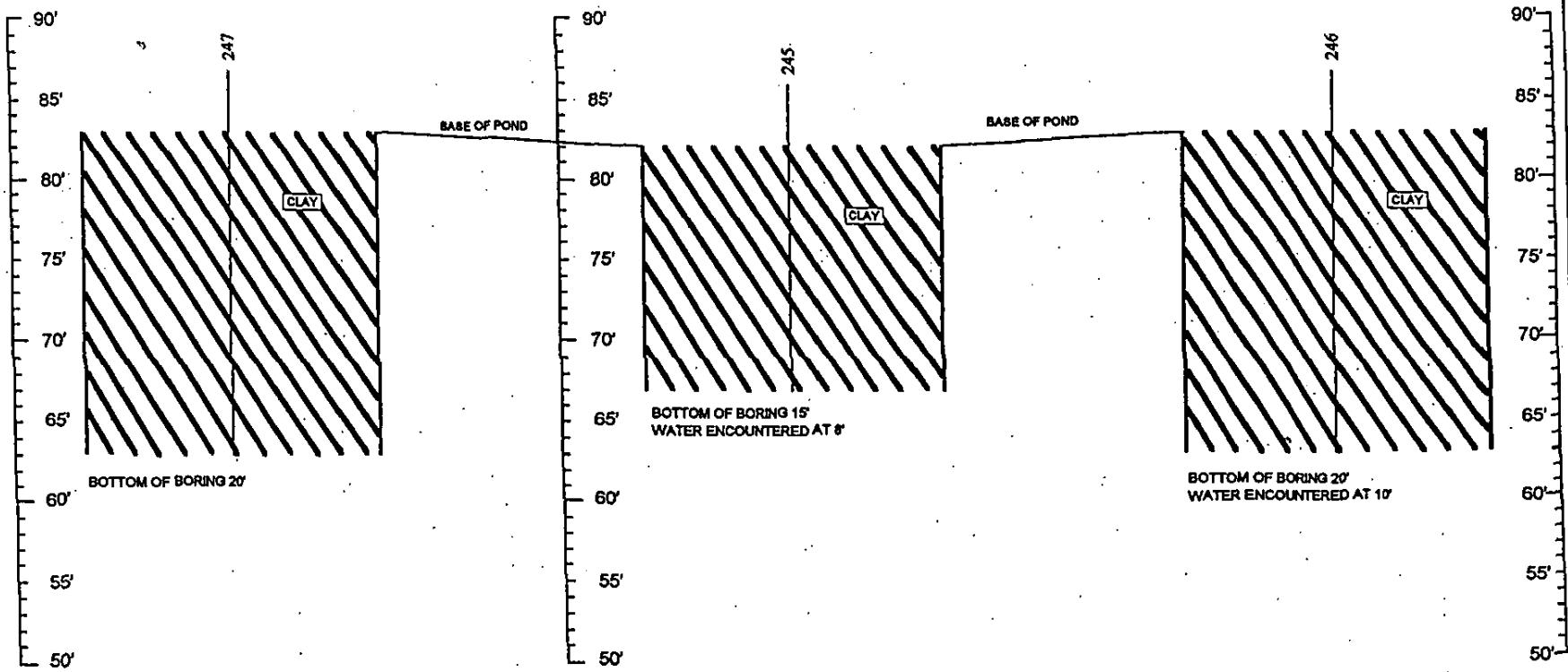
(5) Laboratory Vertical Permeability Test performed on undisturbed Shelby tube samples unless otherwise



CROSS SECTION  
C - C'  
247, 245, 246

C  
SOUTH  
247

C'  
NORTH  
246

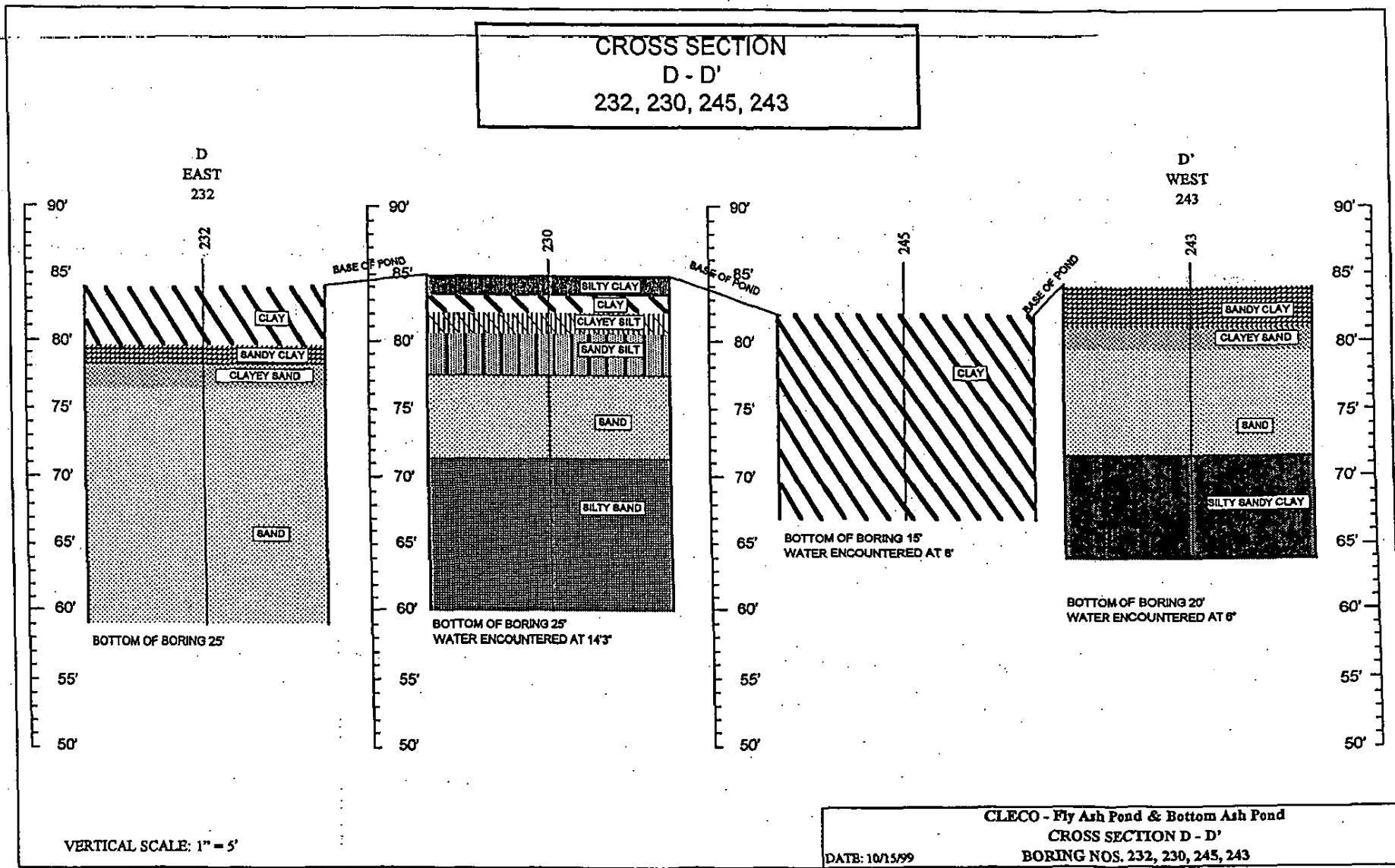


VERTICAL SCALE: 1" = 5'

CLECO - Bottom Ash Pond  
CROSS SECTION C - C'  
BORING NOS. 247, 245, 246

DATE: 10/15/99

CROSS SECTION  
D - D'  
232, 230, 245, 243



## **APPENDIX D – DESIGN DOCUMENTS**

## **S21.F. FACILITY PLANS AND SPECIFICATIONS**

### **1. CERTIFICATION**

Appendix D contains a certification by the person who prepared the permit application in accordance with 33.VII.521.F.1

### **2. INFORMATION REQUIRED FOR TYPE I AND II FACILITIES**

#### **2.a. Topography**

Typical cross sections of the above ground structures for the Bottom Ash Pond are shown in Exhibits 16, 17 and 18.

#### **2.b. Levee Construction**

Exhibit 12 shows the Bottom Ash Pond with original and final contours. The Bottom Ash Pond is located on both alluvial and terrace deposits. The surface area of the pond is 36 acres at elevation 106. The dikes built for the pond have a slope of 3 horizontal to 1 vertical. Four inches of seeded top soil are placed on the outward portions of the dikes for erosion control. The limits of excavation were controlled by the required design size. The ash pipe corridor is also shown in Exhibit 17 along with the discharge channel to the NPDES discharge point. Cross sections of the bottom ash dikes and other details are shown in Exhibit 16.

The size of the pond was designed to accommodate the bottom ash sludge expected to be generated over the lifetime of Unit 2. It is not planned to monitor the daily quantities put into the Bottom Ash Pond beyond normal plant engineering practice of every few years recording an elevation of the top of the sludge and computing the remaining volume versus projected disposal volumes.

Erosion protection was constructed at the water's edge after approval by the LDEQ in 1992.

#### **2.c. Construction Materials**

The levees were constructed from on-site materials. Since additional construction is not anticipated, calculations are not applicable. Erosion protection is concrete fabriform.

### **3. INFORMATION REQUIRED FOR TYPE I, II, AND III LANDFILLS**

#### **3.a. Daily Fill and Cover**

This section is not applicable to surface impoundments.

#### **3.b. Cover Material**

This section is not applicable to surface impoundments.

521.F (cont'd)

**4. PREVENTION OF GROUNDWATER CONTAMINATION**

**4.a. Representative Cross-Sections**

The soil types underlying the Bottom Ash Pond comprised a minimum of 3 feet of compacted clay over silty to clayey sands or very plastic in situ clay (CH). Cross sections of the subsurface conditions are shown in Exhibits 13 and 14.

**4.b. Liner System**

The ground water table is at least 6 feet below construction grade and the 6 feet of soil between the ground water and the bottom of the pond is a CH material. In the northwestern part of the Bottom Ash Pond and in the surrounding dikes, the minimum thickness of compacted clay is 3 feet. The natural impermeability of the in situ soils and the compacted clay liner form a suitable protective barrier to the ground water.

No leachate collection or treatment facilities are needed for the liquid waste pumped to the Bottom Ash Pond. The design of the facility incorporates an impermeable silty clay liner within the dike and over the western portion (see Exhibit 13 for limits) with a natural silty clay liner along the remaining bottom portion of the pond.

**4.c. Leachate Collection and Removal System**

A leachate collection and removal system was not included as part of the original design of the facility.


No leachate collection and/or treatment system is planned for the Bottom Ash Pond since it is designed to contain liquids.

**5. GROUNDWATER MONITORING**

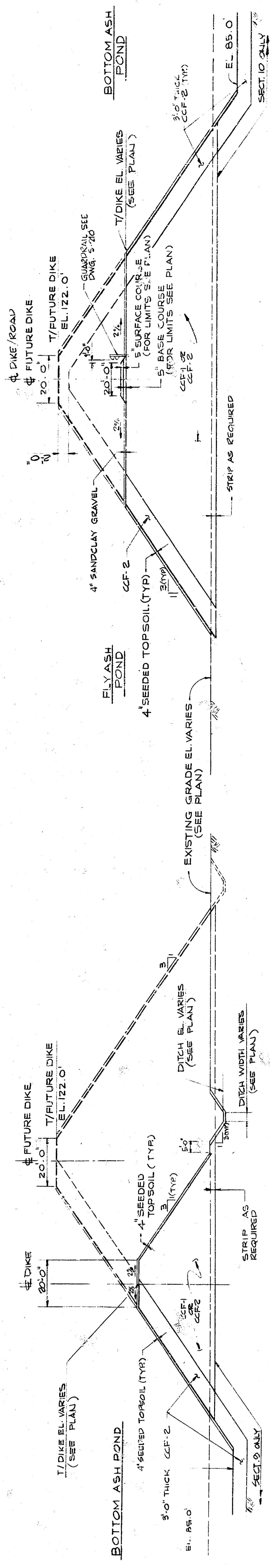
Appendix E contains a comprehensive groundwater monitoring program.

**6. GAS COLLECTION AND TREATMENT SYSTEM**

A gas collection and treatment system is not provided because surface impoundments do not have a potential to produce any gases.

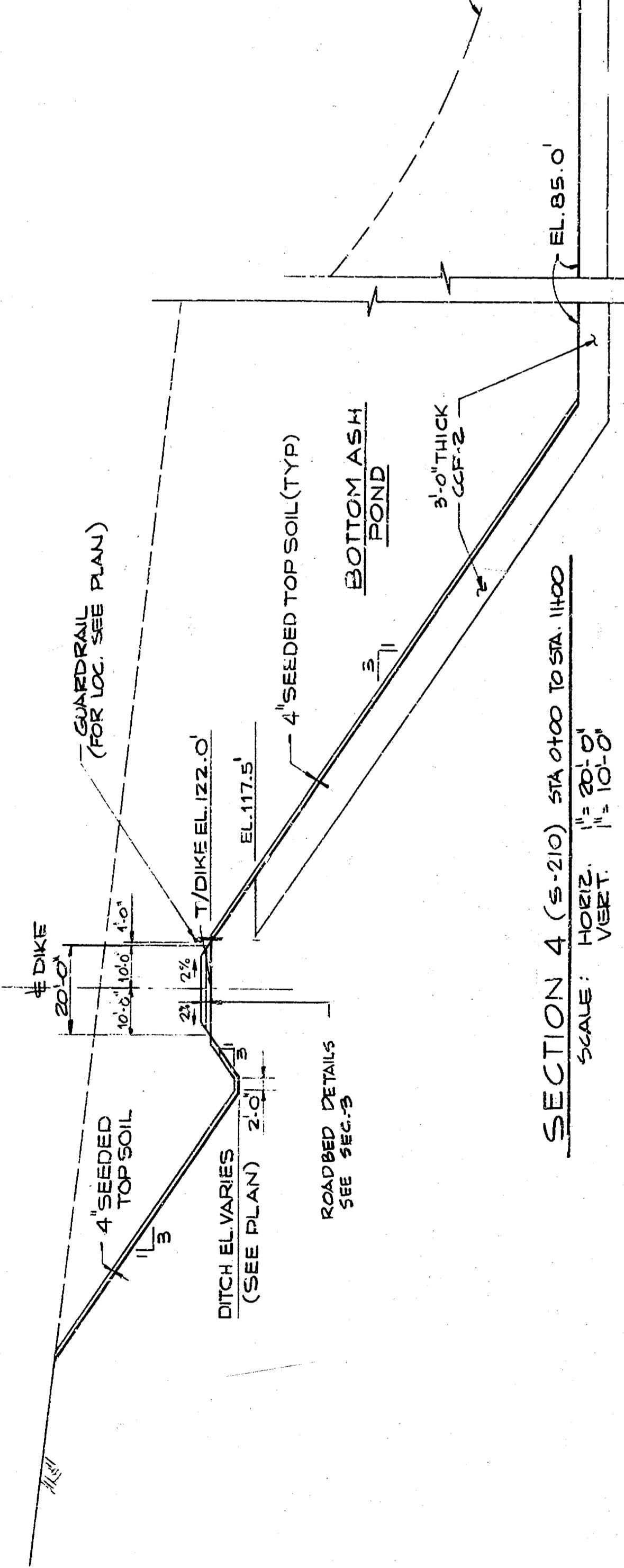


S-21



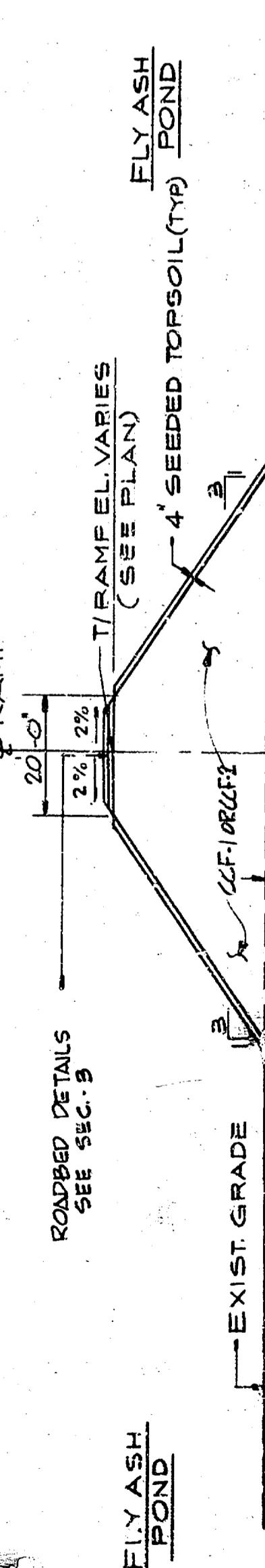
SECTION 2 AS NOTED (S-210) STA 8150 TO STA 27+92.07

SECTION 2 AS NOTED (S-210) STA 1100 TO STA 8150  
SCALE : HORIZ. 1"-20'-0" VERT. 1"-10'-0"



SECTION 4 (S-210) STA 8150 TO STA 1100

SCALE : HORIZ. 1"-20'-0" VERT. 1"-10'-0"



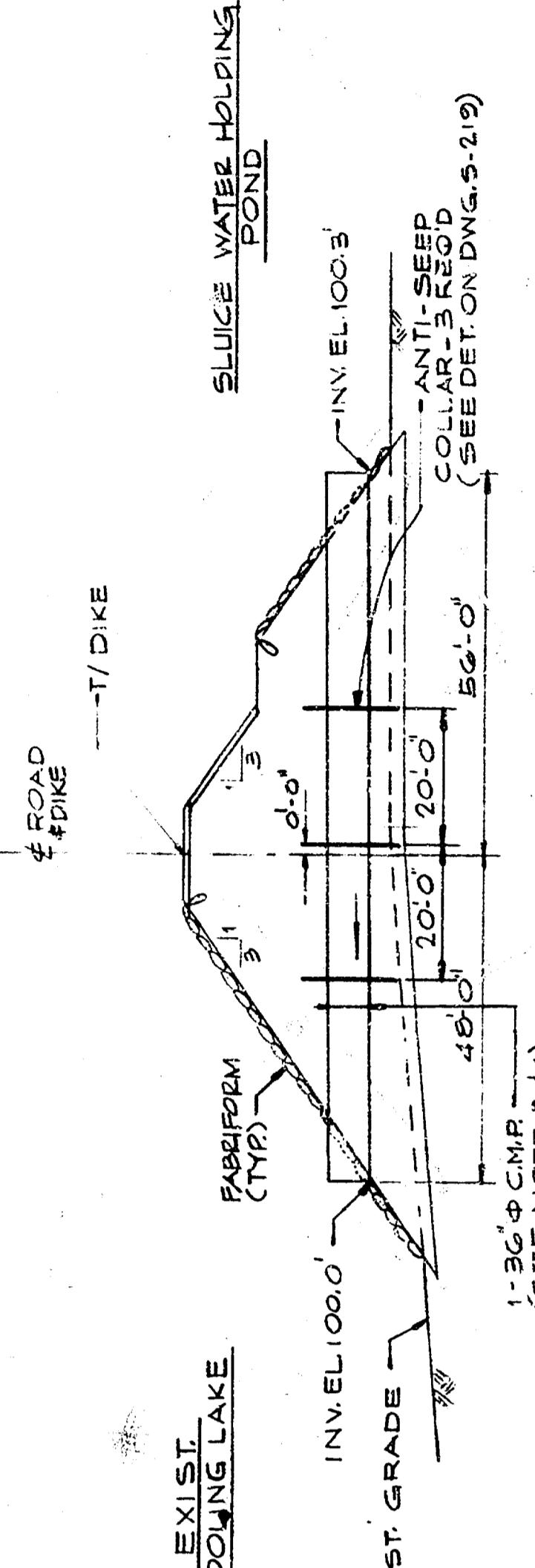
SECTION 6 (S-210) STA 8150 TO STA 8151

SCALE : HORIZ. 1"-20'-0" VERT. 1"-10'-0"



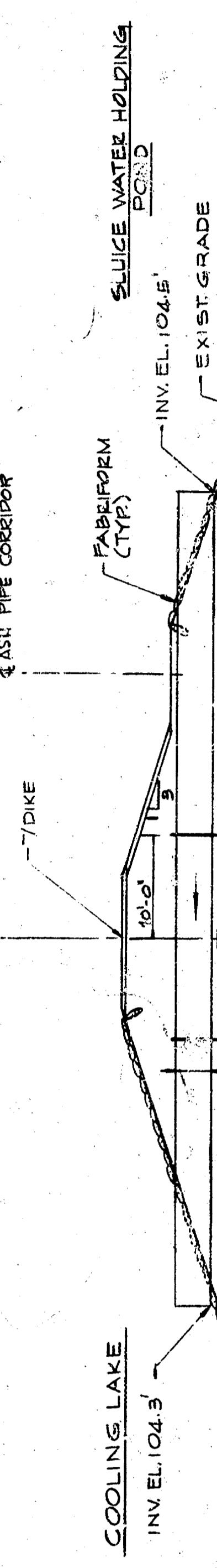
SECTION 3 (S-210) CENTER DIKE STA 9150 TO STA 24+19.46

SECTION 10 AS NOTED (S-210) CENTER DIKE STA. 9150 TO STA. 9150  
SCALE : HORIZ. 1"-20'-0" VERT. 1"-10'-0"



SECTION 5 (S-210)

SCALE : HORIZ. 1"-20'-0" VERT. 1"-10'-0"



SECTION 7 (S-210)

SCALE : 1"-10'-0"

**NOTES**


1. FOR GENERAL NOTES SEE DRAWING S-206.  
2. ALL NEW WORK SHOWN ON THIS DRAWING SHALL BE BY THE GENERAL WORK CONTRACTOR IN ACCORDANCE WITH SPECIFICATION R-3810 UNLESS PROVIDED OTHERWISE.  
3. COAL ASH AND BOTTOM ASH ARE TO BE PLACED IN LAYERS NO MORE THAN 12 INCHES THICK AND PROVIDED WITH TRANSFERS STANDARDS DOUBLE BUTT WELDS, COATING WITH MINIMUM THICKNESSES OF ONE INCHES (SO MILS) EACH FACE.  
4. IN COAL ASH AND BOTTOM ASH LAYERED PIPE IS TO BE USED AS APPROVED EQUIPMENT NO. 1005G-A OR APPROVED EQUIPMENT NO. 1005G-B.

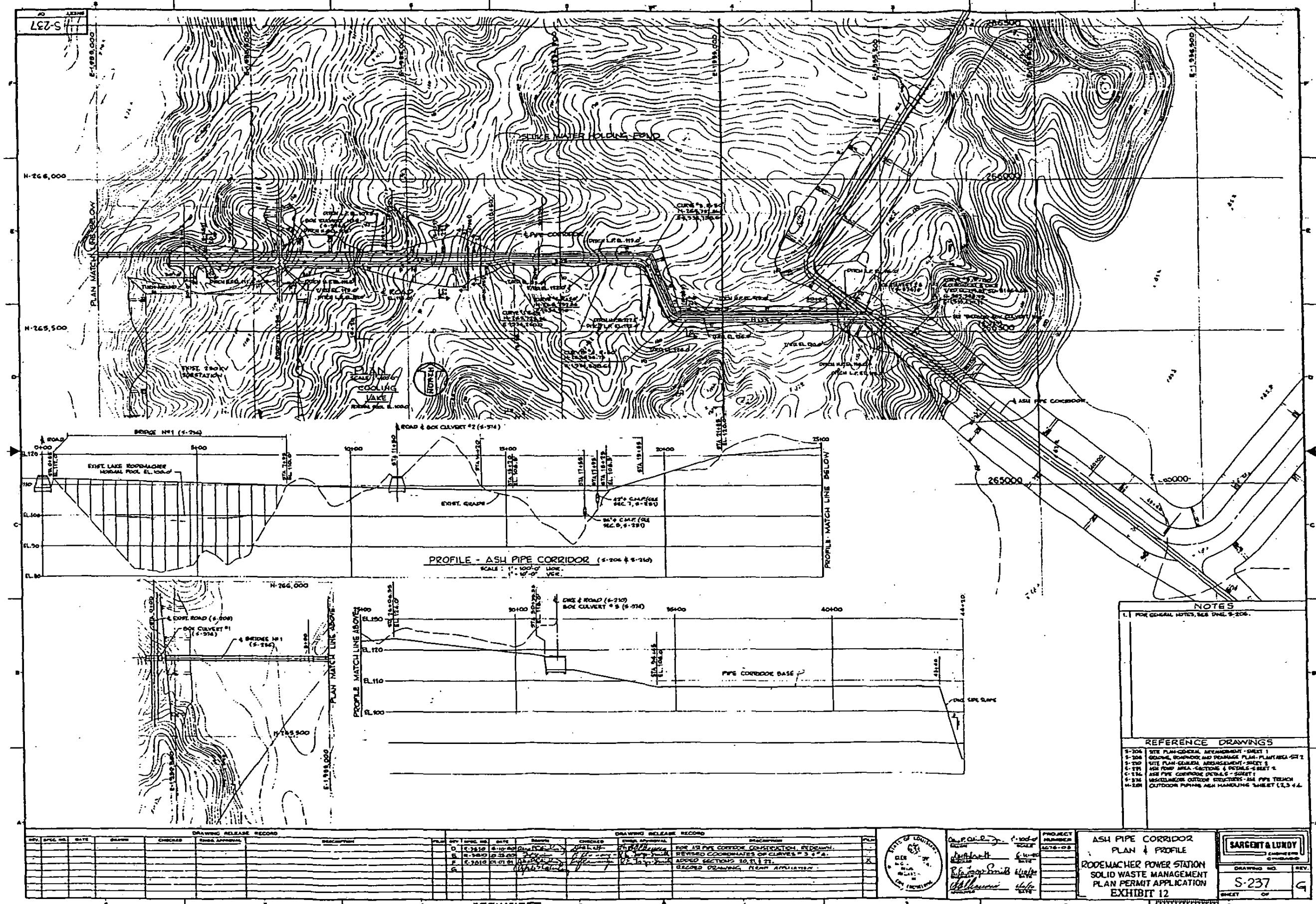
**REFERENCE DRAWINGS**

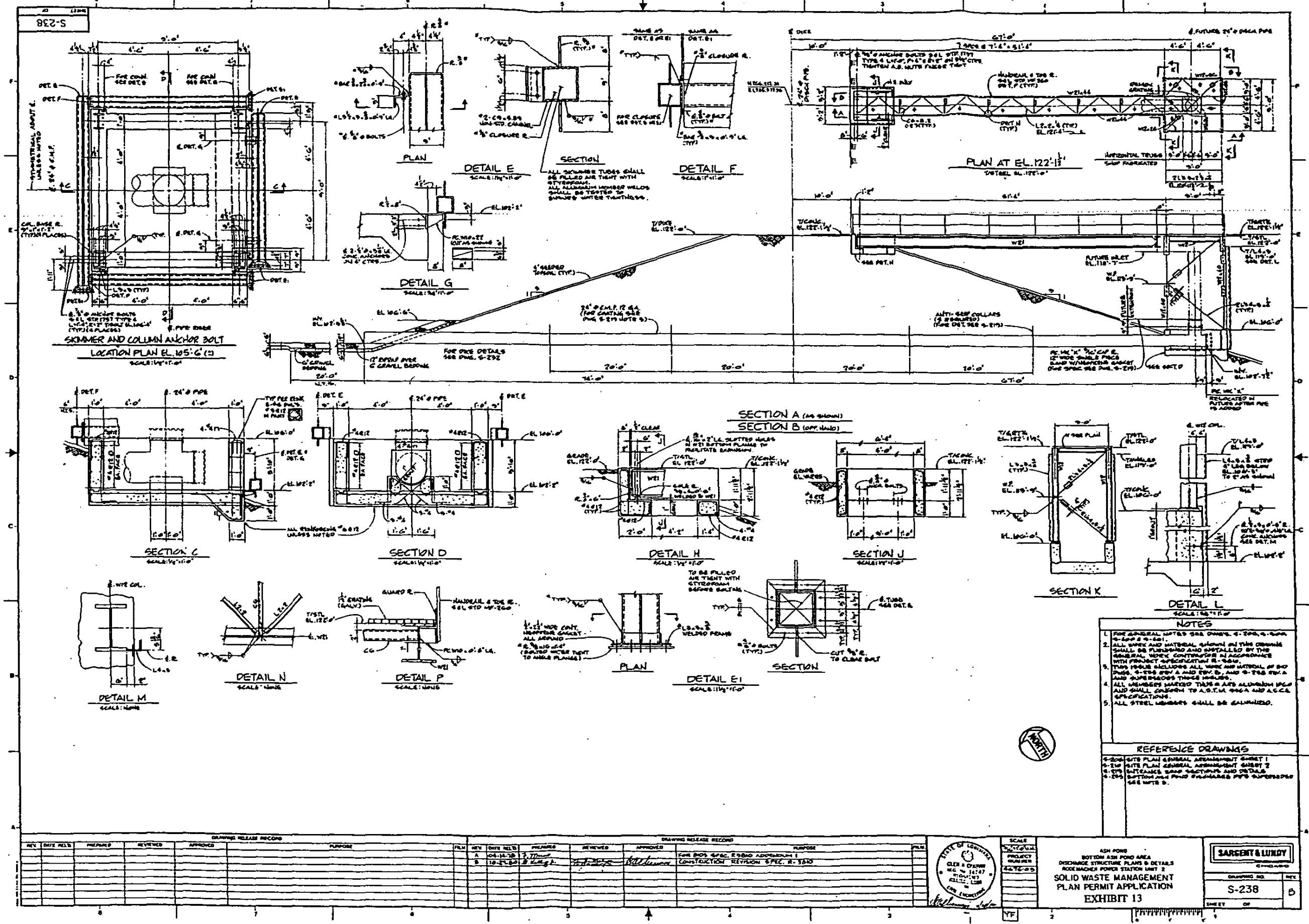
S-206 SITE PLAN - GENERAL ARRANGEMENT SHEET 1  
S-210 SITE PLAN - GENERAL ARRANGEMENT SHEET 2  
S-211 GUARDRAIL PIPING  
S-212 ASH PIPE CORRIDOR - SECTION 1  
S-213 ASH PIPE CORRIDOR - SECTION 2  
S-214 ASH PIPE CORRIDOR - SECTION 3  
S-215 ASH PIPE CORRIDOR - SECTION 4  
S-216 ASH PIPE CORRIDOR - SECTION 5  
S-217 ASH PIPE CORRIDOR - SECTION 6  
S-218 ASH PIPE CORRIDOR - SECTION 7  
S-219 ASH PIPE CORRIDOR - SECTION 8

NEW DATE REV'D	PREPARED	REVIEWED	APPROVED	DRAWING RELEASE RECORD			PURPOSE	
				FILM	REV. DATE REC'D	PREPARED	APPROVED	PURPOSE
A 04-14-78	W. J. Lembke							FOR ELLIS - SPEC. R-3810 ADDENDUM 1
B 04-14-78								GENERAL REVISION FOR ASH POND DIKE CONSTRUCTION, SPEC. R-3810
C 04-22-78								REMOVED HOLD SPEC. R-3810
D 04-22-78								REMOVED HOLD SPEC. R-3810
E 4-27-81	P. Chabot							REMOVED SECTION 4, ADD. R-3810
F 02-03-82								REMOVED DRAWING, RECENT APPLICATION
G 02-03-82								REMOVED SECTION 2, ELLIS


SARGENT & LUNDY		PROJECT NUMBER		SCALE	
INGENIERIE	CHICAGO	S-206	SITE PLAN - GENERAL ARRANGEMENT SHEET 1	GRAPHIC SCALE	1"-20'-0"
		S-210	SITE PLAN - GENERAL ARRANGEMENT SHEET 2	GRAPHIC SCALE	1"-10'-0"
		S-211	GUARDRAIL PIPING	GRAPHIC SCALE	1"-10'-0"
		S-212	ASH PIPE CORRIDOR - SECTION 1	GRAPHIC SCALE	1"-10'-0"
		S-213	ASH PIPE CORRIDOR - SECTION 2	GRAPHIC SCALE	1"-10'-0"
		S-214	ASH PIPE CORRIDOR - SECTION 3	GRAPHIC SCALE	1"-10'-0"
		S-215	ASH PIPE CORRIDOR - SECTION 4	GRAPHIC SCALE	1"-10'-0"
		S-216	ASH PIPE CORRIDOR - SECTION 5	GRAPHIC SCALE	1"-10'-0"
		S-217	ASH PIPE CORRIDOR - SECTION 6	GRAPHIC SCALE	1"-10'-0"
		S-218	ASH PIPE CORRIDOR - SECTION 7	GRAPHIC SCALE	1"-10'-0"
		S-219	ASH PIPE CORRIDOR - SECTION 8	GRAPHIC SCALE	1"-10'-0"



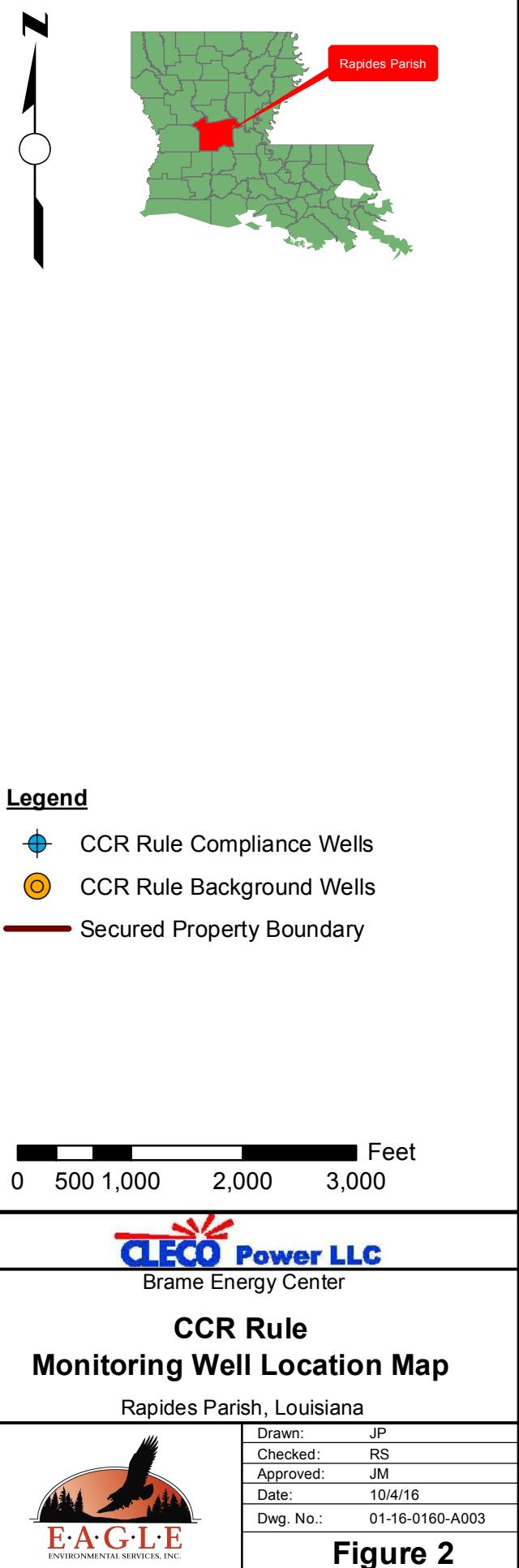




## **APPENDIX E - DIVERSION DESIGN FEATURES**



## **APPENDIX F - INSTRUMENTATION**



8  
7  
6  
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2  
1

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D

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C

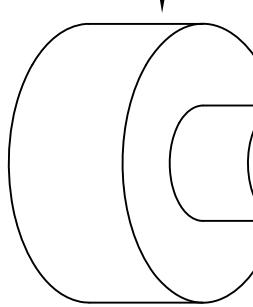
B

B

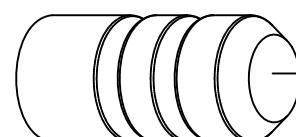
A

A

SUCTION STRAINER TYPICAL



BOWL ASSEMBLY



ENCLOSURE TUBE ASSEMBLY

GIB KEY

LINE SHAFT

TENSION BEARING

ENCLOSURE TUBE O-RING SEAL

TOP OIL SEAL

MOTOR DRIVE COUPLING, THREADED

PUMP DRIVE COUPLING, THREADED

MOTOR DRIVE COUPLING

DRIVE KEY

MOTOR ATTACHMENT BOLTS AS REQUIRED

ELECTRIC MOTOR

CANFIELD CUSTOM PUMPS

GENERAL PUMP ASSEMBLY DETAIL

ASSEMBLY-00406

REV 2

SCALE: NONE

SIZE B

DWG. NO.

WEIGHT:

SHEET 1 OF 1

NEXT ASSY

USED ON

FINISH

DO NOT SCALE DRAWING

COMMENTS

INTERPRET GEOMETRIC TOLERANCING PER

Q.A.

MATERIAL

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D.S.F., INC.

GENERAL PUMP ASSEMBLY DETAIL

ASSEMBLY-00406

REV 2

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SIZE B

DWG. NO.

WEIGHT:

SHEET 1 OF 1

NEXT ASSY

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ASSEMBLY-00406

REV 2

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DWG. NO.

WEIGHT:

SHEET 1 OF 1

NEXT ASSY

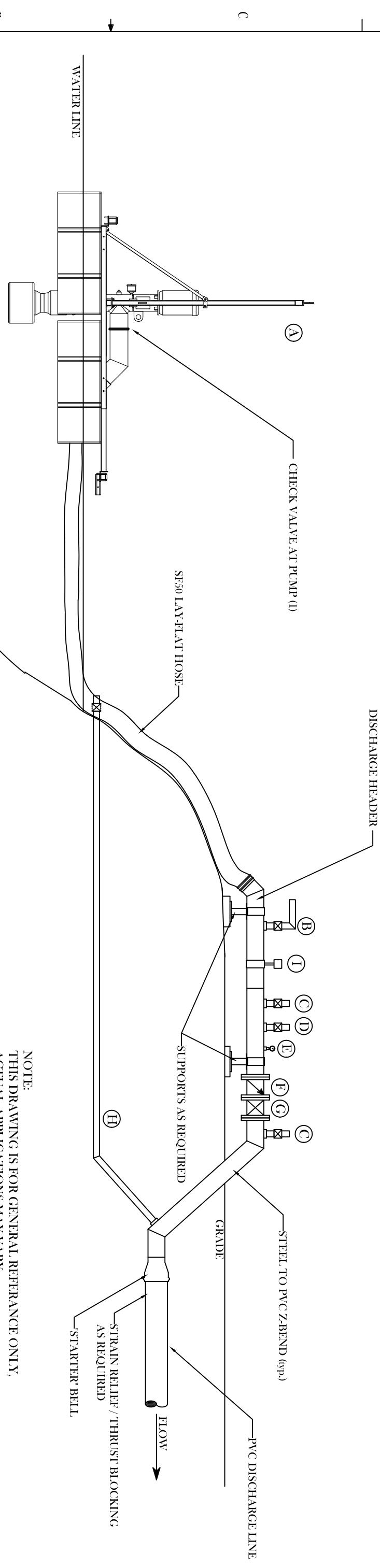
USED ON

FINISH

DO NOT SCALE DRAWING

## TYPICAL TURBI-FLOAT AGRICULTURAL INSTALLATION

A	TURBI-FLOAT PUMP
B	MANUAL BLOW-DOWN / RELIEF VALVE ASSY.
C	AIR RELEASE VALVE - VACUUM BREAKER
D	PRESSURE RELIEF VALVE - OPTIONAL
E	PRESSURE GAUGE
F	CHECK VALVE
G	ISOLATION VALVE
H	OPTIONAL DRAIN LINE w/ VALVE
I	OPTIONAL FLOW METER



**NOTE:**  
THIS DRAWING IS FOR GENERAL REFERENCE ONLY.  
ACTUAL APPLICATIONS MAY VARY.

**NOTE:**  
THIS DRAWING IS FOR GENERAL REFERENCE  
ACTUAL APPLICATIONS MAY VARY.

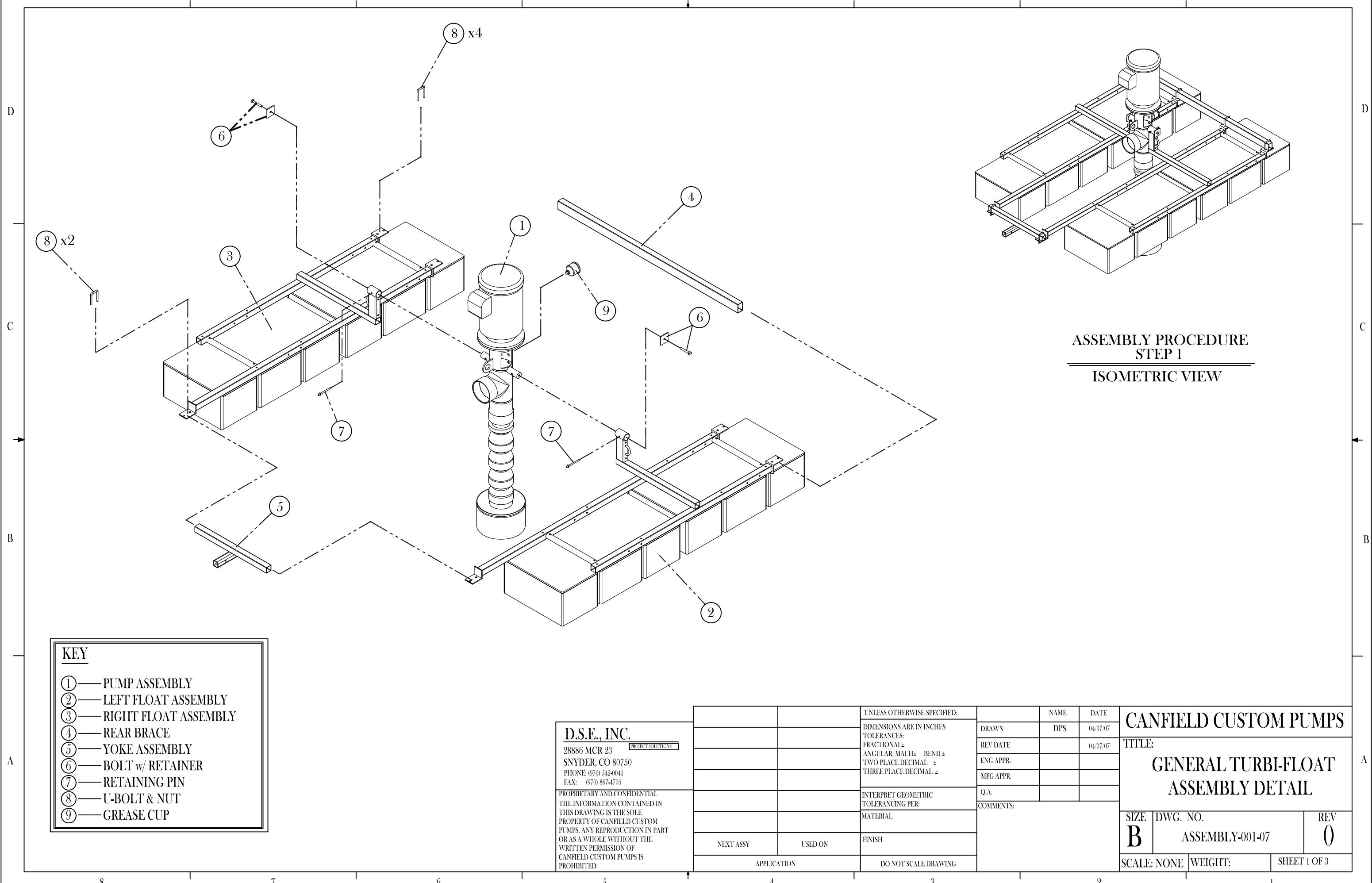
**STARUP:**  
1 - OPEN BLOW-DOWN VALVE PRIOR TO ENERGIZING PUMP.

- 1-OPEN BLOW-DOWN VALVE PRIOR TO ENERGIZING PUMP.**  
**2-SLOWLY CLOSE BLOW-DOWN VALVE AFTER SYSTEM FLOW IS INITIATED.**  
**(TO PREVENT HYDRAULIC SHOCK ON THE HOSE.)**

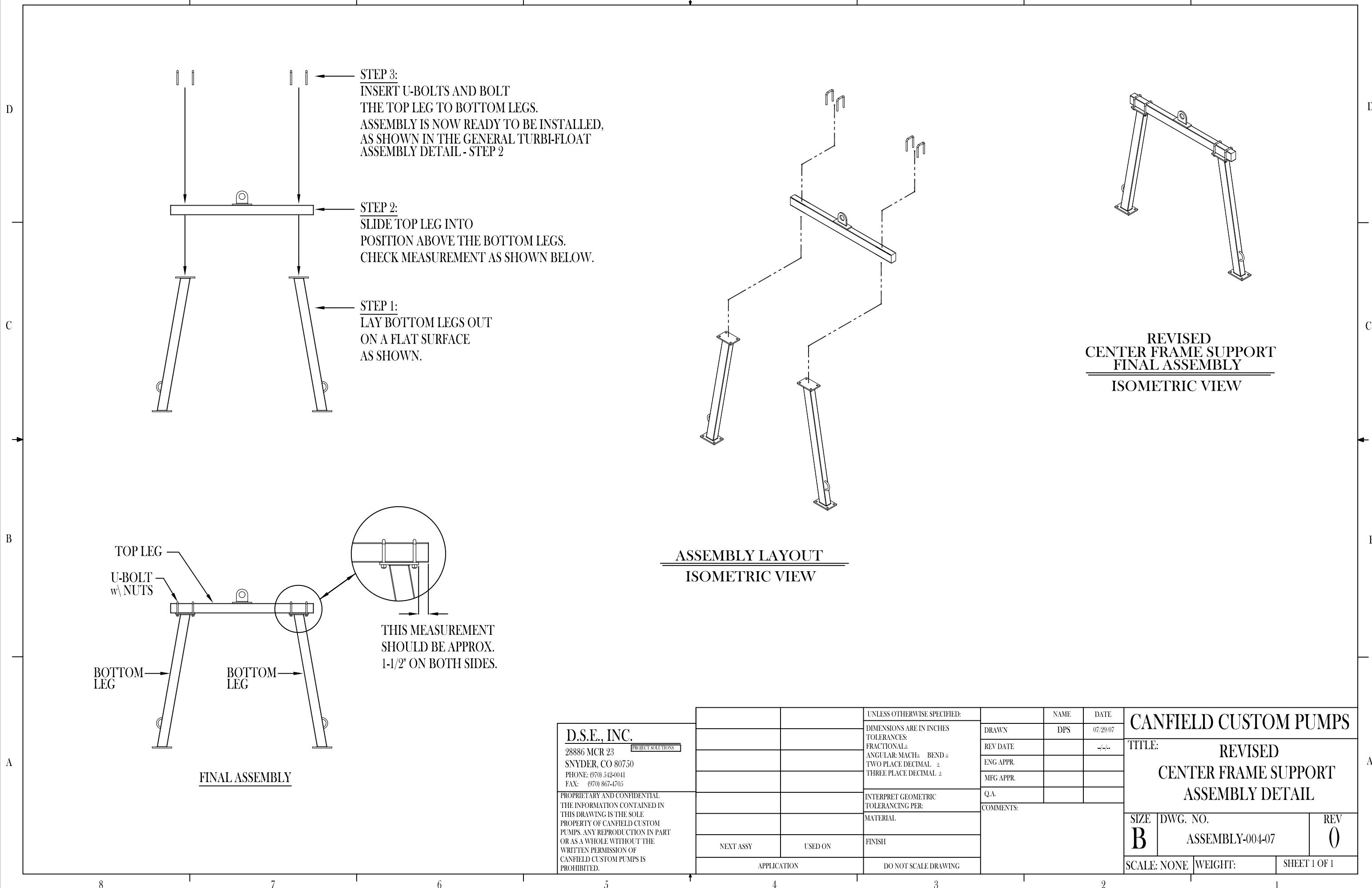
**NOTE: (1)**  
AUTOSTART SYSTEMS MAY REQUIRE USE OF A CHECK VALVE  
AT THE PUMP DISCHARGE TO PREVENT HYDRAULIC SHOCK ON THE HOSE,  
CONSULT MANUFACTURER FOR ASSISTANCE.

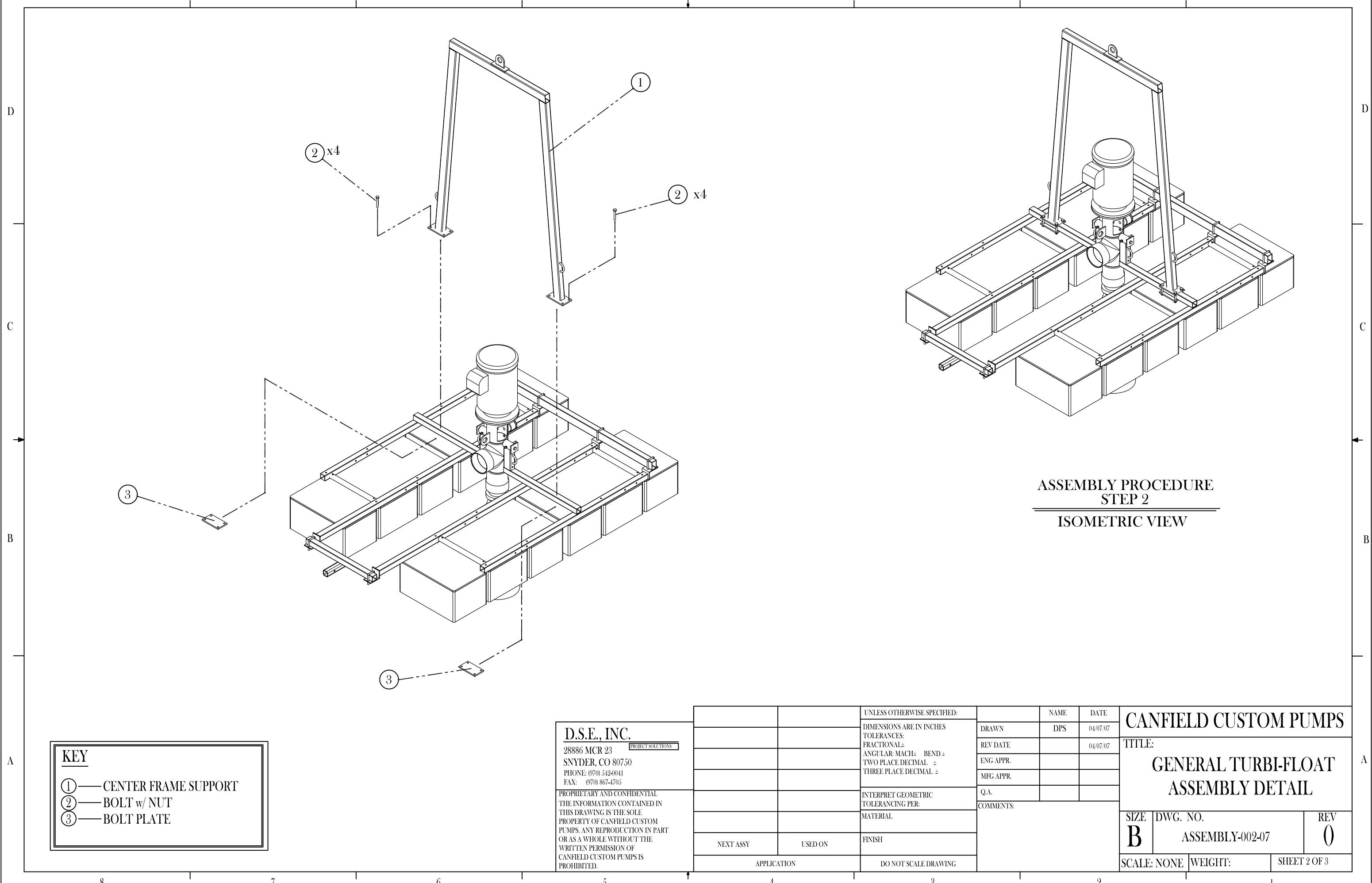
		UNLESS OTHERWISE SPECIFIED:	
		DIMENSIONS ARE IN INCHES	DRAWN
		TOLERANCES:	DPS
		FRACTIONAL $\pm$	REVISED
		ANGULAR MACH $\pm$ BEND $\pm$	DPS
		TWO PLACE DECIMAL $\pm$	01/15/09
		THREE PLACE DECIMAL $\pm$	TITLE:
		INTERPRET GEOMETRIC	<b>CANFIELD CUSTOM PUMPS</b>
		TOLERANCING PER:	
		MATERIAL:	
		Q.A.	
		COMMENTS:	
		SIZE:	DWG. NO.
		<b>B</b>	TF-AG-INSTALL-07
		SCALE: N.T.S.	REV
		WEIGHT:	<b>1</b>
		SHEET 1 OF 1	
NEXT ASY	USED ON	FINISH	
APPLICATION		DO NOT SCALE DRAWING	
PROHIBITED.			
CANFIELD CUSTOM PUMPS IS			
WRITTEN PERMISSION OF			
THIS DRAWING IS THE SOLE			
PROPERTY OF CANFIELD CUSTOM			
PUMPS. ANY REPRODUCTION IN PART			
OR AS A WHOLE WITHOUT THE			
PROHIBITED.			
THE INFORMATION CONTAINED IN			

8 7 6 5 4 3 2 1



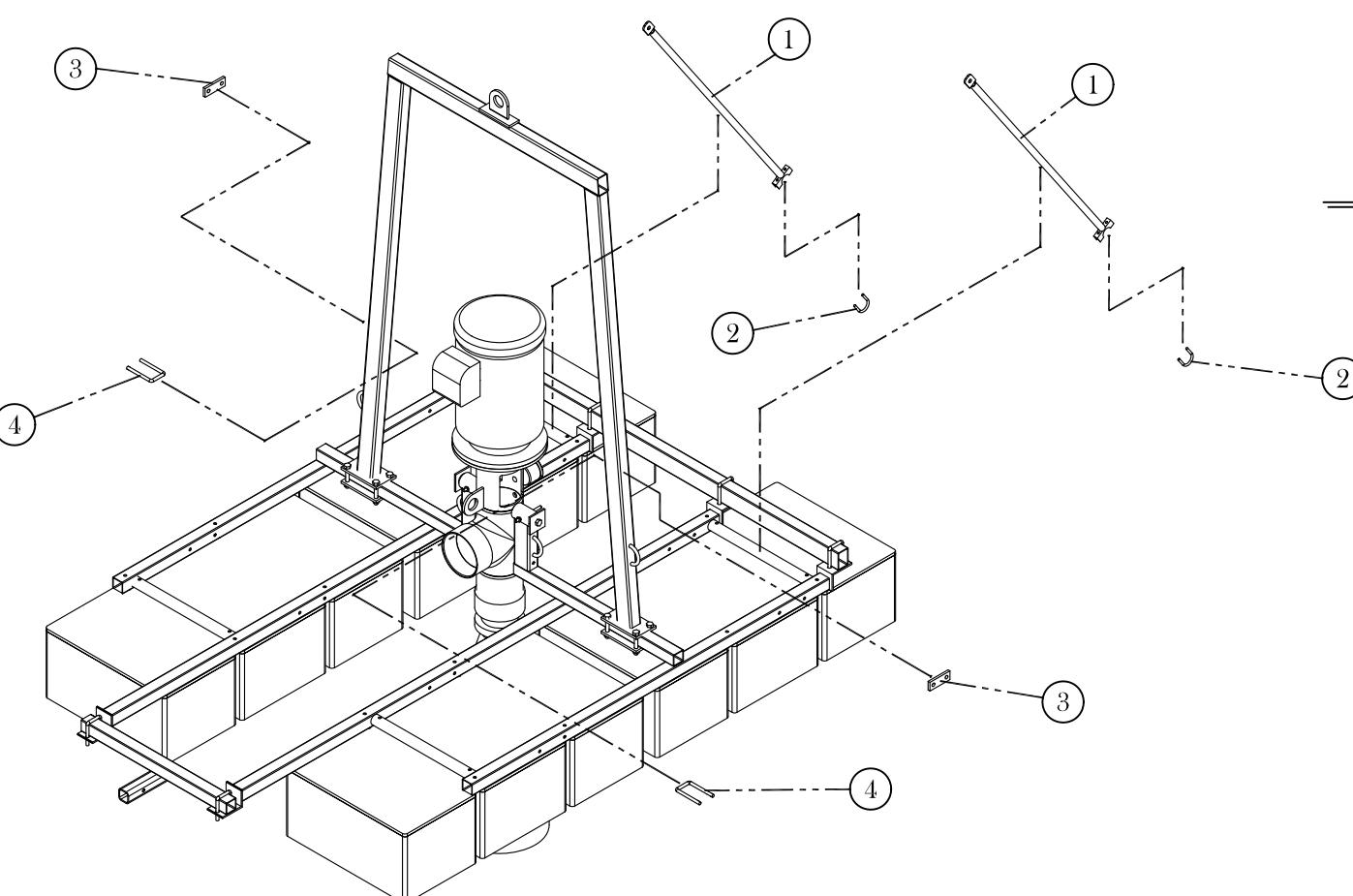
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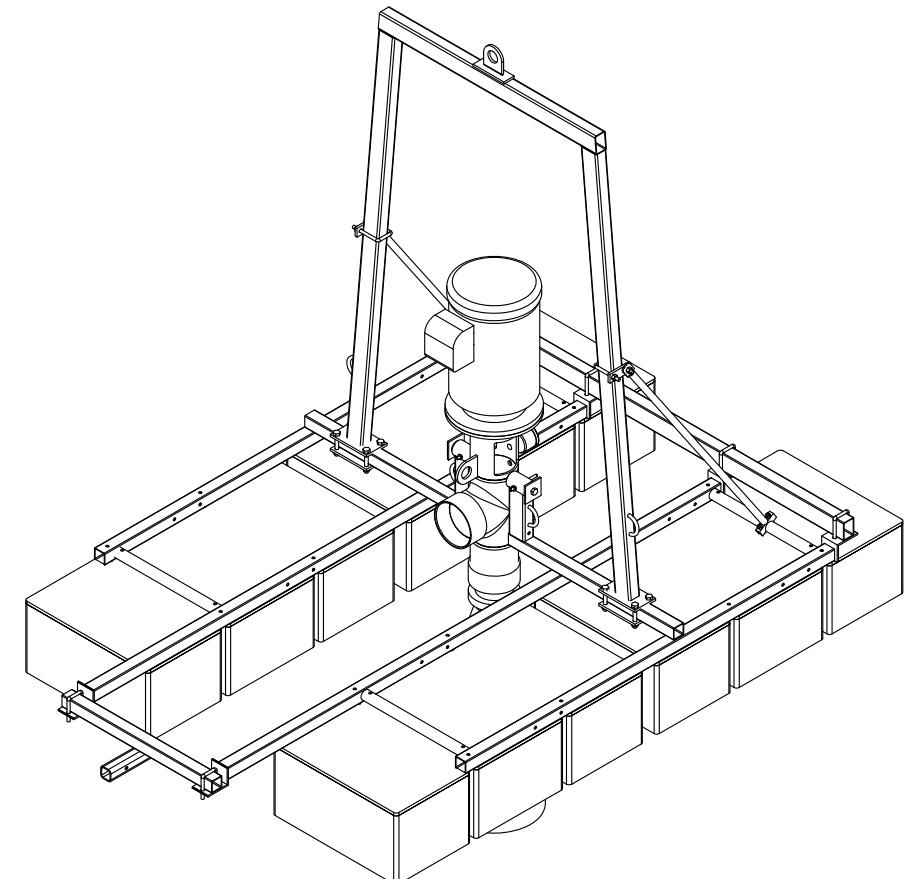


D

D



**COMPLETED BRACE  
ASSEMBLY**  
ISOMETRIC VIEW



**ASSEMBLY PROCEDURE  
STEP 3**  
ISOMETRIC VIEW

<b>KEY</b>	
①	REAR BRACE ASSEMBLY
②	MUFFLER U-BOLT w/ NUT
③	BOLT PLATE
④	U-BOLT w/ NUT

**D.S.E., INC.**  
PROJECT SOLUTIONS  
28886 MCR 23  
SNYDER, CO 80750  
PHONE: (970) 542-0411  
FAX: (970) 867-4705

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PUMPS. ANY REPRODUCTION IN PART  
OR AS A WHOLE WITHOUT THE  
WRITTEN PERMISSION OF  
CANFIELD CUSTOM PUMPS IS  
PROHIBITED.

		UNLESS OTHERWISE SPECIFIED:	NAME	DATE	<b>CANFIELD CUSTOM PUMPS</b>	
DIMENSIONS ARE IN INCHES		DRAWN	DPS	04/07/07	TITLE: <b>GENERAL TURBI-FLOAT ASSEMBLY DETAIL</b>	
TOLERANCES:		REV DATE		04/07/07		
FRACTIONAL $\pm$		ENG APPR.				
ANGULAR: MACH $\pm$ BEND $\pm$		MFG APPR.				
TWO PLACE DECIMAL $\pm$		Q.A.				
THREE PLACE DECIMAL $\pm$		INTERPRET GEOMETRIC TOLERANCING PER:			SIZE   DWG. NO.   REV <b>B</b> ASSEMBLY-003-07 <b>0</b>	
		MATERIAL				
		NEXT ASSY	USED ON	FINISH		
		APPLICATION		DO NOT SCALE DRAWING		
					SCALE: NONE	WEIGHT:
						SHEET 3 OF 3

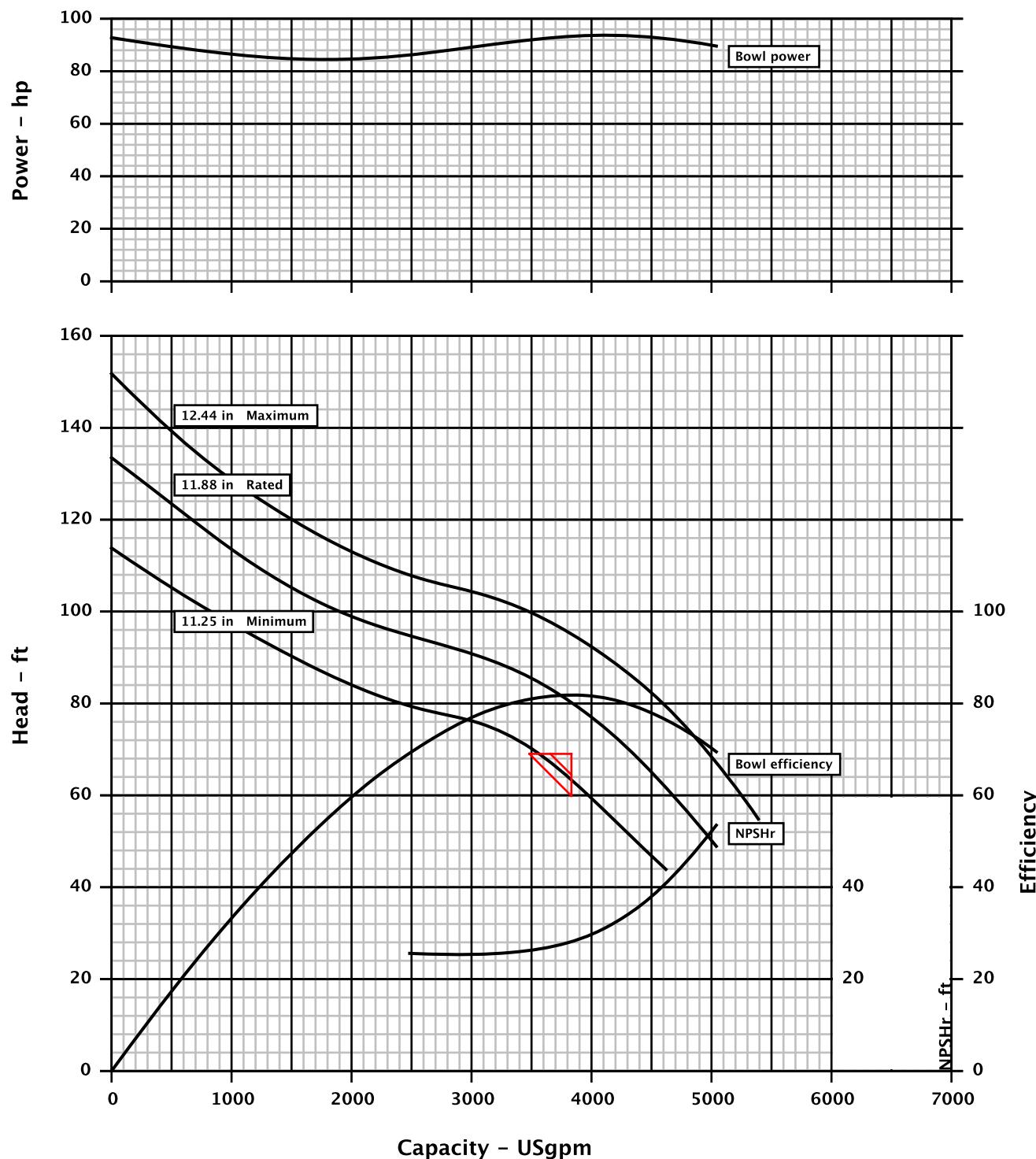


Pump size & type : 16ENH  
Based on curve no. : EC-1822  
Number of stages : 1

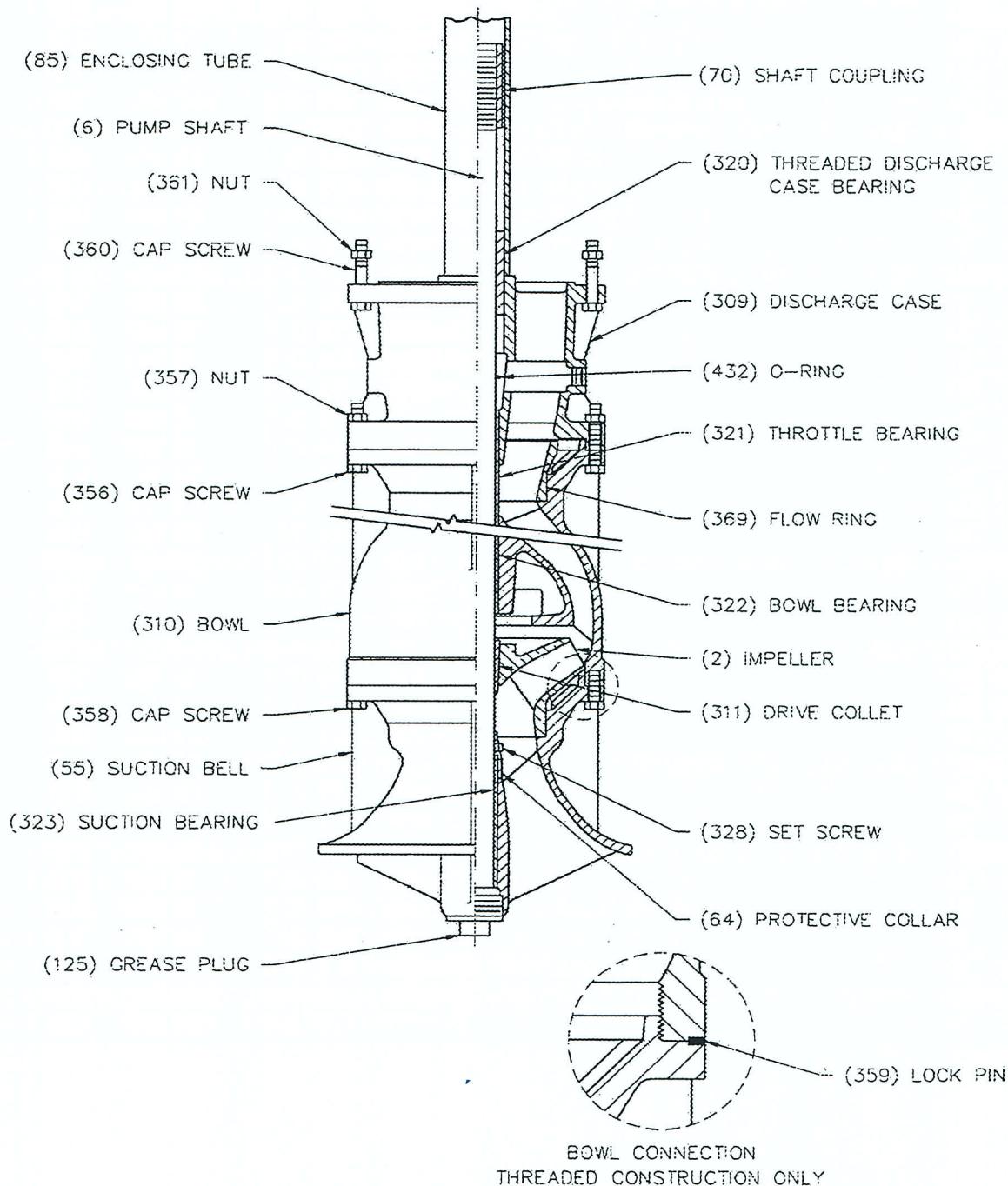
Customer : Canfield Drilling	Capacity : 3841.0 USgpm
Item number : -	Head : 69.00 ft
Service :	Specific gravity : 1.000
Flowserve reference : Default 0.1	Pump speed : 1770 rpm
Date : February 13, 2014	Test tolerance : Hydraulic Institute Level A

CURVES ARE APPROXIMATE, PUMP IS GUARANTEED FOR ONE SET OF CONDITIONS; CAPACITY, HEAD, AND EFFICIENCY.

Bowl performance shown below is corrected for materials, viscosity and construction.



Bowl head of 72.89 ft corresponds with 69.0 ft head at discharge flange adjusted for elevation and friction losses.

**BOWL ENCLOSED DESIGN FLANGED CONSTRUCTION  
OIL LUBE**


01-Apr-2001

NEW SHEET

**BOWL COMPONENTS****16EN BOWL**

PART NO.	REF. NO.	DESCRIPTION	LIST PRICE	MATERIAL	WEIGHT
<b>The Following to be Used With Type W Head</b>					
~	103	Lineshaft or Reducer Bearing, LH - To Match Bowl Oil Tube to Column Oil Tube	~	Brz	~
82189671	85	Bowl Oil Tube, 3-1/2 x 9-1/2, LH	\$125.00	Stl	10
82175696	320	Lineshaft Bearing, 2-3/16 x 3-1/2, LH	110.00	Brz	9.5
82189739	432	O-Ring, 2-3/16	0.25	Rub	~
82491655	309	Flow Adapter 15/16 x 10 Thd	850.00	C I	~
81813172	309	Flow Adapter 15/16 x 12 Thd	900.00	C I	~
82491804	309	Flow Adapter 15/16 x 10 Flg	850.00	C I	~
81813222	309	Flow Adapter 15/16 x 12 Flg	900.00	C I	~
82080920	320	Brg Thd Disc-CS 3-1/2 x 2-3/16 ID LH	250.00	Brz	~
81813016	309	Case Disc 15/16 x 10 Thd LH	1,000.00	C I	~
81812901	309	Case Disc 15/16 x 12 Thd LH	1,050.00	C I	~
81812851	309	Case Disc 15/16 x 14 Thd LH	1,150.00	C I	~
81813123	309	Case Disc 15/16 x 10 Flg LH	1,000.00	C I	~
81813016	309	Case Disc 15/16 x 12 Flg LH	1,000.00	C I	~
82007139	369	Flow Ring 16EN 10" Column	250.00	C I	~
82007105	369	Flow Ring 16EN 12" Column	250.00	C I	~
81782468	321	Bearing Sleeve / Throttle 2-3/16 x 2-7/8 x 10-1/2 LG	215.00	Brz	~
81855215	310	Bowl Intermediate 16EN	1,150.00	C I	~
82491812	322	Bearing Sleeve 2-3/16 x 2-7/8 x 4-1/2 LG	53.00	Brz	~
82007865	2	Impeller 16ENL full Diameter	1,000.00	Brz	~
82007873	2	Impeller 16ENH full Diameter	1,000.00	Brz	~
82006933	311	Collet Drive for 2-3/16 Shaft	27.00	Stl	~
82006909	64	Sand Collar for 2-3/16 Shaft	109.00	Brz	~
95231379	328	Set Screw for Sand Collar	0.10	SS	~
81855876	313	Case Suction 16EN x 12 Thd	1,050.00	C I	~
81855330	55	Bell Suction 16EN	1,050.00	C I	~
82491820	323	Bearing Sleeve 2-3/16 x 2-7/8 x 8 LG	122.00	Brz	~
95249645	125	Grease Plug 2-1/2 NPT	1.25	M I	~
95251872	358	Screw Cap Hex Head 5/8 x 1-3/4 (12 x # of stages + 12)	1.25	SS	~

All Prices FOB Hastings, Ne and Subject to Change Without Notice



CREATE AMAZING.

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